

PERFORMANCE OPTIMIZATION
OF AN OXYGEN PLANT
USING A COMPUTER SIMULATOR

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خاتمة

هذه الرسالة تبحث الدارة التشغيلية لمصنع الأكسجين سوفييتي الصنع وهو من النوع K-0.15 الذي يستخدم دورة تبريد ذات ضغط متوسط. إن هذا البحث يطمح أساساً الى تفصي إمكانية تحسين القدرة الإنتاجية للمصنع لمواجهة الطلب المتزايد على الأكسجين .

ولإنجاز حسابات الإيزانين الحراري والكتلي للعمليات التي تؤديها معدات المصنع فقد تم استخدام برنامج حاسوب للمحاكاة يعرف باسم CODE حيث تم بمساعدته إنشاء مخطط عمليات يحاكي دارة التشغيل للمصنع المذكور .

إن متطلبات الطاقة تعتبر العامل الأساسي في حساب كلفة الإنتاج ضمن مصنع الأكسجين . ومثل هذه المتطلبات يمكن التحكم بها من قِبل شبكة المبادلات الحرارية الموظفة في المصنع .

وللتنبؤ بشبكة مثلى للمبادلات الحرارية تم تبني تحليل تكاملي للطاقة باستخدام أسلوب يعرف بجدول المسألة (المشكلة) . وهو أسلوب غايته تحديد المتطلبات الدنيا من الطاقة للدارة التشغيلية .

ولما كانت دارة المصنع تتوفر على نوع واحد من هذه المتطلبات (متطلبات تبريد) أصبح ممكناً استخدام ما يعرف بالتصميم ذي الإسترداد الأقصى للطاقة ويرمز له بـ MER Design . وعن طريق التأخير يمكن توقع ومن ثم الإختبار بالحاسوب للوضع الأمثل الذي ينبغي أن تكون عليه مسارات العمليات . إن ما تم الحصول عليه من نتائج يبين أن الوضع المشار إليه يتفق مع الظروف التشغيلية لدارة المصنع . إضافة الى أنه تم التثبت من أن الوضع الجديد لمسارات العمليات يحقق خفضاً مقداره (21%) من المساحة اللازمة للانتقال الحرارية وذلك بثبوت القدرة الإنتاجية .

وعلاوة على ما تقدم ، فقد ظهر أن عمودي (برجي) التكرير بإمكانهما استيعاب معدل اضافي من المائع قيد التكرير يصل الى (60%) من أصل القيمة الإسمية لمعدل التدفق . مع ذلك فإن معدات رئيسية في المصنع (الضاغطة، مضخة الأكسجين السائل، منقي الهواء، الممدد التوربيني، وبعض أجزاء من شبكة الانابيب) ينبغي إعادة تصميمها اذا تقرر التوسع في القدرة الإنتاجية .

وبدراسة اقتصادية مقارنة في آخر البحوث تبين ان كلفة الوحدة المنتجة (متر مكعب واحد من غاز الاكسجين) في المصنع بعد رفع قدرته الإنتاجية بمقدار (860) تعادل ما نسبته (890) من الكلفة ذاتها اذا ما تم استخدام مصنع آخر مماثل للموجود حالياً.

ان النتائج التي ينتهي اليها هذا البحث لا تشجع على الاخذ بقرار توسعه المصنع الحالي .

CONTENTS

| | <u>page</u> |
|---|-------------|
| AKNOWLEDGEMENT | v |
| ABSTRACT | vi |
| NOMENCLATURE | viii |
| List of Tables | xi |
| List of Figures | xii |
| Chapter One | |
| INTRODUCTION | 1 |
| 1.1 Problem Statement | 1 |
| 1.2 Oxygen Plant | 2 |
| 1.2.1 Application | 2 |
| 1.2.2 Circuit arrangement and operating principles | 3 |
| a. General information | 3 |
| b. Modes of operation | 3 |
| Mode i | 3 |
| Mode ii | 7 |
| Mode iii | 7 |
| Mode iv | 7 |
| 1.2.3 Technical data | 8 |
| 1.2.4 Equipment list | 9 |
| 1.2.5 Individual description of equipment | 9 |

| | |
|----------------------------------|----|
| * Separation unit | 9 |
| * Heat exchanger, A4 | 10 |
| * Preliminary heat exchanger, A3 | 12 |
| * Sub-cooler, A21 | 13 |
| * Sub-cooler, A6 | 14 |
| * Lower column, A7 | 15 |
| * Upper column, A9 | 15 |
| * Packet (plate-fin condenser) | 16 |
| * Moisture separator | 17 |
| * Liquid-oxygen pump | 18 |
| * Turbo-expander | 18 |
| * Air purifier | 19 |
| * Air compressor | 21 |

Chapter Two

| | |
|---|----|
| LITERATURE SURVEY | 24 |
| 2.1 Oxygen Discovery | 24 |
| 2.2 Old Production Techniques | 26 |
| 2.3 Gas Liquefaction | 29 |
| 2.4 Heat Exchanger Network Optimization | 32 |

Chapter Three

| | |
|-------------------------|----|
| METHOD OF ANALYSIS | 36 |
| 3.1 CODE Program | 37 |
| 3.1.1 CODE skills | 39 |
| 3.1.2 Run procedure | 42 |
| 3.1.3 Equipment modules | 43 |

| | |
|------------------------------------|----|
| 3.2 Plant Simulation | 45 |
| - Air compressor | 47 |
| - Preliminary heat exchanger | 47 |
| - Air purifier | 48 |
| - Heat exchanger/ upper half | 48 |
| - Heat exchanger/ lower half | 49 |
| - Lower column | 50 |
| - Sub-cooler, A21 | 50 |
| - Sub-cooler, A6 | 50 |
| - Upper Column | 50 |

Chapter Four

| | |
|---|----|
| INVESTIGATION OF THE EXISTING PLANT | 54 |
| 4.1 Introduction | 54 |
| 4.1.1 Optimum process design | 54 |
| 4.2 Energy Integration Analysis | 56 |
| 4.2.1 Method of approach | 56 |
| 4.2.2 Stream definition | 58 |
| 4.2.3 Calculation of minimum energy requirements | 62 |
| 4.3 Maximum Energy Recovery Design | 68 |
| 4.3.1 Stream matching/ exchanger network | 68 |
| 4.4 Column-Tray Sizing | 78 |

Chapter Five

| | |
|-----------------------------|----|
| DISCUSSION OF RESULTS | 82 |
| 5.1 Base Design | 82 |

| | | |
|-------------|--|-----|
| 5.1.1 | Plant simulation | 82 |
| 5.1.2 | Evaluation of the heat exchanger network | 83 |
| 5.1.3 | Inspection of the air-separation unit/ rectifying columns | 96 |
| 5.2 | Economical Comparison of the Existing and the Proposed Designs | 99 |
| Chapter Six | | |
| | CONCLUSION | 106 |
| | REFERENCES | 108 |
| | APPENDIXES | 112 |
| | Appendix A : Temperature interval analysis | 113 |
| | Appendix B : Computer results of the simulating flowsheet of the oxygen plant of type K-0.15 | 136 |
| | Appendix C : Computer results of the optimized heat exchanger network of the oxygen plant | 171 |
| | Appendix D : Computer results of the column-tray sizing under the nominal flow rate of air | 183 |
| | Appendix E : Computer results of the column-tray sizing under 1.7 times the nominal flow rate of air | 202 |

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ABSTRACT

This thesis investigates the operating circuit of a Soviet made oxygen plant of type K-0.15 which employs a medium-pressure refrigeration cycle. The purpose of this investigation is to explore the possibility of improving the production capacity of the plant to meet the increasing market demand on oxygen.

A computer program, CODE, which is a steady state process simulator has been used to calculate heat and material balances of process equipment. A flowsheet is generated to simulate the operating circuit of the plant under consideration.

Energy requirements are considered to be the primary factor determining the production cost of the oxygen plant. Such requirements are controlled by the employed network of heat exchangers of the plant.

To predict the optimum exchanger network, the Energy Integration analysis is adopted using the Problem Table method. This method determines the minimum energy requirements of the operating circuit.

Since the plant circuit includes only one type of energy

requirements (that is cooling requirement), it has become possible to use the Maximum Energy Recovery (MER) design. Such type of a problem is sometimes referred to as threshold problem.

Using MER, an optimum configuration of process streams are predicted and checked by the computer simulator. The results obtained show that the predicted configuration complies with the operating conditions of the plant circuit. A reduction in heat transfer area of about 21% is found possible while keeping the production capacity invariant.

Furthermore, it is determined that the rectifying columns are capable of handling a flow rate 60% higher than the nominal flow rate value. However, major components of the plant (compressor, pump, purifier, turbo-expander and some piping) should be redesigned if expansion is implemented. A comparative economical study shows that the cost of unit production after expanding the existing plant by 60% points to 90% of the unit production cost if a new similar plant is erected. This result indicates that a decision to expand the plant may not be favourable.

NOMENCLATURE

- A : Surface area of heat transfer, m^2
- A1 & A2 : Moisture separators
- A3 : Preliminary heat exchanger
- A4 : Heat exchanger
- A6 : Three-way subcooler
- A7 : Lower column
- A8 : Plate-fin condenser
- A9 : Upper column
- A15 & A16 : Cylinders of the air purifier
- BP1, BP2 & BP3 : Throttle valves
- CP : Heat-capacity flow rate, $kW/^\circ C$
- CP_i : Heat-capacity flow rate of stream i, $kW/^\circ C$
- C_p : Specific heat, $kW/kg.^\circ C$
- d : Tube diameter, m
- D_e : Hydraulic diameter, m
- D_i : Inside diameter of the outer tube for
tube-in-tube section, m
- d_i : Inside diameter of the inner tube for
tube-in-tube section, m
- D_o : Outside diameter of the outer tube for
tube-in-tube section, m
- d_o : Outside diameter of the inner tube for

- tube-in-tube section, m
 dQ : differential heat flow-rate, kW
 \dot{H} : Enthalpy flow rate, kW
 H1 : Liquid-oxygen pump
 HAF : Heat availability function
 h : Film coefficient of heat transfer, $W/m^2 \cdot ^\circ C$
 h_i : Film coefficient of heat transfer based on
 the inside diameter of the tube, $W/m^2 \cdot ^\circ C$
 h_{io} : Modified h_i , $W/m^2 \cdot ^\circ C$
 h_o : Film coefficient of heat transfer based on
 the outside diameter of the tube, $W/m^2 \cdot ^\circ C$
 JISICO : Jordan Iron and Steel Industries Company
 K1 : Air compressor
 L : Tube length, m
 LMTD : logarithmic mean temperature difference, $^\circ C$
 \dot{m} : Mass flow rate, kg/s
 MER : Maximum Energy Recovery (design)
 O_2 : Oxygen
 Pr : Prandtl number
 Q : Heat flow rate, kW
 Re : Reynolds number
 T : temperature, $^\circ C$
 T1 : Air temperature before preliminary heat
 exchanger, $^\circ C$
 T2 : Air temperature after preliminary heat
 exchanger, $^\circ C$
 T3 : Air temperature after air purifier, $^\circ C$
 T4 : Nitrogen temperature after heat exchanger

A4, °C

- T5 : Nitrogen temperature after preliminary heat exchanger A3, °C
- T9 : Air temperature before turbo-expander, °C
- T10 : Air temperature after turbo-expander, °C
- TA1 : Turbo-expander
- T_s : Supply temperature of a stream, °C
- T_t : Target temperature of a stream, °C
- U : Overall coefficient of heat transfer, $W/m^2 \cdot ^\circ C$
- UA : The "UA" product of U times A, $W/^\circ C$
- v : Flow velocity, m/s
- ΔT : Temperature difference, °C
- ΔT_i : Temperature difference for stream i, °C
- ΔT_{min} : Minimum temperature difference, °C
- $\Delta \dot{H}$: Difference of enthalpy flow rate, kW
- μ : Kinetic viscosity, Pa.s
- ρ : Density, kg/m^3

LIST OF TABLES

| <u>Table</u> | <u>Page</u> |
|--|-------------|
| 4.1 : Stream data | 62 |
| 4.2 : Temperature interval analysis | 65 |
| 5.1 : "UA" for actual design | 86 |
| 5.2 : "UA" for predicted flowsheet | 87 |
| 5.3 : "U" for actual design | 88 |
| 5.4 : Heat transfer area for the predicted design | 89 |
| 5.5 : Pr & Re numbers for air and oxygen | 93 |
| 5.6 : Cost elements for a new oxygen plant of type K-0.15 and the extra capacity with respect to 60% expansion | 100 |
| 5.7 : Cost of expanding the production capacity of the existing plant by 60% | 101 |
| 5.8 : Annual costs for the existing and expanded plants | 102 |
| 5.9 : Alternative - decision analysis | 104 |

LIST OF FIGURES

| <u>Figure</u> | <u>Page</u> |
|--|-------------|
| 1.1 : Schematic flow diagram of the oxygen plant of type K-0.15 | 5 |
| 3.1 : Simulating flowsheet of the oxygen plant | 52 |
| 3.2 : Scheme of equipment connection | 53 |
| 4.1 : Stream - equipment layout | 59 |
| 4.2 : Stream formation | 59 |
| 4.3 : Temperature - enthalpy diagram | 61 |
| 4.4 : Temperature interval analysis | 64 |
| 4.5 : Heat cascading | 67 |
| 4.6 : Stream enthalpy | 69 |
| 4.7 : Stream matches | 71 |
| 4.8 : Final configuration | 72 |
| 4.9 : Matches 1 and 2/first stage | 74 |
| 4.10: Matches 1 and 2/second stage | 75 |
| 4.11: Match 4 | 77 |
| 4.12 : Optimized exchanger - network of the oxygen plant | 80 |
| 4.13 : Tray - sizing of the air rectification columns | 81 |
| 5.1 : Tube-in-tube section | 91 |

INTRODUCTION

1.1 Problem Statement

In 1988-89, Jordan Iron and Steel Industries Company (JISICO) has installed and commissioned a new imported oxygen plant at its factories in Zerka. The installation and commissioning were done under the supervision of the manufacturer.

During his work as plant engineer at JISICO, the author tried to investigate the plant circuit and its operating conditions. During this investigation, the following questions were raised

- Do the operating conditions set by the manufacturer lead to the optimum performance of the plant ?
- Is it possible to increase the production capacity of the plant without replacing any parts of the plant? If so, what will be the individual contribution of each component to this increase?
- Is there a bottleneck in implementing such an

increase ? If yes, how is it possible to get through this bottleneck ?

- Is it possible to increase the plant capacity by changing the present configuration of the process streams and/ or the operating conditions of the plant only ?

These questions are the basis of the present research. In this thesis, answers to the questions listed above are presented.

The following section is a brief description of both the circuit and components of the oxygen plant under consideration.

1.2 Oxygen Plant

1.2.1 Application

The plant under consideration is of type K-0.15⁽¹⁾ and is designed to produce gaseous oxygen of grade 1 according to the USSR standard ГOCT 5583-78. The plant is manufactured in versions intended for operation in temperate and tropical climatic regions; It displays stable operation in the ambient temperature range of -40 to 40°C.

The oxygen produced by this plant is intended for use mainly in machine building and metal working - welding and

flame cutting of metals -as well as in chemical industry and other fields of technology.

The plant can also be used to produce technical gaseous oxygen of higher purity (99.9%) according to the standard ГOCT 5583-78 or technical liquid oxygen of grade 1 according to the standard ГOCT 6631-78 or liquid nitrogen of grade 2 according to the standard ГOCT 9293-74.

1.2.2 Circuit arrangement and operating principle

a. General information

Air is precooled in the preliminary heat exchanger. Water vapor, hydrocarbon products and carbon dioxide are removed from air by the zeolite air purifier. The refrigeration losses are compensated by the medium pressure refrigeration process employing the turboexpander. Refrigeration is recuperated in a tubular heat exchanger. The air is separated into oxygen and nitrogen by a two-column rectification system.

b. Modes of operation

The plant has the following four modes of operation :

Mode i : Making grade 1 gaseous oxygen

After passing through a dust filter, air is compressed by

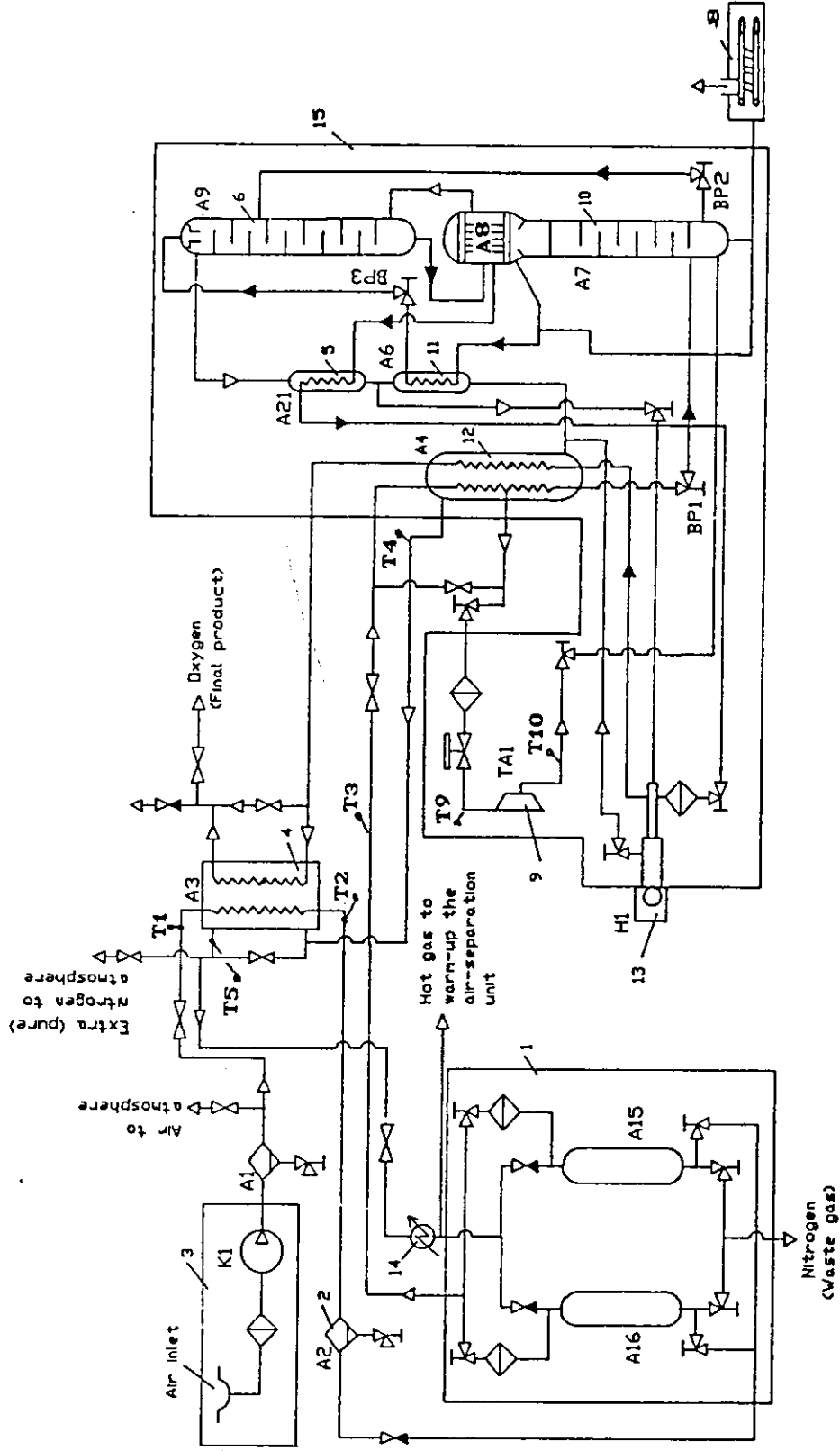


Figure 1.1 : Schematic flow diagram of the oxygen plant type K-015

- 1-Air purifier, 2-Moisture separator, 3-Air compressor, 4-Preliminary heat-exchanger, 5-Two-way sub-cooler,
- 6-Upper column, 7-Plate-fin condenser, 8-Emergency oxygen-evaporator, 9-Turbo-expander, 10-Lower column,
- 11-Three-way sub-cooler, 12-Heat exchanger, 13-Liquid-oxygen pump, 14-Electric heater, 15-Casing of the air-separation unit

In the lower column, air is separated into oxygen-rich (33.5%) liquid and nitrogen reflux containing 2.0-2.5% oxygen.

The still liquid in the amount of 60% of the processed air is throttled to a pressure of 0.04 MPa by valve BP2 and passed to the 40th plate of the upper column A9 (if counting from bottom to top).

The nitrogen reflux in the amount of 40% of the processed air is passed to subcooler A6 in which it is cooled by the gaseous nitrogen leaving the upper column. Then the nitrogen reflux is throttled by valve BP3 and passed to the top plate of the upper column.

In the upper column, air is finally separated into gaseous nitrogen and liquid oxygen.

Liquid oxygen is withdrawn from the still of the upper column to condenser-evaporator A8. Liquid oxygen in the amount of 19% of the processed air is passed from the condenser-evaporator to subcooler A21. On passing through the subcooler, liquid oxygen is used for cooling the jacket of the liquid oxygen pump H1 whereupon it is passed to the suction side of this pump. Liquid oxygen is pumped at any required pressure within the range of 0 to 20 MPa and directed to the heat exchanger A4 in which it is evaporated and passed to the preliminary heat exchanger. Gaseous oxygen

from the preliminary heat exchanger is passed to a filling manifold.

Gaseous nitrogen in the amount of 80% of the processed air is passed from the upper column to subcooler A6 and then to heat exchanger A4 in which it is heated to temperature T4. Thereafter it is directed to preliminary heat exchanger A3 and heated to temperature T5. Part of the gaseous nitrogen is passed to the air purifier for regeneration of the zeolite and cooling the absorbers. The remaining gas is released to the atmosphere.

Mode ii : Making high purity gaseous oxygen

When the plant is operated in mode ii, higher purity gaseous oxygen is produced by reducing the rate of product withdrawal (decreasing the pump delivery.)

Mode iii : Making grade 1 liquid oxygen

When the plant is operated in this mode, liquid oxygen is withdrawn and transferred to a storage tank. In this case the liquid oxygen pump is kept inoperative. The air pressure at the compressor exit is increased to 6.4 MPa.

Mode iv : Making liquid nitrogen

When the plant is operated in this mode, a part of the sub-cooled nitrogen reflux is withdrawn as product. In this

case the pressure after the compressor is raised up to 6.4 MPa. The liquid oxygen pump is kept inoperative.

1.2.3 Technical data

The nominal production capacity of the plant is $170 \text{ m}^3/\text{hr}$ of 99.7% pure gaseous oxygen at 10°C and 15 MPa. This capacity is restricted to the following conditions

- Delivery of the air compressor employed in the plant complies with the technical specifications in its certificate and its negative tolerance does not exceed 5%.
- Suction conditions conform with ГОСТ 2939-63, whereby the pressure equals 101,325 Pa (760 mm Hg), and the temperature equals 293.15 K (20°C).
- Temperature of the cooling water delivered to the compressor is 283.15 K (10°C).
- Purging losses of air do not exceed 3% .

The plant will normally operate with the volumetric flow rate of the air supplied for separation ranging from $750 \text{ m}^3/\text{hr}$ to $1056 \text{ m}^3/\text{hr}$.

1.2.4 Equipment list

- (a) Air separation unit KK 0216.00.000 (15)
- (b) Turboexpander AT-0.6/4 (9)
- (c) Air purifier KK 0926.000 (1)
- (d) Set of testing instruments and devices KK 0036.10.000
- (e) Preliminary heat exchanger KK 3283.000 (A3)
- (f) Air compressor 305 БП 16/70 (K1)
- (g) Two moisture separators KK 5013.000 (A15,A16)

The complete list also incorporates valves which are installed on the pipelines interconnecting units of the plant, as well as instruments for measuring purity of the product and a set of spare parts, service tools and accessories.

1.2.5 Individual description of equipment

* Separation unit

The separation unit is designed for cooling, liquefying and separating compressed atmospheric air into oxygen and nitrogen. A medium pressure cycle employing a turboexpander is used for cooling the air. Oxygen and nitrogen are produced from air by double-column rectification.

The separation unit consists of a housing, apparatus for

392091

separating air into oxygen and nitrogen (high- and low-pressure rectifying columns, condenser-evaporator), heat exchanger, liquid oxygen subcooler and subcooler of still liquid and nitrogen reflux, turboexpander, liquid-oxygen pump, valve equipment and instruments.

All the apparatus of the separation unit are accommodated in the housing. This housing is filled with a heat insulating material (expanded perlite powder), which reduces refrigeration losses to environment.

* Heat exchanger, A4

The heat exchanger is designed for cooling the air coming into the separation unit by the outgoing nitrogen and by compressed oxygen.

It is a three-stream wound tube-in-tube type apparatus. Air is the hot stream while oxygen and nitrogen are the cold streams. The number of wound tube layers is 8, and the number of tubes is 19. The outer tubes are of 10x1 mm diameter while the inner tubes are of 5x1 mm diameter.

* The outside diameter of the tube equals 10 mm while its thickness equals 1 mm. This convention of tube diameter is adopted all through this thesis.

The apparatus weighs 274 kg. The working pressure in 5x1 mm diameter tubes is 20 MPa. These tubes are subjected to a test pressure of 25 MPa.

The working pressure in 10x1 mm diameter tubes is 7.0 MPa. These tubes are subjected to a test pressure of 9.0 MPa. The working pressure in the space between tubes is 0.07 MPa.

The operating temperature is from $+10^{\circ}\text{C}$ to -176°C . The external heat exchange surface of 10x1 mm diameter air tubes is 9.16 m^2 . The external exchange heat surface of 5x1 mm diameter oxygen tubes is 4.58 m^2 .

The operating temperature is from $+10^{\circ}\text{C}$ to -176°C . The external heat exchange surface of 10x1 mm diameter air tubes is 9.16 m^2 . The external exchange heat surface of 5x1 mm diameter oxygen tubes is 4.58 m^2 .

When the exchanger is in operation, the high pressure oxygen is passed through the 5x1 mm diameter tubes; the air to be cooled is passed through the annular space inside the 10x1 mm diameter tubes while the cooling nitrogen flows through the space between the tubes.

The hydraulic resistance in the inter-tubular space as determined by testing at 20°C is as follows :

- in the upper zone it is of 330 80 mm H₂O,
- in the lower zone it is of 30 10 mm H₂O,

The air flow rate during testing is 400 m³/hr.

* Preliminary heat-exchanger, A3

The preliminary heat-exchanger is intended for cooling the air before it enters the purifier. It is a coiled-tube three -stream apparatus with parallel wound coils of air and oxygen tubes. The coils are wound in eight layers. The air tubes are 8x1 mm in diameter and 16 in number. The oxygen tubes are 8x1.5 mm in diameter and 3 in number.

The working pressure in the air tubes amounts to 7.0 MPa. The tubes are subjected to a test pressure of 9 MPa. The working pressure in the oxygen tubes amounts to 20 MPa. The tubes are subjected to a test pressure of 25 MPa.

The working pressure in the space between the tubes and casing amounts to 0.07 MPa.

Technical characteristics of the preliminary heat exchanger intended for use in temperate conditions are as follows :

- The mass of the apparatus is 311 kg.
- The height of the tube winding is 293 mm.
- The height of the apparatus is 1605 mm.

- The outside heat exchange surface of :

- Air tubes is 7.1 m² and,
- Oxygen tubes is 1.4 m²

When the apparatus is in operation, air to be cooled is passed through 8x1 mm diameter tubes and high pressure oxygen is passed through the 8x1.5 mm diameter tubes while gaseous nitrogen flows through the space between the tubes.

The hydraulic resistance in the inter-tubular space as determined at 20°C is 390 90 mm H₂O at air flow rate of 700 m³/hr.

* Sub-cooler, A21

This sub-cooler is designed for subcooling oxygen by means of still liquid.

The sub-cooler is a coiled tube two-stream apparatus with 4 tubes coiled in 2 layers. The apparatus weighs 12.0 kg. The working pressure in the tubes is 0.07 MPa. The tubes are subjected to a test pressure of 0.2 MPa. The working pressure in the space between the tubes is 0.2 MPa. The test pressure applied in the space is 0.3 MPa.

The design temperature is within -186oC to -188oC. The

outside heat exchange surface of the 8x0.8 mm diameter tubes amounts to 0.41^2 m.

When the sub-cooler in operation, liquid oxygen is passed through the tubes while the still liquid flows through the space between the tubes.

*** Sub-cooler, A6**

This sub-cooler is designed for sub-cooling the still liquid and nitrogen reflux by the outgoing nitrogen. It is a coiled tube three-stream heat exchanger with two bundles of 8x0.8 mm diameter tubes which are parallel-coiled in four layers.

There are 8 tubes in each section of the apparatus (in still liquid section and nitrogen reflux section). The outside heat exchange surface area of the still liquid tubes is 0.85 m^2 , while the outside heat exchange surface area of the nitrogen reflux tubes is 2.12 m^2 .

The apparatus weighs 55 kg. The working pressure in the tubes with still liquid is 0.6 MPa, while the test pressure is 0.9 MPa. The working pressure in the tubes with nitrogen reflux is 0.6 MPa and the test pressure applied to these tubes is 0.9 MPa. The working pressure in the space between the tubes is 0.07 MPa while the test pressure is 0.2 MPa.

* Lower column, A7

The lower column is designed for the separation of air into oxygen-rich liquid, nitrogen reflux, and gaseous nitrogen.

The column is a cylindrical vessel accommodating 20 circular perforated plates. These plates are secured in special creases on the column casing by means of rolling them in.

- Working pressure = 6 MPa.
- Testing pressure = 9 MPa.
- Operational temperature = 93 K.
- Column capacity = 200 liter.
- Mass of column = 75 kg.
- Plate diameter = 0.4 m.

The column complies with the standards for construction and safe operation of high pressure vessels.

* Upper column, A9

The upper column is designed for the final separation of air into gaseous nitrogen and liquid oxygen.

The column is a cylindrical vessel accommodating 56

circular rectifying sieve plates which are fixed in special creases on the column casing by means of rolling them in. Installed in the column still a plate-fin condenser (called "packet" hereinafter).

| | |
|------------------------------|-----------|
| - Working pressure in column | 0.07 MPa |
| - Testing pressure | 0.14 MPa |
| - Operational temperature | 80 K |
| - Column capacity | 900 liter |
| - Mass of column with packet | 300 kg |
| - Plate diameter | 0.5 m. |

*** Packet (plate-fin condenser), A8**

The packet is built into the upper column still and is designed for condensing nitrogen incoming from the lower column owing to the oxygen boiling.

The packet consists of a number of 1 mm thick identical flat spacer plates silumin-coated on both sides, which are inter-laid with corrugated aluminum-foil packing of 0.2 mm thick (working portion) and 0.7 mm thick (distribution portion).

On the opposite ends of the spacer plates are lateral packing bars made of aluminum section. At top and bottom the packet is fitted with 4-mm thick cover plates coated inside

with silumin. The spacer and cover plates are made of an aluminum alloy, as well as the aluminum packing foil.

The channels of nitrogen are communicated by means of headers. The oxygen space channels are at the end faces of the packet so that oxygen passes through the packet from top to bottom.

| | |
|--------------------------------------|----------|
| - Working pressure in nitrogen space | 0.6 MPa |
| - Testing pressure in nitrogen space | 0.9 MPa |
| - Working pressure in oxygen space | 0.07 MPa |
| - Testing pressure in oxygen space | 2.0 MPa |
| - Operational temperature | 77 K |
| - Number of nitrogen space channels | 16 |
| - Number of oxygen space channels | 17 |
| - Mass of packet | 76 kg |

* Moisture separator, A1 & A2

The moisture separator is designed for removing moisture droplets from air before the preliminary heat exchanger and before the air purifier inlets.

The water separator is a welded cylindrical vessel into which the air flow is directed tangentially.

The capacity of the apparatus is 16 liters and it weighs

40 kg.

The working pressure in the separator amounts to 7.0 MPa while test pressure applied to the apparatus is 8.8 MPa.

When the apparatus is in operation, moisture is separated from the air due to the sharp change in the velocity and direction of the air flow.

*** Liquid-oxygen pump, H1**

The pump used is one of the Russian pump series 2HCF. These pumps are designed for use in air separation plants or gasifiers to transfer super-cooled or compressed liquefied oxygen, nitrogen or argon.

- Mean delivery per charging cycle at a piston stroke of 30 mm, m^3/s (l/h) $(7.0 - 0.7) * 10^{-5}$
(252 \pm 25)
- Delivery control range, % $(100 - 40) \pm 10$
- Mean discharge pressure per cycle, MPa 14.7
- Maximum discharge pressure, MPa 22.5 - 1.2
- Maximum power (at maximum delivery), kW 4.4

*** Turboexpander, TA1**

The expansion turbine type AT-0.6/4 incorporated in the air separation plant is designed for expansion cooling of

compressed air in a low-temperature refrigeration cycle. The air to be expanded must be free from mechanical admixtures and carbon dioxide.

| | | |
|--|-------|-------------------------------|
| - Refrigerating capacity, W | | 6400 |
| - Inlet air pressure, MPa : | | |
| Working | | 3.96 ± 0.49 |
| Maximum | | 6.28 |
| - Air-handling capacity, kg/hr | | 600^{+60}_{-30} |
| - Outlet air pressure, MPa, | | 0.59 |
| - Inlet air temperature, K ($^{\circ}\text{C}$) | | 173 ± 5 (-100 ± 5) |
| - Outlet air temperature, K ($^{\circ}\text{C}$) | | 120 (-153) |
| - Rotor speed, thousands of rpm | | 150^{+25}_{-15} |
| - Cooling water consumption, kg/hr | | 3 |
| - Cooling water pressure, MPa, | | 0.196 |

*** Air purifier, A15 & A16**

The air purifier is intended for removal of moisture, carbon dioxide and any other hydrocarbon from air to be distilled. It is designed to operate at the medium pressures (3.5 - 7 MPa).

The purifier may be incorporated in an air separation plant or in air complex purification installation.

An electric heater is provided with the purifier. This heater is intended for warming regenerating gas. When the air purifier is incorporated in an air separation plant, The heater is also used for warming the air or nitrogen used for warming up the separation unit.

Technical Data

1. Air purifier capacity, m^3/s 0.227 - 0.267
2. Working pressure, MPa 3.5 - 7.0
3. Air temperature at
purifier inlet, K ($^{\circ}C$) 278 - 283
(5 - 10)
4. Content of CO_2 :
 - a) in purified gas, ppm 3 max.
 - b) at the end of adsorption
cycle, in 8 hours on comp-
letion of parallel operation, ppm ... 20 max.
5. Dehydration level, dew
point, K ($^{\circ}C$) 203 max.
(-70) max.
6. Length of adsorber working
cycle in air purification, with
parallel operation taken into
consideration, hr 9 max.
7. Length of desorption cycle, 2 hrs and
10 - 20 min.
8. Length of adsorber cooling cycle 4 hrs and
45 min. to 5 hrs

9. Duration of adsorbent operating cycle prior to replacement, ..:..... 2 years approx.
10. Temperature of regenerating gas after it is raised by electric heater, K ($^{\circ}\text{C}$) 673 (400)
11. Temperature of regenerating gas at the adsorber outlet by the end of regeneration cycle, K ($^{\circ}\text{C}$) 493 (220)
12. Regeneration flow rate, m^3/s :
- a) At a temperature of 0 to 5°C at the electric heater inlet 0.0472
- b) At a temperature of 35 to 45°C at the electric heater inlet 0.061 to 0.695
13. Electric heater consumed power, kW 30
14. Weight of zeolite used as adsorbent, particle size 4 mm, kg 460
15. Main dimensions of air purifier, m :
- a) Height 3.35
- b) Width 1.845
- c) Depth 2.05
16. Total weight of air purifier, kg 2565
- including weight of zeolite 460 ± 50

* Air compressor, K1

It is a stationary, reciprocating, direct action, four-stage, with perpendicular cylinders and with inter- and terminal coolers compressor.

Technical Data

1. Discharge pressure, MPa 7
2. Free; air delivery, m³/min 16 ± 5%
3. Power consumed, kW 190
4. Speed, rpm 500
5. Cooling water requirements
without terminal cooler with
entrance 15^oC, liter/min 110
6. Recommended cooling water
requirement for terminal
cooler with entrance temp-
arature 15^oC, liter/min 40
7. Number of cylinders 4
8. Cylinder bores, mm :
 - 1st stage 500
 - 2nd stage 270
 - 3rd stage 145
 - 4th stage 100
9. Piston stroke, mm 220
10. Stage outlet pressures, MPa :
 - 1st stage 0.22 - 0.28
 - 2nd stage 0.8 - 1.2
 - 3rd stage 2.2 - 2.85
 - 4th stage 7
11. Lubrication :
 - a) Crank mechanism circulation system with
gear pump
 - b) Cylinders central force - feed

from a lubrication unit
 incorporated with the
 compressor

12. Oil capacity of compressor
 frame, liter 136
13. Force - feed delivery rate, g/hr 70
14. Overall dimensions, mm :
- a) length 2,670
 - b) width 1,880
 - c) height 2,560
15. Mass, kg 4,400
16. Automatics protection and signaling
 for main compressor para-
 meters.
17. Drive synchronous motor,
 direct coupled.
18. Synchronous motor :
- a) Rated power ,kW 200
 - b) Speed, rpm 500
 - c) Voltage, V 380
 - d) Mass, kg 1,660

Chapter Two

LITERATURE SURVEY

Oxygen is the most abundant element on the earth's surface. It occurs both as the free element and combined in innumerable compounds: It comprises 23% of the atmosphere by weight, 46% of the lithosphere, and more than 85% of the hydrosphere (~ 85% of the oceans and 88.81% of pure water).

2.1 Oxygen Discovery

In the 15th century, *Leonardo da Vinci* noted that air has several constituents, one of which supports combustion.⁽²⁾

The discovery of oxygen, however, is generally credited to *C. W. Scheele* and *J. Priestley* independently in 1773-4, though several earlier investigators had made pertinent observations without actually isolating and characterizing the gas⁽³⁻⁵⁾. Indeed, it is difficult to ascribe a precise meaning to the word *discovery* when applied to a substance so ubiquitous present as oxygen; particularly when (a) experiments on combustion and respiration were interpreted in terms of the phlogiston theory, (b) there was no clear consensus on what constituted "an element", and (c) the birth of *Dalton's* atomic theory was still far in the future.

Moreover, the technical difficulties before the mid-eighteenth century of isolating and manipulating gases compounded the problem still further, and it seems certain that several investigators had previously prepared oxygen without actually collecting it or recognizing it as a constituent of "common air".

Scheele, a pharmacist in Uppsala, Sweden, prepared oxygen at various times between 1771-3 by heating KNO_3 , $\text{Mg}(\text{NO}_3)_2$, Ag_2CO_3 , HgO and a mixture of H_3AsO_4 and MnO_2 . He called the gas vitriol air and reported that it was colorless, odorless and tasteless, and supported combustion better than common air, but the results did not appear until 1777 because of his publisher's negligence.

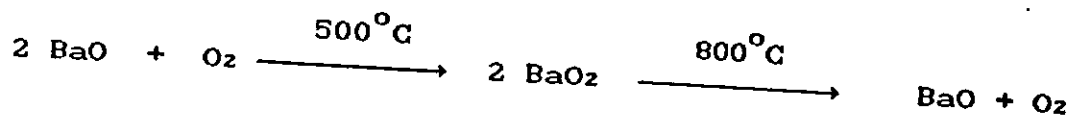
Priestley's classic experiment of using a "burning glass" to calcite HgO confined in a cylinder inverted over liquid mercury was first performed in Clone, England, on Monday, August 1, 1774; he related this to *A. L. Lavoisier* and others at a dinner party in Paris in October 1774 and published the results in 1775 after he had shown that the gas was different from nitrous oxide. *Priestley's* ingenious experiments undoubtedly established oxygen as a separate substance (dephlogisticated air) but it was *Lavoisier's* deep insight which recognizes the new gas as an element and as the key to our present understanding of the nature of combustion. This led to the overthrow of the phlogiston theory and laid the foundations of modern chemistry. *Lavoisier* named the

element "oxygène" in 1777 in the erroneous belief that it was an essential constituent of all acids (Greek $\acute{o}\xi\upsilon\gamma\eta$, oxys, sharp, sour; $\gamma\epsilon\iota\nu\mu\alpha\iota$, geinomai, I produce; i.e. acid forming).

H. Cavendish (1781) reported that water constituents of oxygen and hydrogen. The decomposition of water into its two constituents was first performed in 1800 by W. Nicholson and A. Carlisle through electrolysis.⁽⁷⁾

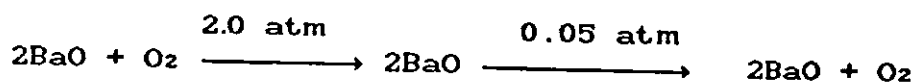
2.2 Old Production Techniques

Before the development of low-temperature distillation route oxygen was made by chemical methods. In the United Kingdom Brin's process was operated commercially from 1886 to 1906⁽⁷⁾. It depended on laboratory observations that barium oxide would react with atmospheric oxygen at about 500°C and that the peroxide so formed would decompose if the temperature was raised to about 800°C ,



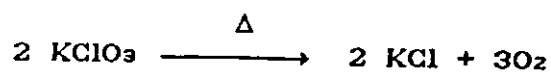
In commercial practice it was found that the barium oxide lost its power to react after a few cycles unless the incoming air was first freed from carbon dioxide, organic

matter and dust.⁽⁷⁾ It was also found that, instead of the expensive and time-consuming practice of raising and lowering the temperature by 300°C, the process could be operated at about 600°C using two different pressures :



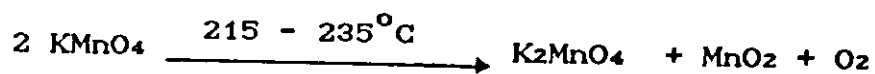
The gas produced by this process was impure by modern standards, usually containing 90-96% oxygen together with nitrogen and smaller amounts of argon and other gases. Occasionally, small-scale laboratory preparations of oxygen are required and the method chosen depends on the amount and purity required and the availability of services. Electrolysis of degassed aqueous electrolytes produces wet O₂, the purest gas being obtained from 30% potassium hydroxide solution using nickel electrodes. Another source is the catalytic decomposition of 30% aqueous hydrogen peroxide on a platinized nickel foil.

Many oxoacid salts decompose to give oxygen when heated. A convenient source is KClO₃ which releases oxygen when heated to 400-500°C according to the simplified equation⁽²⁾,



The decomposition is reduced to 150°C in the presence of

MnO₂ but then the product is contaminated with up to 3% of ClO₂. Small amounts of breathable oxygen for use in emergencies (e.g. failure of normal supply in aircraft or submarines) can be generated by decomposition of NaClO₃ in "Oxygen candles". The best method for the controlled preparation of very pure oxygen is the thermal decomposition of recrystallized pre-dried, degassed KMnO₄ in a vacuum line. Mn^(VI) and Mn^(IV) are both formed and the reaction can be formally represented as⁽²⁾,



Where electric power is exceptionally cheap, oxygen may be manufactured by the electrolysis of water, but the amount made by this process constitutes a very small percentage of total production in USA and Canada⁽⁸⁾.

By far, the most important method of manufacturing oxygen is by means of fractional distillation after the liquefaction of air. Liquid air is essentially a mixture of approximately one-fifth oxygen and four-fifths nitrogen. Nitrogen, having a lower boiling point, is allowed to escape, leaving oxygen in the liquid form, which may then be purified.

2.3 Gas Liquefaction

Air-separation plants are built for a wide variety of outputs: To produce one or more of the products in liquid form; and to make products of various purities. The precise practical method employed depends to some extent on the definition of these requirements.

An air-separation plant, however, always has three basic stages, namely purification, liquefaction and distillation. The other processes of prime importance is that of heat transfer, so as to keep losses of coldness to minimum. Among these four processes, liquefaction of a gas presented a serious challenge which was the first article in establishing the gases industry.

Michael Faraday (1845) was able to liquefy many gases for the first time, including ammonia, chlorine, sulphur dioxide and hydrogen sulfide⁽⁷⁾. He generated his gas in one arm of a sealed tube shaped like an inverted V and immersed the other arm in an appropriate cooling mixture, so that a combination of high pressure and low temperature was achieved in one piece of equipment.

Despite the efforts of other workers who used still high pressure there remained a number of gases which could not be converted to liquid form and these became known as "permanent gases". It was only when the concept of critical temperature

was developed following Andrew's work on carbon dioxide in 1869 that the liquefaction of permanent gas became possible.⁽⁶⁾ The critical temperature is defined as that temperature above which it is impossible to liquefy a gas however great the applied pressure. It should be noted that the critical pressure is the pressure required to liquefy the gas at its critical temperature. At lower temperatures a lower pressure suffices.

Oxygen was first liquefied in 1877 by two workers quite independently using quite different methods.⁽⁷⁾

Cailletet (France) cooled oxygen to -29°C by bath of evaporating sulphur dioxide, compressed to a pressure of 200 atm and released the pressure suddenly. A mist of liquid oxygen was seen. He observed the same phenomenon when using carbon monoxide, acetylene and nitrous oxide but not with hydrogen.

Pictet (Switzerland) used a method now known as the "cascade method" which involves proceeding to lower and lower temperatures in a series of stages using different coolants. Thus he liquefied oxygen compressed to 320 atm by cooling it in liquid carbon dioxide at 140°C . The latter had in its turn been obtained by cooling in sulphur dioxide

Wroblewski and *Olszewski* in the period 1880-90 were the first to obtain relatively large quantities of liquid oxygen.

They employed a cascade method sometimes combined with gas expansion.⁽⁷⁾

Another feature of work with liquefied gases is the difficulty of keeping any product obtained. The influx of heat from the surroundings posed serious problems for the workers in this field. The major advance was made by *Dewar* (1892) when he invented a vacuum flask to store liquefied gases originally designed by *d'Arsonval* in 1887.⁽⁷⁾

Production of oxygen on an industrial scale was pioneered by *Linde company* (1900) who built an air liquefier using ammonia for precooling⁽⁹⁾. Further development have been carried out by the same company in 1902 and 1907 when they erected the single and double-stage air separation column, respectively.

Other companies, *Claude*, *Heylandt* and *Messer*^(9&10) became involved in the air liquefaction and separation of air constituents since 1902.

The first commercial plants for oxygen production by the low temperature distillation method were started up almost simultaneously in England, Germany and France (1912) based on technical developments by *Hampson*, *Von Linde* and *Claude* respectively.⁽⁹⁾

Further improvements to the air liquefaction plants were

added by Linde Co. (1926) who in 1932 introduced expansion turbines for the first time in air separation plants⁽¹⁰⁾.

Kapitsa (1937-39) built a high efficiency expansion turbine permitting air separation on the basis of a low pressure cycle alone. Kapitsa's low-pressure cycle is the basis of all existing tonnage air separation plants.

Continued increase in efficiency and capacity resulted in plants capacities of 70,000 cubic meter per hour in the seventies⁽⁹⁾. In 1985, the world production of liquid oxygen to half million tons with a purity of around 99.5%⁽¹¹⁾

2.4 Heat Exchanger Network Optimization

In the oxygen plant under question, the liquefaction duty is actually performed through network of heat exchangers. Any possible optimizing of this network will support an optimum final design of the plant. Due to the rising costs of energy, the design of an optimal heat exchanger network between hot and cold process streams becomes an important problem. A heat exchanger network is defined as several heat exchangers arranged in series and/or parallel to affect the heat exchange between several hot and cold streams. The target was always to minimize the total area required for heat exchange using a thermodynamic approach. Other economic factors were not taken into consideration.

Early optimization work on heat exchanger networks was reviewed by Hendry *et al.*⁽¹²⁾ and Raghavan⁽¹³⁾. Some of the early authors used heuristic approaches for stream matching which do not guarantee optimality. A practical method of evaluating the heat exchange among multiple streams in parallel and in series was developed by Chato *et al.*⁽¹⁴⁾. This can be used most effectively in the final design stage of a heat exchanger network. Lee *et al.*⁽¹⁵⁾ used a mathematical approach based on a branch and bound method to synthesize networks and find the optimum. This procedure requires too much time for large-scale problems.

Nishida *et al.*⁽¹⁶⁾ used an algorithm which they claimed give the least total heat transfer area and, by using a few heuristic rules, reduced it to a final form. Raghavan argued that this method did not guarantee optimality and proposed a Heat Availability Function (HAF) with which the maximum recoverable energy could be computed. An algorithm to determine an optimal network was also presented. In 1978, Linnhoff and Flower⁽¹⁷⁾ presented a method similar to that presented by Raghavan in that they proposed a method which first generated preliminary networks which gave maximum heat recovery and then a final network was evolved using the preliminary networks as starting points. Malhotra *et al.*⁽¹⁸⁾ used the Discrete Maximum Principle to minimize the total cost of heat exchanger chains in which one cold stream was heated by several hot auxiliary streams. In an extension to this work, Siddique *et al.*⁽¹⁹⁾ considered the optimization of

a heat exchanger train (as a network sometimes called) in which one cold stream to be heated by several hot streams using the same procedure as in their earlier work. Recently, *Siddique et al.*⁽²⁰⁾ extended their earlier work to include two cold streams. This method can only be applied to small-scale problems and is thus restrictive.

Parkinson et al.⁽²¹⁾ considered the optimal design of resilient heat exchanger networks. A resilient network is defined as one which can tolerate fluctuations in stream temperatures and flow rates. They presented an algorithm which synthesized networks resilient for all stream fluctuations and minimized network investment costs for the conditions of maximum energy recoverable. In an extension of their earlier work, *Parkinson et al.*⁽²²⁾ also solved the problem of resilient heat exchanger networks optimization using Monte Carlo simulation.

Hesselmann⁽²³⁾ presented an approach which incorporated the economic aspect of heat exchanger design. A functional relation between minimum investment costs and energy losses was determined and, by plotting the investment costs against energy losses, an optimal network could be determined.

The above approaches to the problem of heat exchanger network optimization rely on large computer algorithms and are time consuming. A hand application technique has been used by *Linnhoff and Turner*⁽²⁴⁾ and *Hindmarsh et al.*⁽²⁵⁾ to

optimize various process systems, including heat exchanger (or heat-recovery) systems. In 1986, Chato et al.⁽²⁰⁾ presented a simpler method based on the second law of thermodynamics, using the load curves for a particular problem. The method can be easily performed on a graph.

In this literature survey, the ideas and sometimes the expressions of the cited papers were used.

Chapter Three

METHOD OF ANALYSIS

It has been understood that oxygen production is compromised of four processes: compression, heat removal, liquefaction, and rectification of air. For these processes to be evaluated and analyzed, a large set of thermodynamic calculations are needed. The multiple parameters of plant circuit (like flow rate, pressure, temperature, product purity, product state, etc.) make it more complicated.

To perform necessary calculations for the plant parameters when operating under steady state, it has been thought of a computer program which is able to simulate the actual design of the plant as close as possible. Through the plant simulation program, a large set of runs could be performed in order to evaluate the circuit parameters under a set conditions of operation.

To get the required program, two options exist. The first one is to construct an independent, specific and comprehensive program which should meet all details given by the plant design. Although it is direct and attractive, this option calls for a tedious and complicated work because of the wide variety of processes and equipment. Even, the resulting program will still satisfy only the plant under

question , which in turn seems a simple gain when compared with the efforts behind.

The second option suggests to search for a program among several of them available in the market.; Fortunately, the Faculty of Engineering and Technology at the University of Jordan possesses and provide a quality computer software.

Finally, after the investigation of different technical softwares available at the faculty, a computer simulating program referred to as COMPUTER CODE has been chosen to perform the simulation of the oxygen plant. In the coming section, CODE is briefly described.

3.1 CODE Program

CODE is a steady state process simulator that calculates heat and material balances around process equipment. It is able to

1. prepare process design,
2. analyze design alternatives,
3. predict the effect of changes on plant operating conditions,
4. optimize energy consumption and
5. eliminate bottlenecks and increase throughput.

CODE contains a database with physical properties of 427 pure substances. The user can also create his own database containing other components by supplying the required physical properties.

Flowsheets containing up to 100 streams and 50 pieces of equipment can be simulated. With the aid of 16 built-in equipment modules, it is possible to model virtually all process plants. A brief description of each equipment module will follow.

3.1.1 CODE skills

These skills are listed in the CODE menu shown below.

| C O D E M E N U | |
|-----------------|---------------------------|
| A.> | Input/Edit Data File |
| B.> | Input Data Checking |
| C.> | CODE Flowsheet Simulation |
| D.> | Run Time Message |
| E.> | Report Generation |
| F.> | Pure Components Databank |
| G.> | HP Plotter Driver |
| H.> | Apple Laser Writer Driver |
| I.> | List Data Files |
| J.> | Type Files |
| K.> | Tray Sizing Input |
| L.> | Exit - Return to DOS |

This menu is the interface with different phases of the package.

A. Input/Edit Data File

This is the user interface with the system. With Option A

one can create new problems, review results of problems already run, or build case studies or make modifications of previously run problems.

B. Input Data Checking

Once a problem has been created or modified, this phase of system is used to check or detect input errors in the problem data.

C. CODE Flowsheet Simulation

This is the computational phase of the program. Phase C reads the problem data file, performs the calculations, and records the results in the problem data file.

D. Run Time Message

This program allows to review any screen messages or error messages which may have occurred during a problem run. Phase D should be run each time when the problem calculations are performed.

E. Report Generation

This phase reads the problem output file and generates a report containing the problem results.

F. Components Databank

This program accesses the physical properties in the pure component databank. It allows inspection of the databank and the addition of new components and pseudo components.

G. HP Plotter Driver

This program provides an interface to the Hewlett-Packard 7400 series plotters. This phase is used to generate a graphical hard copy of the flow sheet outputs.

H. Apple Laser Writer Driver

This program provides an interface to the Apple Laser Writer. It is used to generate graphical hard copy flow sheet outputs.

I. List of Data Files

This program will list all data files (files with .DAT extension) on the default directory.

J. Type Files

This program will print a file to the screen. This option can be used to type out various files, such as Data, Result, or Report files.

K. Column-Tray Sizing

This program allows to enter data for tray sizing. It must be executed before the Report program.

L. Exit - Return to DOS

This program allows users to leave CODE and return to DOS.

3.1.2 Run procedure

1. Through phase A a data file is created. By the graphics option within this phase a set of equipment modules are selected, laid down and then connected to each other according to the problem being dealt with. Both equipment and streams are automatically numbered. Necessary information are provided by using the spreadsheets option. Local menus are so helpful to indicate the required information either for equipment or streams. Of course, the user should begin with specifying the components handled by his process(es) and thermal options of solution.
2. Phase B is used to survey errors accompanying step # 1. If errors are assigned, phase A is recalled to correct them or their causes. When phase B shows a well refined data file, it becomes possible to move further to the next step.
3. Phase C is selected and the required data file is assigned. Calculations will be performed upon a number of loops depending on how far entered data can help accuracy.
4. Phase D is then loaded to display errors detected during performing the calculations.
5. Using phase E a report file is generated. There is a variety of report files : comprehensive, stream details only, equipment details only, both stream and equipment

details or what is referred to as the user report.

3.1.3 Equipment modules

The following list introduces the equipment modules available in CODE.

- ABSR : Absorber-stripper module using absorption and stripping factor method of Edmister.
- ADBF : Two-phase equilibrium flash module with a third product stream containing a free water phase in hydrocarbon systems.
-
- COLM : Comprehensive, rigorous multistage equilibrium routine using a modified simultaneous corrections algorithm. COLM can handle up to 300 stages and is relatively fast for problems with few components. It may be used for simulating absorbers, and fractionators.
- CTRL : Flow sheet controller with feed forward and feedback control.
- DISC : Short-cut distillation rating or design module. In the design mode, three options are available

for feed tray location. In the rating mode, the fractional recovery of the light key component is computed.

- DIST : Component splitter module.
- DVDR : Stream and component divider module. It divides one input stream into two to six streams with flow or proportional control and arbitrary component separation.
- ENTM : Isentropic compressor or expander for vapor or gas.
- EVLP : Phase envelope module which generates dew point, bubble point, and condensing curves.
- FHTR : Fired heater module controlling either output temperature or heat addition.
- HXER : Multi-pass heat exchanger module with ten modes. Change of phase is allowed and single- or two-stream cases can be used.
- MIXR : Rigorous mixing point module with flash equilibrium at the output.
- MMIX : Simple stream adder module. It should always be followed in the layout by an ADBF if thermal

conditions are important.

- PUMP : Liquid pump or multistage polytropic vapor compressor module.
- REAC : Simple stoichiometric reactor module with heat of reaction.
- TOWR : Fast, comprehensive , multistage equilibrium routine using a state-of-the-art "inside-out" algorithm. This module should be used instead of COLM to save run-time. TOWR is limited to 100 stages. It may be used for simulating absorbers, strippers, reboiled absorbers, and fractionators.
- VALV : Downstream pressure controller module.

The modules have been used in simulating the plant are : DVDR, ENTM, HXER, MIXR, PUMP, TOWR and VALV.

3.2 Plant Simulation

This section describes the simulation steps with reference to Figure 3.1.

Prior to the implementation of plant simulation the following assumptions have been established :

- a) The plant operates under steady-state conditions.
- b) Air is assumed to be a binary mixture of only nitrogen and oxygen with molar ratios of 81% and 19% , respectively. This means that other constituents of air (water vapor, carbon dioxide other hydrocarbons, argon, helium, etc.) were neglected based on their very small total contribution to an air sample when compared with that of the two major constituents (N_2 and O_2 .)
- c) Also, air is assumed to follow the laws of perfect gas when necessary for the simulating program.
- d) Refrigeration losses to ambient were neglected along the heat transfer blocks of the simulated layout.
- e) The whole quantity of air fed to the compressor is processed by all the rest of equipment; i.e. no purging losses are allowed.

Figure 3.2 shows the scheme of equipment connection.

- Air compressor

In the plant description, its operation has been reported to be normal with a volumetric flow rate of air supplied for separation ranging from $750 \text{ m}^3/\text{hr}$ to $1056 \text{ m}^3/\text{hr}$. A flow rate of 40 mol/hr ($961.62 \text{ m}^3/\text{hr}$ at 20°C and 1.0 atm) has been selected. Under temperature of 15.6°C and pressure of 1.0 atm , this is equivalent to $947.608 \text{ m}^3/\text{hr}$. Both values are in good agreement with the range specified before.

The four-staged, inter-cooled compressor is simulated using the two equipment modules ENTM and HXER.

The temperature increase of the compressed air due to deviation from isothermal compression has been limited to the final (fourth) stage of compression.

According to Figure 3.1, ENTM # 1 through ENTM # 4 stand for the respective four compression stages. Heat exchanger modules HXER # 5 through HXER # 7 simulate the respective three inter-coolers of the compressor, while HXER # 8 represents the terminal cooler.

In fact, the compression process could be simulated as a one-staged process without altering the final state of air at compressor delivery.

- Preliminary heat exchanger

Through this exchanger, air is precooled to its

purification temperature (10 - 12°C). Moisture separators have not been included in the analysis because moisture (water vapor) was not assumed as a constituent of air.

According to the operating principle of this exchanger, direct heat exchange only occurs between the hot stream (air) and one cold stream (nitrogen). The other cold stream (oxygen) is not allowed to exchange heat directly with air; its effect is to sustain the temperature of nitrogen as long as the heat transfer mechanism is valid.

Three units of equipment module HXER are connected to simulate the function of the preliminary heat exchanger.

- Air purifier

Following the assumption that air is a binary mixture of only nitrogen and oxygen, air purifier is automatically dropped off. The only effect produced by this equipment is the temperature rise of air across the purification process by 2°C. This effect is considered in the analysis. Equipment module HXER # 13 is used to provide the required temperature rise.

- Heat exchanger/upper half

For this exchanger, the part before the branching of air stream will be termed as upper half while that part after the branching will be termed as lower half.

Through the upper half of the heat exchanger air is to be cooled to the inlet temperature of the turboexpander.

Two units of equipment module HXER (HXER # 11 HXER # 12) are arranged to represent a three-stream heat exchanging unit. A divider module (DVDR # 14) precedes the formed unit to split the air stream into two streams. Splitting ratio complies with thermodynamic equilibrium which requires that air (as a single stream) has a unique temperature at any specified location of the heat exchanger.

- Heat exchanger/lower half

Through this section, part of the processed air (40%) is allowed to exchange heat with the two cold streams (N_2 and O_2). A divider module (DVDR # 17) precedes the exchanger section to partition the air stream. The rest of the air (60%) is directed to the turboexpander (ENTM # 18). A divider module (DVDR # 19) is again used to split the main hot stream in order to have the arrangement of three-stream heat-exchanging section.

Beyond this section of the heat exchanger, the outgoing hot stream is throttled by equipment module VALV # 23.

The outlet pressures of both turboexpander and throttling valve comply with the requirements of the separation unit

- Lower column

An equipment module, TOWER # 24, is used to simulate the lower column of the separation unit. The selected mode of operation guarantees the distillation fraction assigned by the manufacturer.

- Sub-cooler A21

This sub-cooler is also a three-stream equipment. Its function is to sub-cool each of the two streams (liquid nitrogen, liquid oxygen-riched air) leaving the lower column.

HXER # 25 and HXER # 26 are the simulating modules.

Across both outlet streams, two valve modules (VALV # 28 and VALV # 29) throttle the running streams to the pressure range required by the upper column follows.

- Sub-cooler A6

For sub-cooling the main product (liquid oxygen) emerging from the upper column by the incoming liquid oxygen-riched air, HXER # 27 exists to simulate the required sub-cooler.

- Upper column

A tower module (TOWER # 30) is used to represent the upper rectifying column. The selected operating mode guarantees the flow rate of the final product as assigned by the manufacturer.

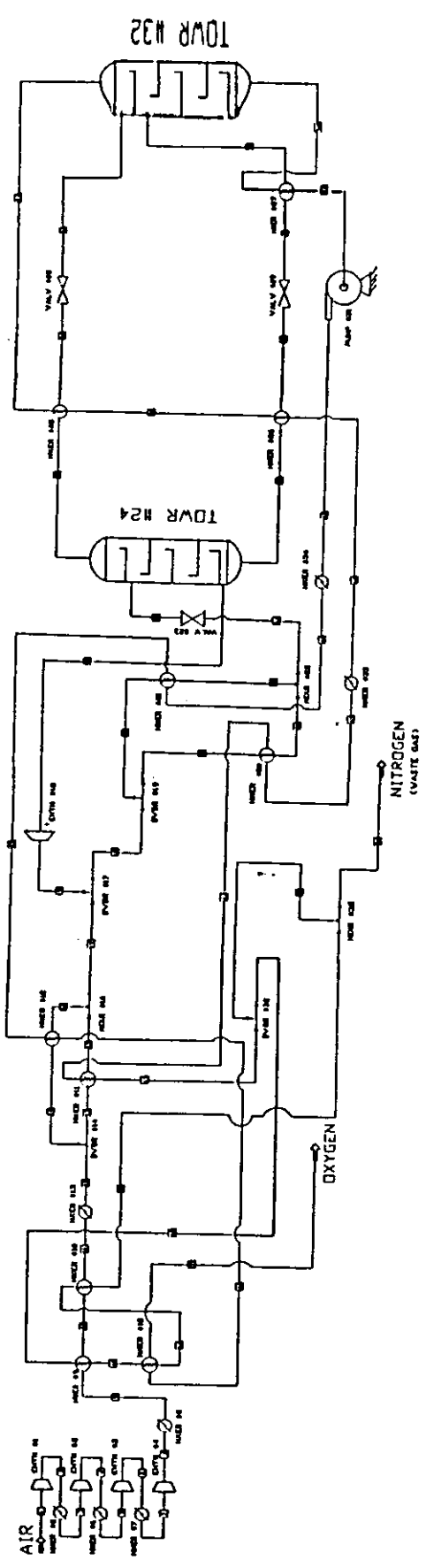
A pump module PUMP # 31 is used across the sub-cooled liquid oxygen stream for the latter to be compressed to the required handling pressure.

The two streams outgoing from the upper column (gaseous nitrogen and liquid oxygen) are the same cold streams encountered by the heat exchangers later.

HXER # 33 & HXER # 34 are being used as temperature controllers to isolate the liquefaction block (preliminary heat-exchanger, heat exchanger and turbo-expander) from temperature variations that may occur at the exit of the rectification block whenever some parameters of the latter are altered.

A divider module, DVDR # 32, is located across the nitrogen stream at the entrance to the preliminary heat-exchanger. This divider corresponds to an actual one in the plant layout design. Its function is to make part of the nitrogen stream bypass the preliminary heat-exchanger for the outlet temperature of the precooled air not to violate its assigned range (5 - 7°C).

Figure 3.1: Simulating Flowsheet of the oxygen plant of type K-015



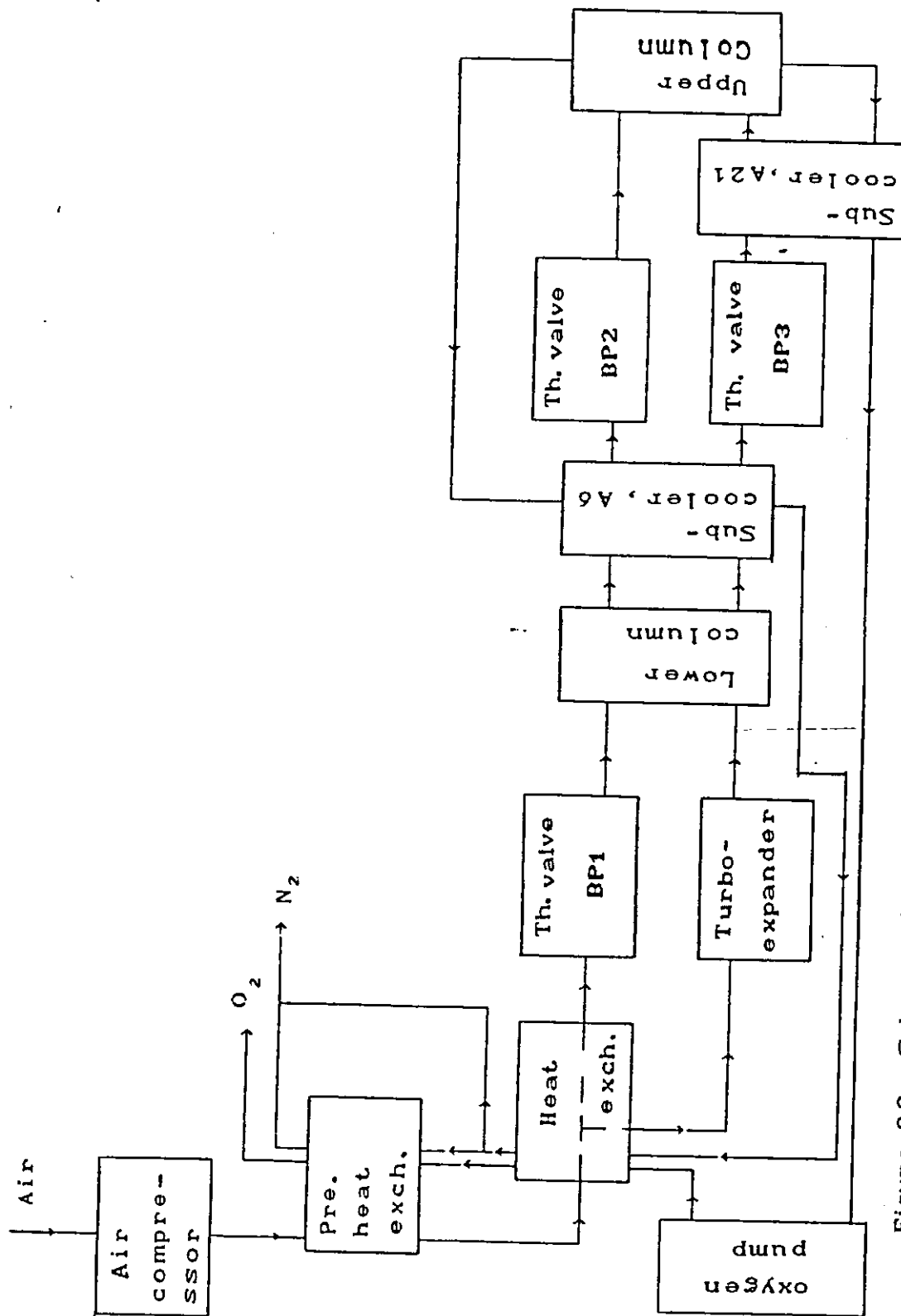


Figure 3.2 : Scheme of equipment connection

Chapter Four

INVESTIGATION OF THE EXISTING PLANT

4.1 Introduction

4.1.1 Optimum process design

Air-separation process may be considered as a series of unit operations. The various components are closely integrated by the process designer and optimized to suit the particular requirements and to suit available energy source(s).

The important factors which influence the selection of the process within the oxygen plant are

- energy consumption,
- product quantity,
- investment cost,
- product purity,
- product state (temperature, pressure, phase)
- continuity of product supply,
- plant flexibility,
- maintenance cost and
- permissible plant dimension.

These factors remain in continuous conflict when searching for an optimum design. The primary factor

determining the cost of the product is the energy cost.

As to our plant, energy is lost due to the following causes

- a) low efficiencies of energized equipment (compressor, pump, electric heater)
- b) heat in-leak to cold blocks due to the imperfect insulation.
- c) incomplete heat transfer resulting from imperfect heat exchanger network.

To improve the efficiencies of the compressor, the pump and the electric heater, it is necessary to increase the capital cost of the plant. Also, to improve the efficiency of the insulation, more expenditure is necessary. However, increasing the efficiency of the heat exchanger network does not necessarily require higher cost.

The plant circuit shows that heat is being exchanged across three locations within the plant. These locations are

1. compressor inter-coolers,
2. sub-coolers contained in the air-separation unit and
3. cooling and liquefaction block (preliminary heat exchanger, heat exchanger and turbo-expander).

A compressor inter-cooler is a water-cooled air cylinder.

Its effectiveness depends on inlet temperature of the cooling water which in turn is determined by the flow rate of water.

For the sub-coolers contained in the air-separation unit, the configuration of streams is controlled by the operation principle of the rectifying columns and so their efficient operation is an integrated part of an effective rectification block.

Since the circuit arrangement does not employ an independent refrigerating system for the liquefaction of air, the cooling and liquefaction block becomes of most importance to focus on. Within this block, expansion of air by the turbo-expander provides the necessary cooling effect. After the separation of air into liquid oxygen and gaseous nitrogen, a heat exchanger network is used to utilize the coolness within the separation products to cool the incoming air.

The following section is an energy integration analysis to investigate the present layout of the plant and to suggest improvements that may be necessary.

4.2 Energy Integration Analysis

4.2.1 Method of approach

The starting point for an energy integration analysis is

the calculation of the minimum heating and/or cooling requirements for a heat exchanger network. These calculations can be performed given the input and output streams without having to specify any heat exchanger network. Similarly, we can calculate the minimum number of heat exchangers required to obtain the minimum energy requirements without having to specify a network. Then the minimum energy requirements and the minimum number of heat exchangers provide targets for the subsequent design of heat exchanger network.

Two well-known approaches are available to estimate the minimum requirements of energy; they are

1. Composite Curves and
2. Problem Table.

In the first approach a single composite of all hot and a single composite of all cold streams are produced in the temperature-enthalpy (T-H) diagram, and handled just in the same way as a two-stream problem. This method will not be used because it would require graph paper and cut and paste approach (for sliding the graphs relative to one another) which would be messy and imprecise.

The second approach which has been published by Linnhoff and Flower (1978)⁽¹⁷⁾, is used for considering the energy

targets algebraically. This approach will be adopted because of its simplicity and applicability to computer handling.

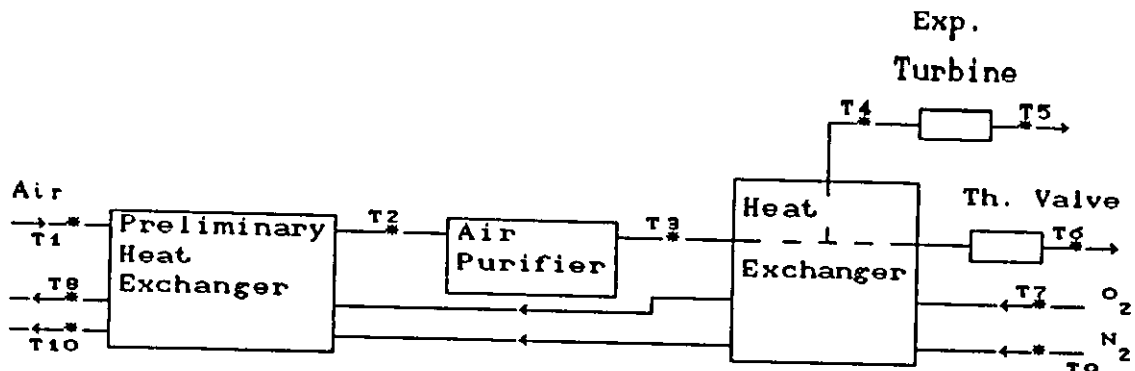
4.2.2. Stream definition

Figure 4.1 shows the connection scheme within the stream-equipment layout of the cooling and liquefaction block in the plant. Also, design-temperature ranges at the equipment boundaries are shown.

Figure 4.2 illustrates the formation of streams according to which the coming analysis is based.

Considering the fluid type, three streams are formulated, they are air, oxygen and nitrogen. The first one is hot stream while the other two are cold streams. Physically, the hot stream, H, is splitted into two parts at the middle of the heat exchanger, A4. The first part, H2, moves through the turboexpander while the other part, H3, is throttled by valve BP1.

The oxygen stream conserves itself as one cold stream, C1. The nitrogen stream, C2, is divided into two parts. The first part travels through the preliminary heat exchanger. The second part bypasses the exchanger such that the outlet temperature of incoming air is controlled. The latter part is excluded from the formed streams. The part which goes through the exchanger is chosen to be the third cold stream,



T_1 : (15 to 40 °C), T_2 : (5 to 10 °C), T_3 : (7 to 12 °C)
 T_4 : (-130 to -115 °C), T_5 : (-173 to -168 °C), T_6 : (not specified)
 T_7 : (-183 to -180 °C), T_8 : (10 to 35 °C), T_9 : (-175 to -173 °C)

Figure 4.1 : stream-equipment layout

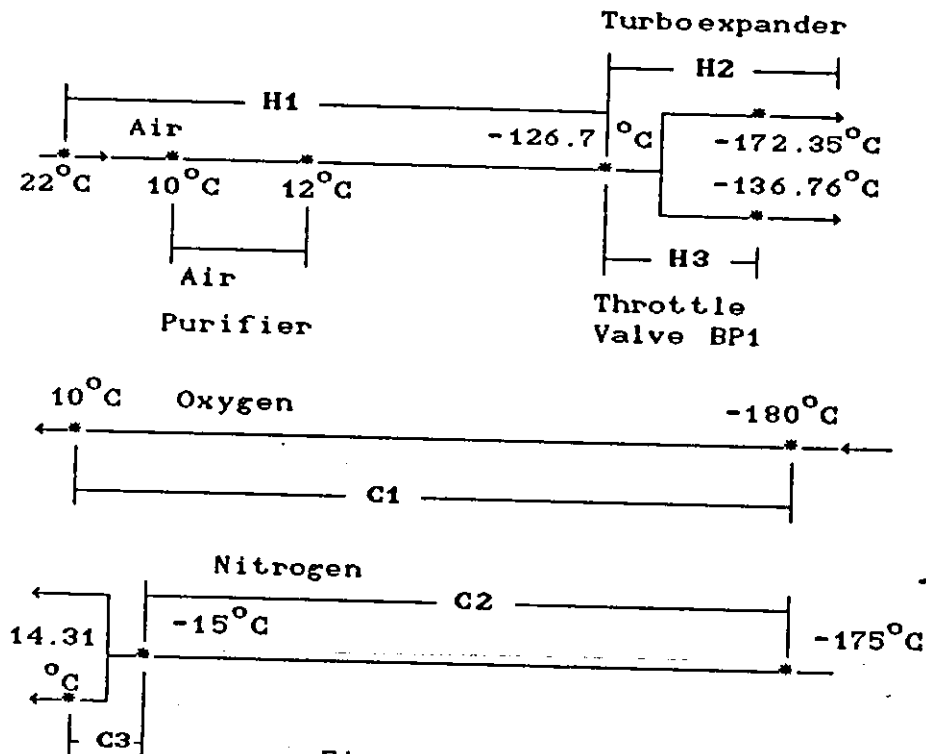


Figure 4.2 : Stream formation

C3.

Using the flowsheet shown in Figure 3.1, hot and cold streams are defined as follows :

Hot stream no.1; H1 (22.0 to -126.69°C)

Comprises air streams numbered in the flowsheet as 9, 10, 11, 12, 13, 14, 15, 16 and 17.

Hot stream no.2; H2 (-126.69 to -172.35°C)

Comprises air streams numbered as 19 and 26.

Hot stream no.3; H3 (-126.69 to -136.76°C)

Comprises air streams numbered as 18, 20, 21, 22, 23 and 24.

Cold stream no.1; C1 (-180.0 to 10.0°C)

Comprises oxygen streams numbered as 42, 45, 46 and 51.

Cold stream no.2; C2 (-175.0 to -15.0°C)

comprises nitrogen streams numbered as 43, 44, 47.

Cold stream no.3; C3 (-15.0 to 14.31°C)

Comprises nitrogen streams numbered as 48, 49, 36 and 38.

The temperature-enthalpy diagram can be used to represent the thermal characteristics of process streams, as illustrated in Figure 4.3. When a differential heat flow dQ

is added to a process stream, it will increase its enthalpy

(II) by $CP \cdot \Delta T$, where,

CP = heat capacity flow rate (kW/K)

= mass flow rate, \dot{m} (kg/s) * specific heat, C_p (kJ/kg.K)

ΔT = differential temperature change

Recalling the assumption of air as an ideal gas and assuming that CP = constant then, the following balance becomes possible,

$$\dot{m} \cdot C_p \cdot \Delta T = CP \cdot \Delta T \quad (4.1)$$

Hence dQ will be the same as ΔH .

Then CP may be calculated as follows,

$$CP_i = \Delta H_i / \Delta T_i \quad (4.2)$$

where i denotes the stream number.

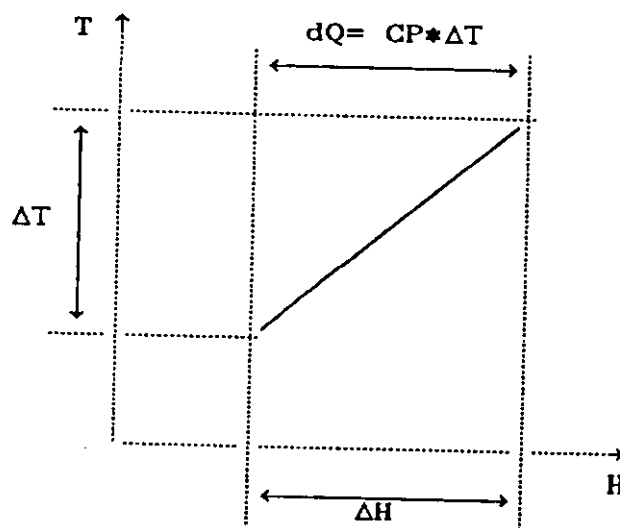


Figure 4.3 temperature - enthalpy diagram

Table (4.1) shows the streams defined before along with their supply and target temperatures, enthalpies and heat capacity flow rates.

TABLE 4.1 - STREAM DATA

| Stream No & Type | T_s (°C) | Enthalpy at T_s (kW) | T_t (°C) | Enthalpy at T_t (kW) | $^{\circ}CP$ (kW/°C) |
|---------------------|---------------|------------------------------|---------------|------------------------------|-------------------------|
| H1, hot | 22.0 | 222.82 | -126.69 | 161.10 | 0.4151 |
| H2, hot | -126.69 | 96.66 | -172.35 | 89.94 | 0.1472 |
| H3, hot | -126.69 | 64.44 | -136.76 | 59.63 | 0.4776 |
| C1, cold | -180.00 | 16.72 | 10.00 | 38.55 | 0.1149 |
| C2, cold | -175.00 | 130.99 | -15.00 | 173.98 | 0.2687 |
| C3, cold | -15.00 | 57.41 | 14.31 | 59.96 | 0.0870 |

4.2.3 Calculation of minimum energy requirements

A very simple way of incorporating the second law of thermodynamics into the energy integration analysis was presented by Hohmann⁽²⁷⁾, Umeda et al⁽²⁸⁾ and Linnhoff and Flower⁽¹⁷⁾. Their analysis will be followed.

Initially, a minimum driving force (temperature difference), ΔT_{min} should be specified. The economical value of ΔT_{min} is usually estimated by trading off energy against capital cost. However, an experience value of ΔT_{min} will be adopted. For a refrigeration system the experience

value of ΔT_{\min} is 5°C (29). Now, we can establish two temperature scales on a graph, one for hot streams and the other for cold streams, which are shifted by 5°C . See Figure (4.2).

Then the stream data are plotted on this graph. Next we establish a series of temperature intervals that correspond to the heads and tails of the arrows, i.e., the inlet (supply temperature, T_s) and the outlet (target temperature, T_t) of the hot and cold streams as given in Table (4.1). Temperature intervals are superimposed.

Setting up the intervals in this way guarantees that full heat interchange within any interval is possible since the driving force is already adequate. Hence, each interval will have either a net surplus or a net deficit of heat as dictated by enthalpy balance, but never both. This is shown in Table 4.2. Knowing the stream population in each interval (from Figure 4.4), enthalpy balances can easily be calculated for each according to

$$\Delta H_i = (T_i - T_{i+1})(\sum CP_{\text{cold}} - \sum CP_{\text{hot}})_i \dots\dots (4.3)$$

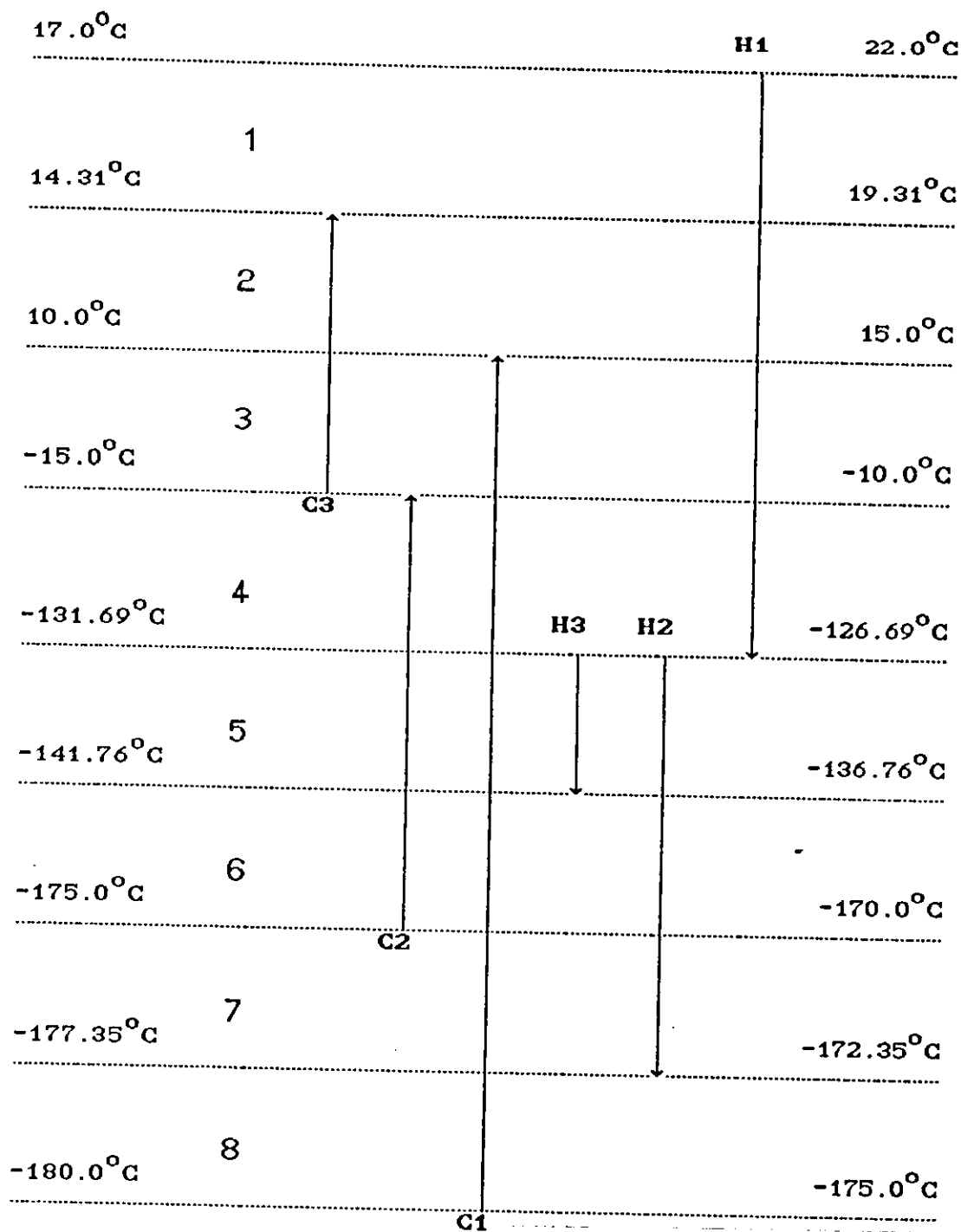


Figure 4.4 - Temperature interval analysis

for any interval i . The last column in Table 4.2 indicates whether an interval is in heat surplus or heat deficit. It

would be possible to produce a feasible network design based on the assumption that all "surplus" intervals rejected heat to cold utility, and all "deficit" intervals received heat from hot utility.

Now, considering the results shown in Table 4.2, Figure 4.3 explains what is called *HEAT CASCADE PRINCIPLE* by which it is possible to evaluate the minimum requirements of energy for a specified process..

TABLE 4.2 - TEMPERATURE INTERVAL ANALYSIS

| Interval No. (i) | $T_i - T_{i+1}$ ($^{\circ}\text{C}$) | $\Sigma \text{CP}_{\text{cold}} - \Sigma \text{CP}_{\text{hot}}$ ($\text{kW}/^{\circ}\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|----------------------------|--|---|------------------------------|--------------------|
| 17.0 $^{\circ}\text{C}$ | | | | |
| 1 | 2.69 | - 0.4151 | -1.1166 | Deficit |
| 14.31 $^{\circ}\text{C}$ | | | | |
| 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 $^{\circ}\text{C}$ | | | | |
| 3 | 25.0 | - 0.2132 | -5.3300 | Surplus |
| -15.0 $^{\circ}\text{C}$ | | | | |
| 4 | 116.69 | - 0.0315 | -3.6757 | Surplus |
| -131.69 $^{\circ}\text{C}$ | | | | |
| 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -141.76 $^{\circ}\text{C}$ | | | | |
| 6 | 33.24 | + 0.2364 | +7.8579 | Deficit |
| -175.0 $^{\circ}\text{C}$ | | | | |
| 7 | 2.35 | - 0.0323 | -0.0759 | Surplus |
| -177.35 $^{\circ}\text{C}$ | | | | |
| 8 | 2.65 | + 0.1149 | +0.3045 | Surplus |
| -180.0 $^{\circ}\text{C}$ | | | | |

Assuming that no heat is supplied to the hottest interval (1) from hot utility, a surplus amount of 1.1166 kW is cascaded into interval (2). Interval (2) has a 1.4141 kW surplus which will be joined with the income from interval

(1) to produce a heat flow of 2.5307 kW passed to interval (3). The cascading process continues through the rest of intervals as shown in Figure 4.5.

By completing the cascading process, the minimum energy requirements are shown to be 5.8788 kW cold.

Appendix B shows the results of the temperature interval analysis for values of ΔT_{\min} ranging from 0.0 to 10.0°C .

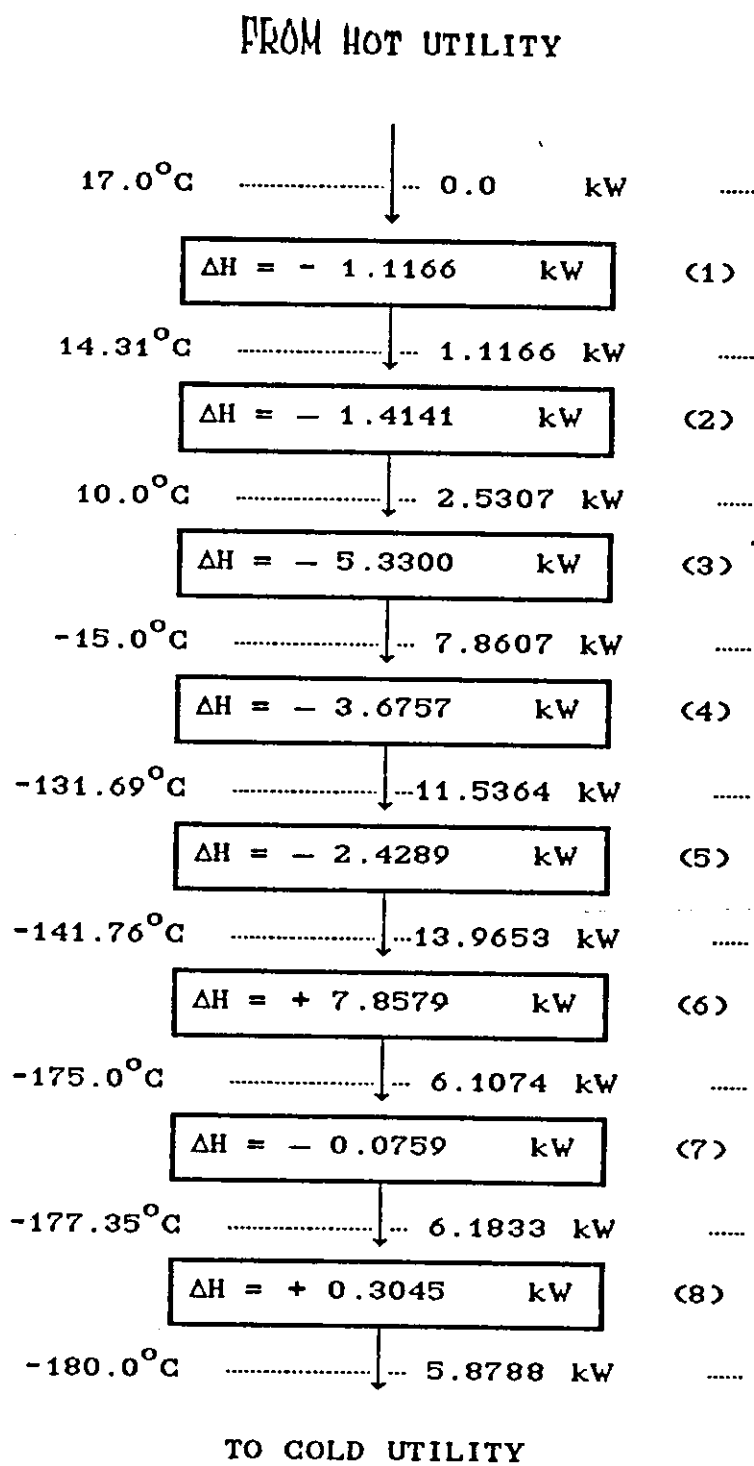


Figure 4.5 - Heat cascading

4.3 Maximum Energy Recovery Design

There are other characteristics of the optimum heat exchanger network. An optimum network should use the minimum area of heat transfer. Also, the number of employed heat exchangers within such network should be minimum. These two characteristics could be investigated for a certain design by using an analysis called MAXIMUM ENERGY RECOVERY (MER) design.

4.3.1 Stream matching / exchanger network

The ruling criterion, is to maximize the individual loads of matches (exchangers) in order to have the minimum number of operating units. This aspect is simply imposed by the fact that the capital cost increases as the number of employed units increases.

Figure 4.6 illustrates the working streams and their enthalpies. The actual cooling utility is also shown.

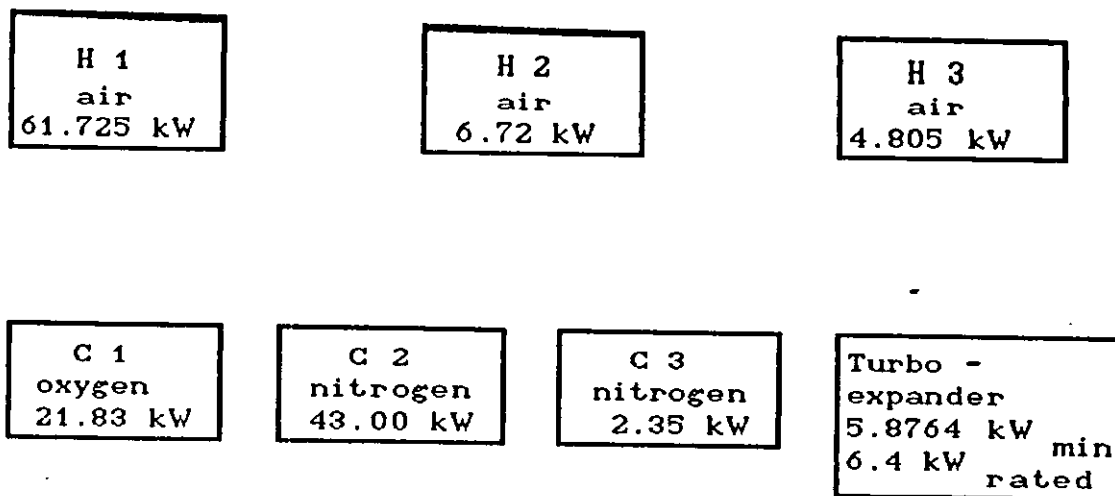


Figure 4.6 - Stream enthalpy

A simplification of the configuration shown in Figure 4.6 is possible; that is to let both C2 and C3 be one stream, say C2'. This unification is justified as follows

- a) physically, C2 and C3 are one stream (both are nitrogen and also have the same pressure) and
- b) outlet temperature of C2 is the same as the inlet temperature of C3.

When the plant is under operation, the partitioning of nitrogen stream into two streams (C2 & C3), Figure 1.1, occurs at inlet to the preliminary heat exchanger.

In order to sustain thermal equilibrium, the newly formed stream C2' must have

- a) a total enthalpy equivalent to the summation of the

individual enthalpies of both C2 and C3 and

- b) a target temperature similar to that of the two streams when mixed at the exit from the preliminary heat exchanger, (1.2°C). Then,

$$\begin{aligned} \text{Enthalpy of } C_2' &= \text{Enthalpy of } C_2 + \text{Enthalpy of } C_3 \\ &= (CP * \Delta T)_{C_2} + (CP * \Delta T)_{C_3} \\ &= (0.2687)(175 - 15) + (0.087)(15 - 12) \\ &= 45.341 \text{ kW} . \end{aligned}$$

The resulting heat capacity flow rate of the new stream will be

$$\begin{aligned} CP &= \frac{\Delta H}{\Delta T} = \frac{45.341 \text{ kW}}{(175 + 1.2)^{\circ}\text{C}} \\ &= 0.2573 \text{ kW}/^{\circ}\text{C} \end{aligned}$$

Now, the streams configuration may be redrawn as illustrated by Figure 4.7.

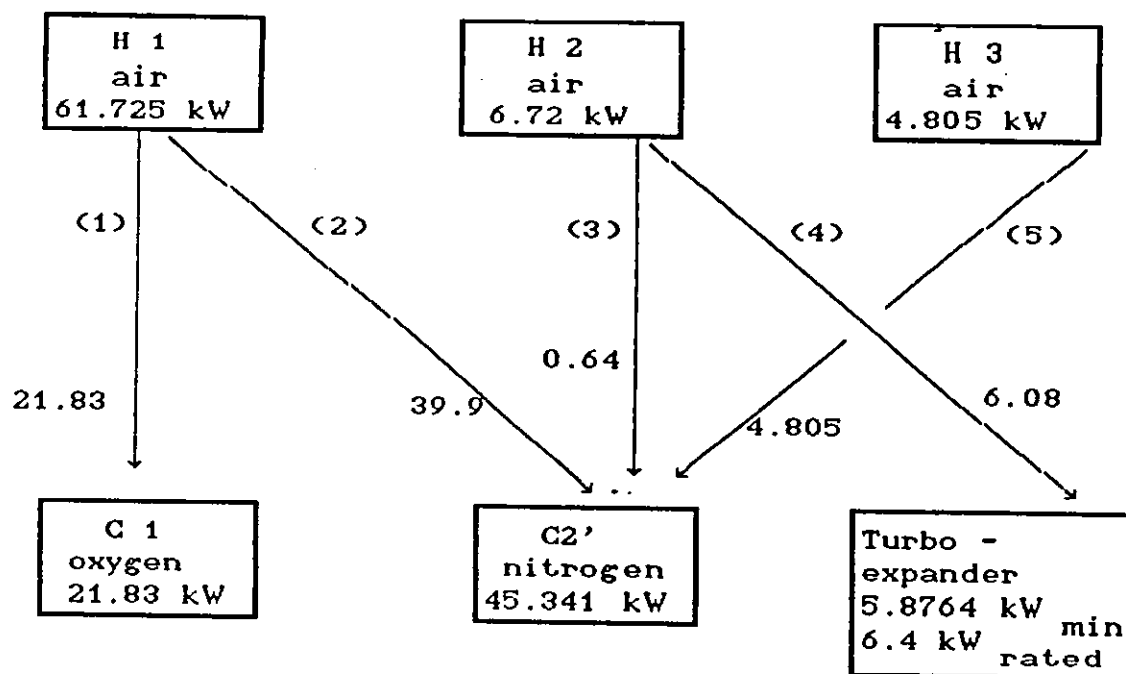


Figure 4.7 - Stream matches

The Figure also illustrates 5 matches started from the cold end (oxygen stream) with their loads.

In this configuration, it is noticed that match (3) is relatively so small to deserve an independent heat exchanger. H3 could be cooled further if the load of match (3) is reloaded upon match (5). This in turn, will leave the cooling load required by H2 handled by only one match; that is match (4). What we have truly done is that we increased the minimum cooling requirement a bit. There is nothing being sacrificed, since the rated capacity of the available cooling utility (turboexpander) allows for such an increase,

recall that its rated capacity is 6.4 kW min.

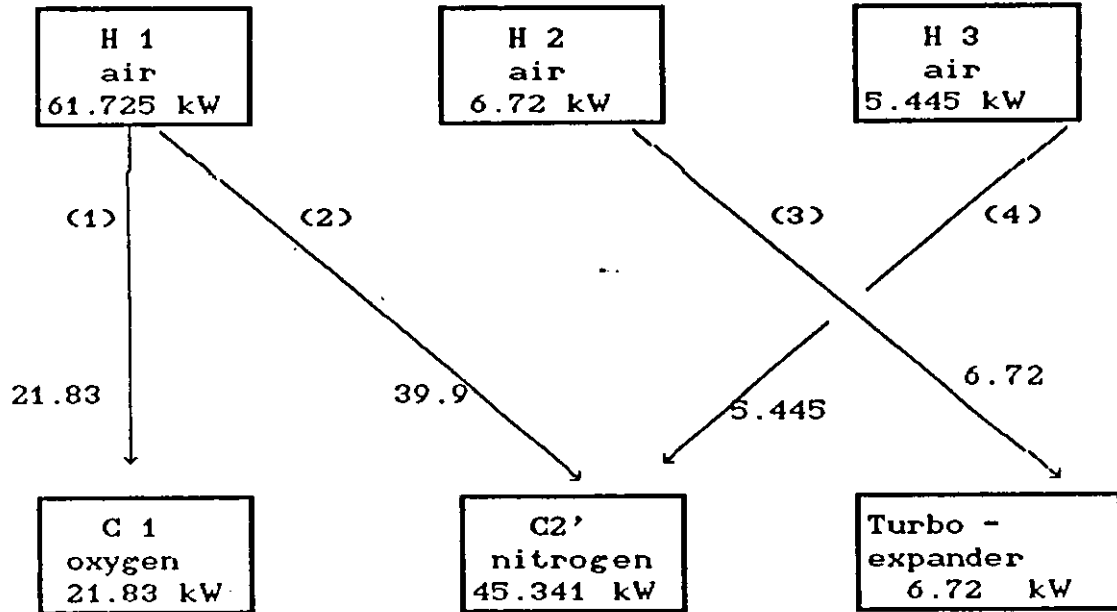


Figure 4.8 -Final configuration

Figure 4.9 shows the final configuration of stream matches and the relevant loads. This configuration indicates that three heat exchangers are needed plus a cooling utility.

It is a common practice to start a design at its most restrictive location. The hot air stream H1 should be interrupted at a certain point; that is, air purifier with a predetermined temperature interval. A temperature increase of 2°C across the air purifier is reported by the manufacturer. The inlet temperature to this unit ranges from 5°C to 10°C .

As a result of this restriction, it becomes necessary to implement matching of streams starting from the hot end bearing in mind that both matches (1) and (2) will be upon two stages to allow for cooling interruption imposed by the air purifier.

Match 1/ 1st stage : H1 is let to exchange heat with C1 such that the outlet temperature of H1 permits a feasible matching with C2; the minimum temperature difference across the warm end of a match (a heat exchanger) should be equal (or even greater than) $\Delta T_{\min} = 5^{\circ}\text{C}$ as presumed at the beginning of analysis. This match stage will be denoted by 1-1.

Match 2/ 1st stage : H1 matches with C2' after it has been cooled through match 1-1. This match stage will be denoted by 2-1.

Along the match stages; 1-1 & 2-1, H1 is to be cooled from its supply temperature down to 10°C which is the maximum permissible value of inlet temperature of air to the purifier. The accompanying temperature drop is chosen to be divided equally among the two match stages.

Supply temperature of C1 is

$$\begin{aligned} (T_s)_{C1} &= (T_t)_{C1} - \frac{(CP * \Delta T)_{H1}}{(CP)_{C1}} \\ &= 10 - \frac{(0.4151)(6)}{0.1149} \\ &= -11.7^\circ\text{C} \end{aligned}$$

Supply temperature of C2' is

$$\begin{aligned} (T_s)_{C2'} &= (T_t)_{C2'} - \frac{(CP * \Delta T)_{H1}}{(CP)_{C2'}} \\ &= 1.2 - \frac{(0.4151)(6)}{(0.2573)} \\ &= -8.5^\circ\text{C} \end{aligned}$$

See Figure 4.8.

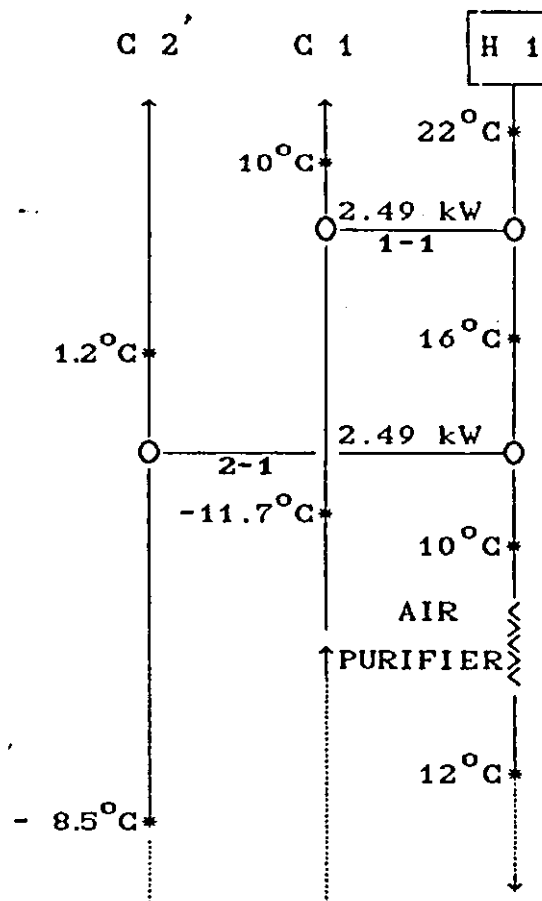


Figure 4.9 Matches 1 and 2 / first stage

By the end of this stage we have :

Supply temperature of H1 = 12°C ,

Target temperature of C1 = -11.7°C and

Target temperature of C2' = -8.5°C .

The load left to the 2nd stage of match 1, denoted by 1-2, will be $21.83 - 2.49 = 19.34$ kW. Similarly, the load of the 2nd stage of match 2; denoted by 2-2, will be

$39.9 \times 2.40 = 97.41 \text{ kW}$. See Figure 4.10.

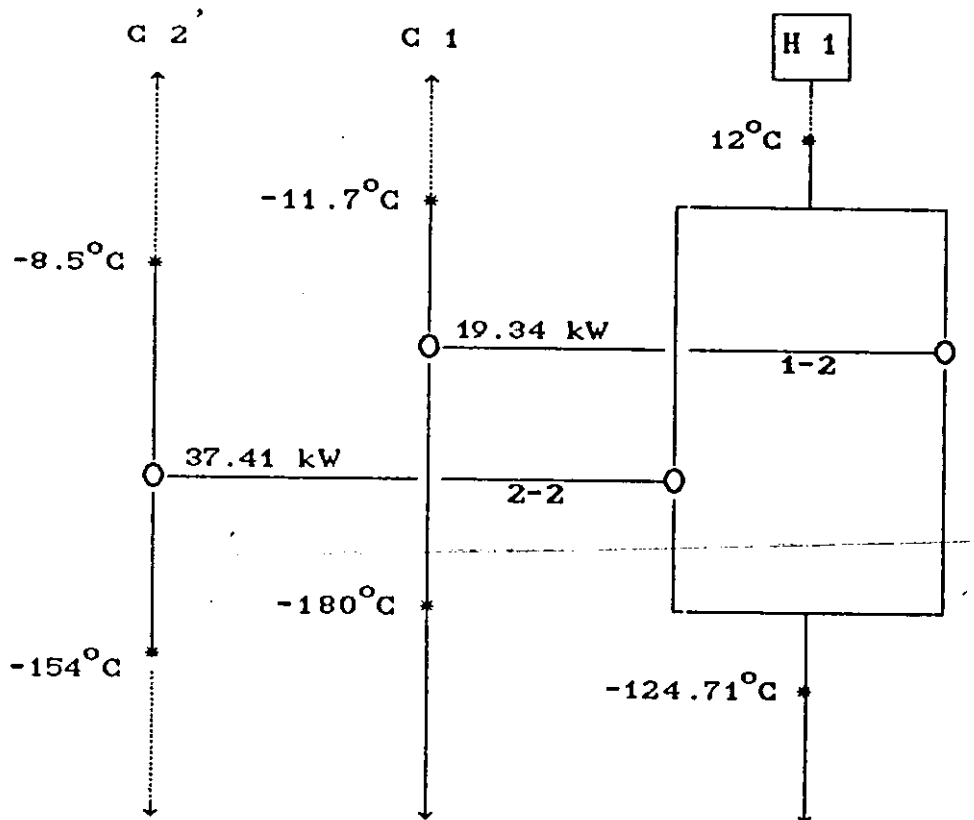


Figure 4.10 - Matches 1 and 2/ second stage

For stream H1 it has been splitted because air stream (H1) actually exchanges heat in parallel with both oxygen stream (C1) and nitrogen stream (C2'). On the other hand, the ratio of splitting should keep air temperature always having the same value of temperature within both resulting parts.

The ratio of air stream splitting is determined in accordance with the decided partial loads. Then :

$$\begin{aligned} \text{H1-part for match 1-2} &= \frac{19.34}{19.34 + 37.41} \\ &= 34\% \text{ H1} \end{aligned}$$

$$\begin{aligned} \therefore \text{H1-part for match 2-2} &= 1.0 - 0.34 \\ &= 66\% \text{ H1.} \end{aligned}$$

Now, target temperature of H1 is

$$\begin{aligned} (T_t) &= T_s - \frac{\Delta H}{CP} \\ &= 12.0 - \frac{19.34 + 37.41}{0.4151} \\ &= -124^\circ\text{C}, \end{aligned}$$

which confirms with technical characteristics of the turbo-expander; since it includes that the inlet temperature of air to the expander should be within $(-130 \text{ to } -115)^\circ\text{C}$.

Supply temperature of C1 is

$$\begin{aligned} (T_s)_{C1} &= (T_t)_{C1} - \frac{(\Delta H)_{\text{match 1-2}}}{(CP)_{C1}} \\ &= -11.7 - \frac{19.34}{0.1149} \\ &= -180^\circ\text{C} \end{aligned}$$

Supply temperature of C2 is

$$\begin{aligned} (T_s)_{C2}' &= (T_t)_{C2}' - \frac{(\Delta H)_{\text{match 2-2}}}{(CP)_{C2}'} \\ &= -8.5 - \frac{37.41}{0.2573} \\ &= -154.0^\circ\text{C}. \end{aligned}$$

Now, match 4 must handle a load of 5.445 kW still available in stream C2'.

Target temperature of H3 is

$$\begin{aligned} (T_t)_{H3} &= (T_s)_{H3} - \frac{(\Delta H)_{H3}}{(CP)_{H3}} \\ &= -124.71 - \frac{5.445}{0.4776} \\ &= -136.11^\circ\text{C} \end{aligned}$$

Supply temperature of C2' is

$$\begin{aligned} (T_s)_{C2'} &= (T_t)_{C2'} - \frac{\Delta H}{(CP)_{C2'}} \\ &= -154.0 - \frac{5.44}{0.2573} \\ &= -175.0^\circ\text{C} \end{aligned}$$

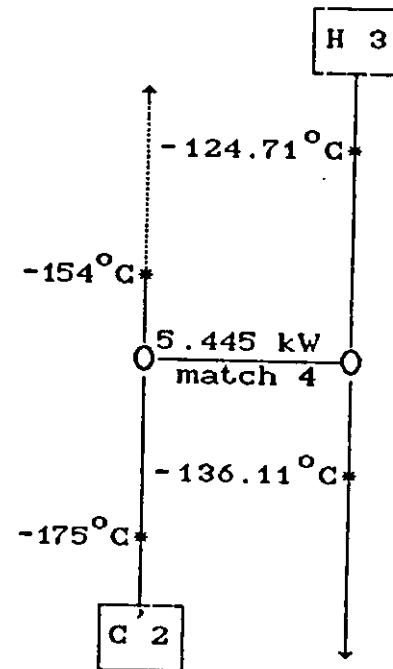


Figure 4.11 - Match 4

A process flowsheet has been established to check the resulting configuration of streams and the relevant matches ; See Figure 4.12.

This flowsheet was exposed to the simulation program of CODE. The results obtained are listed in the Appendix C.

4.4 Column-Tray Sizing

As the simulating program CODE comprises the facility capable for sizing distillation columns, it has been possible to extend our investigation towards the air-separation unit.

A flowsheet segment representing only the double-column rectifying unit is shown in Figure 4.13.

For this segment, the tray sizing calculations were performed using the program phase "Tray Sizing Input". Such calculations aim to estimate the minimum diameters of the distillation columns under operation. The method being used is the Smith-Dresser-Ohlswager technique⁽³⁰⁾.

The program prompts the user to enter the following data: Tray spacing, down comer area, weir length and weir height; then it calculates a diameter for each tray.

The results obtained and shown in Appendix D reveal that:

- The estimated diameter of lower column ≈ 0.30 m.
- The estimated diameter of upper column ≈ 0.40 m.

But the actual diameters of lower and upper columns within the air-separation unit are 0.4 m and 0.5 m, respectively. This means that both of the rectification columns employed in the plant are capable to separate an additional amount of air into oxygen and nitrogen. Also, this

introduces a possibility of expanding the production capacity of the plant while still using the existing air-separation unit. Of course, such expansion should also consider the rated capacities of other existing equipment.

To evaluate the allowance which has already been noticed within both of the rectification columns, CODE program was used. The flow rate of air incoming to the separation unit was increased by increments and then the program phase "Column-Tray Sizing" was run. When the calculations have given column diameters similar to the actual design, a flow rate of air approaching 1.7 times the operating value was permitted. See the results as obtained in the Appendix E.

Figure 4.12 : Optimized exchanger-network of the oxygen plant

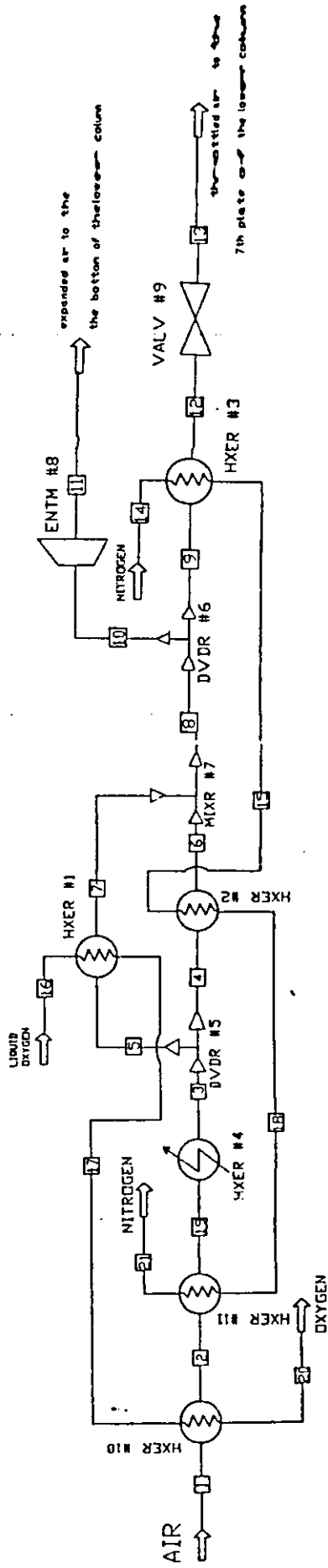
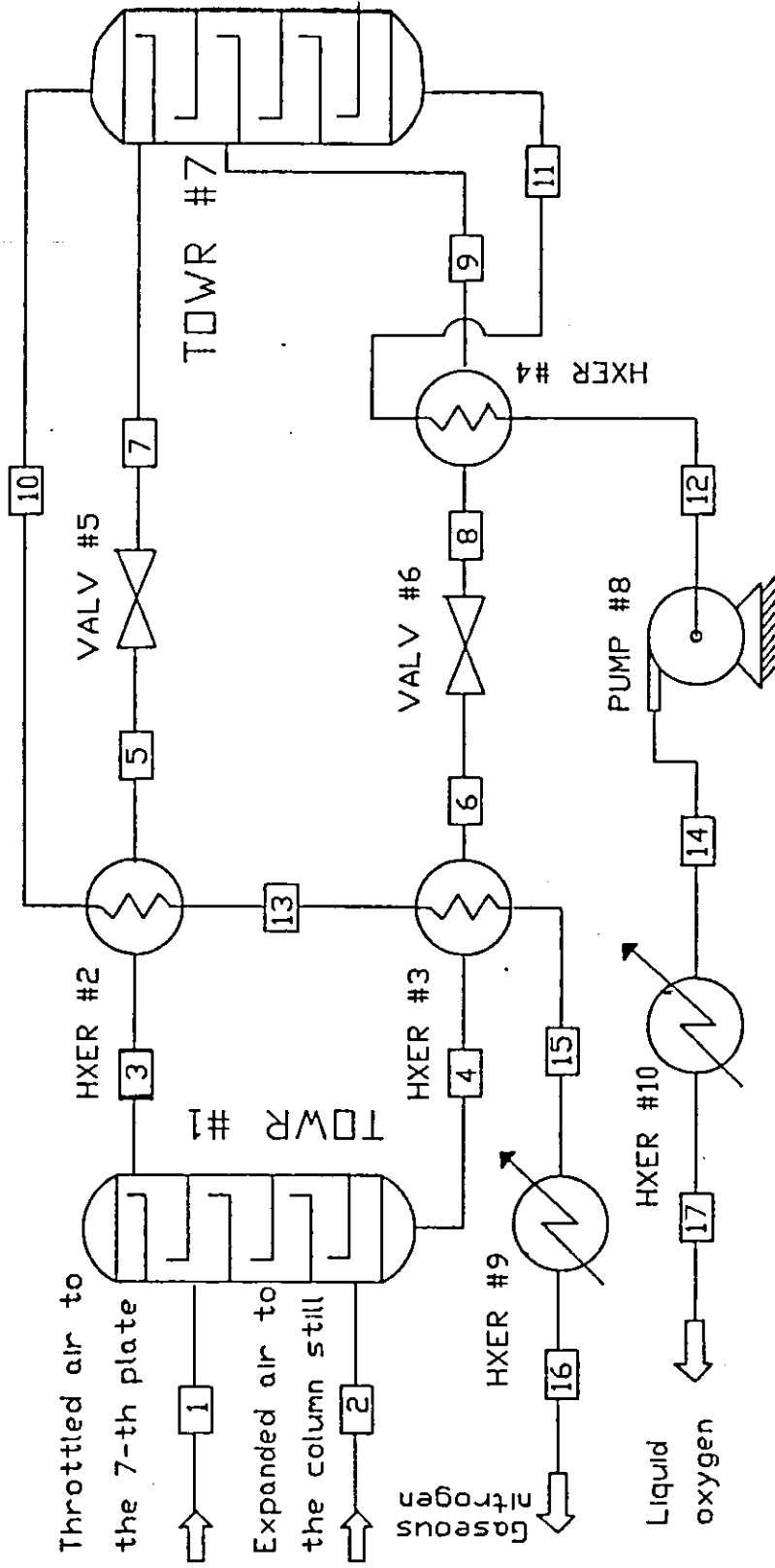


Figure 4.13 : Tray-sizing of the air-rectification columns



Chapter Five

DISCUSSION OF RESULTS

5.1 Base Design

5.1.1 Plant simulation

The results obtained for the simulating flowsheet, shown in Figure 3.1 which are listed in Appendix A, comply with the technical data of the plant as given by the manufacturer. Oxygen purity is only 2% less than stated in the plant certificate. —This deviation does not affect the energy requirements of the circuit; Oxygen purity depends only on the operation characteristics of the rectifying columns. According to the module TOWR, its routine comprises several options that may produce values of purity as high as desired by the user. However, this requires larger number of computer runs and hence longer time necessary for the calculations to converge.

In regard to the modules simulating the heat exchangers, the most important parameter is the logarithmic mean temperature difference (LMTD) which is denoted in all results by "corrected delta T." The value substituted for the coefficient of heat transfer ($300 \text{ MJ/hr.m}^2 \cong 83.33 \text{ W/m}^2$) was not determined in advance; It is only an assumed value. The target, here, is to estimate the product value of the overall coefficient of heat transfer, U , times the heat transfer

area, A , i.e. " UA " corresponding to a specified LMTD and presumed heat duty, Q , for each heat exchanger.

Values of pressure viewed in all results refer to the absolute pressures.

5.1.2 Evaluation of the heat exchanger network

The question that should be answered in this discussion is whether the heat transfer area used in the heat exchanger network is minimum. To answer this question, one should consider the process flowsheet which has been predicted by the energy integration analysis, Figure 4.12. The total area of heat transfer calculated for this network is then compared with that already exists within the actual design of the plant assuming that the coefficients of heat transfer are kept the same.

The scheme to be applied is as follows:

1. The " UA " product of all actual heat exchanger network are are estimated using the general equation of heat transfer,

$$Q = U * A * LMTD \dots\dots(5.2)$$

where,

Q : Load of the exchanger, kW,

U : Overall coefficient of heat transfer of the exchanger, $W/m^2 \cdot ^\circ C$,

A : Heat-transfer area of the tube side , m^2 and

LMTD : Logarithmic mean temperature difference across the heat exchanger, $^\circ C$.

LMTD is known for any heat-exchanging section and Q is obtained from the results of the program calculations. Then, the product "UA" is determined by the equation (5.2). See Table 5.1.

2. Using the same equation, the corresponding "UA" products for the predicted flowsheet in Figure 4.11 can be evaluated using results found in Appendix B. See Table 5.2.
3. The values of the overall coefficient of heat transfer for the actual design are evaluated as follows

$$U_{\text{actual}} = \frac{\text{"UA"}_{\text{actual}}}{A_{\text{actual}}} \dots\dots\dots(5.3)$$

where A_{actual} is recalled from the technical data given for the plant. See Table 5.3.

4. Then the resulting values of U in step 3 and the corresponding "UA"'s in Table 5.2 are substituted in the

following equation to find the predicted area,

$$A_{\text{predicted}} = \frac{U_{\text{actual}}}{U_{\text{predicted}}} \dots\dots\dots (5.4)$$

See Table 5.4.

TABLE 5.1 : "UA" FOR ACTUAL DESIGN

| Section | Simulating Module | Q (kW) | LMTD (°C) | "UA" (W/°C) |
|------------------------------------|-------------------|---------|-----------|-------------|
| <u>Heat Exchanger/</u> | | | | |
| - <u>upper half</u> : | | | | |
| * Air - nitrogen | HXER # 11 | 39.58 | 30.11 | 1314 |
| * Air - oxygen | HXER # 12 | 17.90 | 33.76 | 530 |
| - <u>lower half</u> : | | | | |
| * Air - nitrogen | HXER # 20 | 3.41 | 37.11 | 92 |
| * Air - oxygen | HXER # 21 | 1.40 | 41.59 | 34 |
| <u>Preliminary Heat-Exchanger/</u> | | | | |
| * Air - nitrogen | HXER # 9 | 2.35 | 18.32 | 128 |
| * nitrogen - oxygen | HXER # 15 | - 2.52† | 1.45 | 1737 |
| * Air - nitrogen | HXER # 10 | 2.72 | 7.37 | 370 |
| $\Sigma =$ | | | | 4205 |

† the negative sign is imposed because at this section of heat exchanger, the nitrogen works as a hot stream which is opposite to the nitrogen function throughout the rest of sections.

TABLE 5.2 : "UA" FOR PREDICTED FLOWSHEET

| <u>Section</u> | <u>Simulating Module</u> | <u>Q (kW)</u> | <u>LMTD (°C)</u> | <u>"UA" (W/°C)</u> |
|------------------------------------|------------------------------|-------------------|----------------------|------------------------|
| <u>Heat Exchanger/</u> | | | | |
| - <u>upper_half</u> : | | | | |
| * Air - nitrogen | HXER # 2 | 40.00 | 23.20 | 1724 |
| * Air - oxygen | HXER # 1 | 9.87 | 36.01 | 274 |
| - <u>lower_half</u> : | | | | |
| * Air - nitrogen | HXER # 3 | 5.10 | 32.58 | 157 |
| <u>Preliminary Heat-Exchanger/</u> | | | | |
| * Air - nitrogen | HXER # 11 | 2.38 | 15.51 | 153 |
| * Air - oxygen | HXER # 10 | 1.96 | 19.04 | 103 |
| Σ | | | | 2411 |

TABLE 5.3 : "U" FOR ACTUAL DESIGN

| <u>Section</u> | <u>"UA"</u> (W/°C) | <u>A</u> (m ²) | <u>U</u> (W/m ² . °C) |
|------------------------------------|-----------------------|-------------------------------|-------------------------------------|
| <u>Heat Exchanger/</u> | | | |
| - <u>upper_half</u> : | | | |
| * Air - nitrogen | 1314 | 4.58 | 286.9 |
| * Air - oxygen | 530 | 2.29 | 231.4 |
| - <u>lower_half</u> : | | | |
| * Air - nitrogen | 92 | 4.58 | 20.1 |
| * Air - oxygen | 34 | 2.29 | 14.8 |
| <u>Preliminary Heat-Exchanger/</u> | | | |
| * Air - nitrogen | 128 + 370 | | |
| | = 498 | 7.1 | 70.1 |
| * nitrogen - oxygen | 1737 | 1.4 | 1240.7 |

TABLE 5.4 : HEAT TRANSFER AREA FOR THE PREDICTED DESIGN

| <u>Section</u> | <u>U</u> <u>(W/m².°C)</u> | <u>"UA"</u> <u>(W/°C)</u> | <u>A</u> <u>(m²)</u> |
|------------------------------------|---|------------------------------|------------------------------------|
| <u>Heat Exchanger/</u> | | | |
| - <u>upper_half</u> : | | | |
| * Air - nitrogen | 286.9 | 1724 | 6.0 |
| * Air - oxygen | 231.4 | 274 | 1.18 |
| - <u>lower_half</u> : | | | |
| * Air - nitrogen | 20.1 | 157 | 7.8 |
| * Air - oxygen | 14.8 | 0.0 | 0.0 |
| <u>Preliminary Heat-Exchanger/</u> | | | |
| * Air - nitrogen | 70.1 | 153 | 2.18 |
| * Air - oxygen | x† | 103 | x |
| $\Sigma =$ | | 17.16 + x | |

† x stands for the unknown value of the heat-transfer coefficient between air and oxygen since in the actual design of the plant there is no match between these two streams.

For air-oxygen match suggested within the preliminary heat-exchanger, a coefficient of heat transfer similar to that of air-oxygen match within the upper half of the actual heat exchanger is employed ($U = 231.4 \text{ W/m}^2 \cdot ^\circ\text{C}$.) Also, the geometry of tubes is suggested to remain invariant i.e. tube-in-tube. It is now desired to evaluate the dimensions of these tubes which will suit both the coefficient of heat transfer and the suggested geometry.

When two different fluids, say F and G, flow according to the pattern shown in Figure 5.1, the coefficient of heat transfer U ruling the process of heat transfer between these fluids is estimated as follows⁽³¹⁾, assuming that thermal resistance of the tube wall is negligible when compared to the thermal resistance of the fluid film,

$$U = \frac{h_{i_o} * h_o}{h_{i_o} + h_o} \quad \dots\dots\dots (5.5)$$

where,

h_o : film coefficient of heat transfer for fluid F and

h_{i_o} : film coefficient of heat transfer for fluid G.

Actually h_{i_o} is the modified value of the coefficient (h_i) which is based on the inside diameter of the inner tube such that,

$$h_{i_o} = h_i * \frac{d_i}{d_o} \quad (5.6)$$

where, referring to Figure 5.1,

h_{i_o} : Modified film coefficient of heat transfer, $W/m^2 \cdot ^\circ C$,

h_i : Film coefficient of heat transfer based on the inside diameter of the inner tube, $W/m^2 \cdot ^\circ C$,

d_i : Inside diameter of the inner tube, m and

d_o : Outside diameter of the inner tube, m.

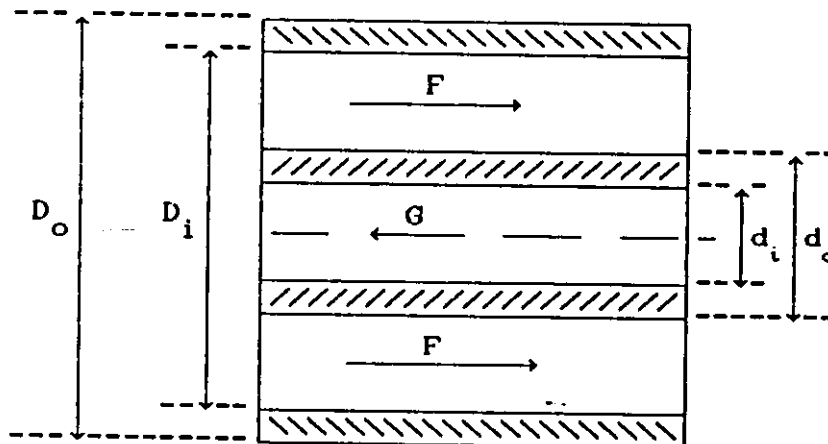


Figure 5.1 Tube-in-tube section

For turbulent flow of gases inside tubes, the film coefficient of heat transfer h can be expressed as a function of both Prandtl and Reynolds numbers as follows⁽³²⁾

$$h = 0.022 * Pr^{0.6} * Re^{0.8} \quad (5.7)$$

To obtain the required value of U ($231.4 W/m^2 \cdot ^\circ C$), equation (5.5) is used. To determine the appropriate heat transfer coefficients h_o and h_{i_o} resulting from the suggested geometry (tube-in-tube), one can use equation (5.7)

whereby the Prandtl number is known at the corresponding range of temperature. The Reynolds number in the predicted section can be now found. As the Reynolds number is known, one can choose a combination of flow conditions and geometry to satisfy the calculated Reynolds number.

Let's denote the parameters related to the upper half of heat exchanger A4 by "1" and those related to the preliminary heat exchanger A3 by "2".

Then, recalling the necessary values from Table 5.5 and substituting into equation 5.6 will give

$$Pr_1^{0.6} * Re_1^{0.8} = Pr_2^{0.6} * Re_2^{0.8}$$

For air,

$$(1.141)^{0.6} * (6.60866E4)^{0.8} = (0.759)^{0.6} * (Re_2)^{0.8}$$

$$\therefore Re_{2,air} = 8.97 E4$$

TABLE 5.5 : Pr & Re NUMBERS FOR AIR AND OXYGEN

| <u>Heat Exchanger/ Upper Half</u> | | |
|-----------------------------------|-----------------------|------------------------|
| <u>Stream</u> | <u>Prandtl Number</u> | <u>Reynolds Number</u> |
| Air | 1.141 | 6.60866 E4 |
| O ₂ | 1.010 | 1.94540 E4 |
| <u>Preliminary Heat-Exchanger</u> | | |
| <u>Stream</u> | <u>Prandtl Number</u> | |
| Air | 0.759 | |
| O ₂ | 1.107 | |

For O₂,

$$(1.010)^{0.6} * (1.9454E4)^{0.8} = (1.107)^{0.6} * (Re_2)^{0.8}$$

$$\therefore Re_{2,O_2} = 1.811E4$$

For the flow inside tube, the Reynolds number is expressed as follows

$$Re = \frac{\rho \cdot v \cdot d}{\mu} \quad \dots\dots\dots(5.8)$$

where,

Re : Reynolds number,

v : Flow velocity, m/s,

d : Tube diameter, m and

μ : Dynamic viscosity of the flowing fluid Pa.s.

But for the flow inside annular space (tube-in-tube), an equivalent diameter, De , is substituted instead of tube diameter, d . For heat transfer, De may be given as in Reference 32,

$$De = \frac{D_i^2 - d_o^2}{d_o} \quad \dots\dots\dots (5.9)$$

in terms of the dimensions shown in Figure 5.1, where

D_i : The inside diameter of the outer tube, m.

Now,

$$Re_{2,air} = \frac{\rho \cdot v \cdot De}{\mu} = \frac{(53.1) \cdot (v) \cdot (De)}{1.811E-5} = 8.97 E4$$

$$\therefore (v \cdot De)_{air} = 0.030 \quad \text{and,}$$

$$Re_{2,o_2} = \frac{(304.35) \cdot (v) \cdot (d_i)}{1.98E-5} = 1.811E4$$

$$\therefore (v d_i)_{o_2} = 1.1782E-3$$

Let's have for oxygen, 19 tubes of 5x1 mm diameter (similar to the upper-half section within the heat exchanger A4). This will yield a flow velocity of

$$v = \frac{1.1782E-3}{d_i (= 3E-3)} = 0.39 \text{ m/s.}$$

This value is less than that of the actual design (0.5 m/s). It is noted that oxygen tubes are selected to have the same thickness as in the heat exchanger since the working pressure is assumed similar to the actual design.

To maintain air velocity as in the actual design (5.0 m/s),

$$De = \frac{0.030}{5.0} = 6.0 \text{ E-3 m} = 6.0 \text{ mm.}$$

Recall that $De = \frac{D_i^2 - d_o^2}{d_o^2}$ where d_o , here, is the outside

diameter of the inner (oxygen) tube i.e. 5 mm.

$$\therefore 5.64 = \frac{D_i^2 - 5^2}{5^2} \text{ then,}$$

$$D_i = 13.22 \cong 13 \text{ mm}$$

In order to calculate the thickness of the outer (air) tube, the equation of hoop stresses has been used⁽³³⁾. The necessary properties of copper were obtained⁽³⁴⁾. The thickness was calculated to be 1.0mm. This means that the

diameter of the air tube is 15x1 mm.

Since $U_{\text{air-O}_2}$ has already been assumed to be 231.4 W/ m² °C and the product of "UA" was determined as 103 W/ °C, then the heat-transfer area required for air-O₂ section will be

$$A_{\text{air-O}_2} = \frac{103}{231.4} = 0.445 \text{ m}^2.$$

Hence, the length of the air tube should be

$$L = \frac{0.445}{(19)(\pi)(5.E-3)} = 1.491 \cong 1.5 \text{ m}.$$

Finally a bundle of straight, copper tube-in-tube arrangement would be necessary. This will result in a total area of heat transfer pointing to $17.16 + 0.445 = 17.605 \text{ m}^2$. This resembles a reduction in heat transfer area of about 21% of the existing design (22.24 m².)

5.1.3 Inspection of the air-separation unit/ rectifying columns

Using the program phase named "Tray Sizing Input", it has been possible to investigate the maximum rectification capacity of the two columns within the air-separation unit.

The sizing of a column is based on the *flooding diameter*. It is the maximum diameter beyond which flooding occurs i.e. the column will function improperly.

The lower and upper column diameters needed to rectify the nominal flow rate of the incoming air have been calculated to be 0.3 m and 0.4 m, respectively. These diameters are less than those within the existing design. The flow rate of air has then been incrementally raised until both lower and upper columns approach their actual diameters (0.4 m and 0.5 m for the lower and upper columns, respectively). The corresponding value of air flow-rate amounts to 70% above the nominal flow rate.

Through plant details, the maximum tolerance provided for design capacities of equipment was noticed to be less than or equal to 10%. If a similar tolerance is assumed for the air-separation unit, it will have a capacity allowance of 60%. This availability indicates the possibility of increasing the plant productivity. Of course, the plant equipment will respond to the new productivity according to the rated capacity of each. Tracking the plant circuit, the following steps are needed for increasing the productivity of the plant by 60% :

1. Installing another air compressor which is able to deliver 60% of the air flow-rate suggested for the existing compressor at the same outlet pressure. The

resulting two outputs could then join each other in a final single line.

2. Replacement of the air purifier with a new one whose cylinders can accommodate the purification of the extra amount of air flow-rate.
3. Replacement of the expansion turbine with a new one whose liquefaction (refrigeration) duty is high enough to fit the running target.
4. Replacement of the liquid-oxygen pump with a new one capable to pump 60% over the rated capacity of the present pump.
5. Replacement of the existing pipe-network with a new one which is capable to withstand 1.6 times the nominal flow rates.
6. Instruments will be independent of any variation. This is due to the constancy of the properties being measured.
7. A reserve of 21% in the heat transfer area has been estimated to exist within the heat-exchanger network if operated according to the configuration predicted before.

Along with these steps, neither new nor additional civil

work will be needed.

5.2. Economical Comparison of the Existing and the Predicted Designs

Table 5.6 illustrates the elements of capital cost of a new oxygen plant based on 1988 prices⁽¹⁾. The Table also shows the extra capacity for the major equipment within the plant over that given by the manufacturer. This capacity has been evaluated such that the production capacity of the existing plant could be expanded by 60%.

Table 5.7 illustrates the cost of expanding the production capacity of the existing plant by 60% of its nominal value and regarding to the steps listed in section 5.1.4.

TABLE 5.6 : COST ELEMENTS OF A NEW OXYGEN PLANT OF TYPE
K-0.15 AND THE EXTRA CAPACITY WITH RESPECT
RESPECT TO 60% EXPANSION

| Cost element | Cost | Extra Capacity |
|----------------------------------|------------|----------------|
| * Air compressor | \$ 100,000 | 0.0% |
| * Air purifier | \$ 10,000 | 0.0% |
| * preliminary heat exchanger, A3 | \$ 15,000 | 35.0% |
| * Heat exchanger, A4 | \$ 20,000 | 0.0% |
| * Turbo-expander | \$ 10,000 | 0.0% |
| * Liquid-oxygen pump | \$ 15,000 | 0.0% |
| * Rectifying columns | \$ 50,000 | 100.0% |
| * Two subcoolers | \$ 15,000 | 0.0% |
| * Electric system | \$ 9,000 | 100.0% |
| * Piping system | \$ 16,000 | 0.0% |
| * Civil construction | \$ 75,000 | 100.0% |
| Σ Cost | \$ 335,000 | |

TABLE 5.7 : COST OF EXPANDING THE
PRODUCTION CAPACITY OF
 THE EXISTING PLANT BY
 60%

| Cost element | Cost |
|----------------------------------|------------|
| * Air compressor | \$ 85,000 |
| * Air purifier | \$ 12,000 |
| * preliminary heat exchanger, A3 | \$ 16,000 |
| * Heat exchanger, A4 | \$ 23,000 |
| * Turbo-expander | \$ 12,000 |
| * Liquid-oxygen pump | \$ 18,000 |
| * Rectifying columns | \$ 0,000 |
| * Two subcoolers | \$ 18,000 |
| * Electric system | \$ 0,000 |
| * Piping system | \$ 25,000 |
| * Civil construction | \$ 0,000 |
| Σ Cost | \$ 209,000 |

Table 5.8 shows the annual costs for both the existing and expanded plants⁽¹⁾.

Now, if JISICO has a future plan demanding more oxygen gas but, less than or equal 1.6 times the production capacity of the existing plant, then two alternatives will rise.

TABLE 5.8 : ANNUAL COST FOR THE EXISTING AND EXPANDED PLANTS

| Cost item | Cost value | |
|----------------|----------------|----------------|
| | Existing plant | Expanded plant |
| Electric power | \$ 10,000 | \$ 16,000 |
| Man-power | \$ 12,000 | \$ 12,000 |
| Maintenance | \$ 8,000 | \$ 12,800 |
| Σ | \$ 30,000 | \$ 40,000 |

These are,

- Alternative 1 : To expand the production capacity of the existing plant by 60%
- Alternative 2 : To install a new plant similar to the existing one.

Upon having a decision to choose either of the two alternatives, lets assume that the company will adopt a simple aggressive policy, and choose a plan for the optimistic sales forecast. This level of analysis is of the least order of complexity⁽³⁵⁾.

The analysis can be summarized as follows :

- (1) The annual costs are estimated for both alternatives 1 & 2.

- (2) The cash necessary to start each alternative is annualized. The calculations are based on 10% interest rate and 20 years life time.

- (3) The summation of values estimated in (1) and (2) is divided by the annual amount of production to estimate cost of unit production as expected along the plant life time.

Table 5.9 illustrates this analysis.

TABLE 5.9 : ALTERNATIVE - DECISION ANALYSIS

| Description | Alternative (1) | Alternative (2) |
|--|----------------------------|--------------------|
| (a) Annual cost : | | |
| - Electric power | \$ 16,000 | \$ 20,000 |
| - Man-power | \$ 12,000 | \$ 24,000 |
| - Maintenance | \$ 12,800 | \$ 16,000 |
| Σ | \$ 40,000 | \$ 50,000 |
| (b) Cash for starting | \$ 209,000 | \$ 335,000 |
| (c) Annualized cash | \$ 24,549 | \$ 39,349 |
| (d) Σ (a) & (c) | \$ 64,549 | \$ 89,349 |
| (e) Annual production of oxygen, m ³ | (1.6)(1.23E6) [*] | (2.0)(1.23E6) |
| (f) Cost of unit production | \$ 0.0327 | \$ 0.0363 |

Alternative 1 is noticed to cost about 94.5% of the alternative 2 cost.

* The annual production of the plant is 1,230,000 m³ of gaseous oxygen⁽¹⁾.

The estimated cost of unit production does not consider the deterioration factor for either equipment or currency. It only indicates the alternatives costs relative to each other.

CONCLUSION

The following statements constitute the conclusion of the research :

- (1) The oxygen plant under consideration satisfies the condition of the minimum energy requirements by 91.8%. Recall that the rated capacity of the turboexpander is 6.4 kW while the minimum cold requirement has been estimated to be 5.8788 kW.
- (2) The heat exchanger network employed within the plant slightly deviates from the optimum configuration. The heat transfer area of the preliminary heat exchanger A3, could be reduced by 21% if a stream configuration similar to that within the heat exchanger A4 was applied.
- (3) The air-separation unit/rectifying columns are capable to handle 60% more flow rate of air than the nominal flow rate. This extra capacity does not consider the (evaporation) losses within practice, it stands for ideal process.
- (4) The existing instrumentation of the plant will need few

modifications to accommodate the additional rates.

- (5) The cost of equipment replacement has been estimated to be \$ 209,000 based on the 1988 prices. While erecting a new similar plant will cost \$ 335,000.
- (6) The cost analysis presented shows that the cost of unit production if the existing plant is expanded is about 90.0% of the cost if a new similar plant is installed next to the existing one. If the alternative of plant expansion was decided upon, the operation of the existing plant would be stalled to implement the necessary equipment replacement. This may impose additional cost such that expansion becomes not profitable.
- (7) The results obtained in this work indicate that expanding the existing plant may not after all be favourable.

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APPENDIXES

Appendix A

Appendix B

Appendix C

Appendix D

Appendix E

Appendix A

Temperature interval analysis

$$\Delta T = 0,0^{\circ}\text{C}$$

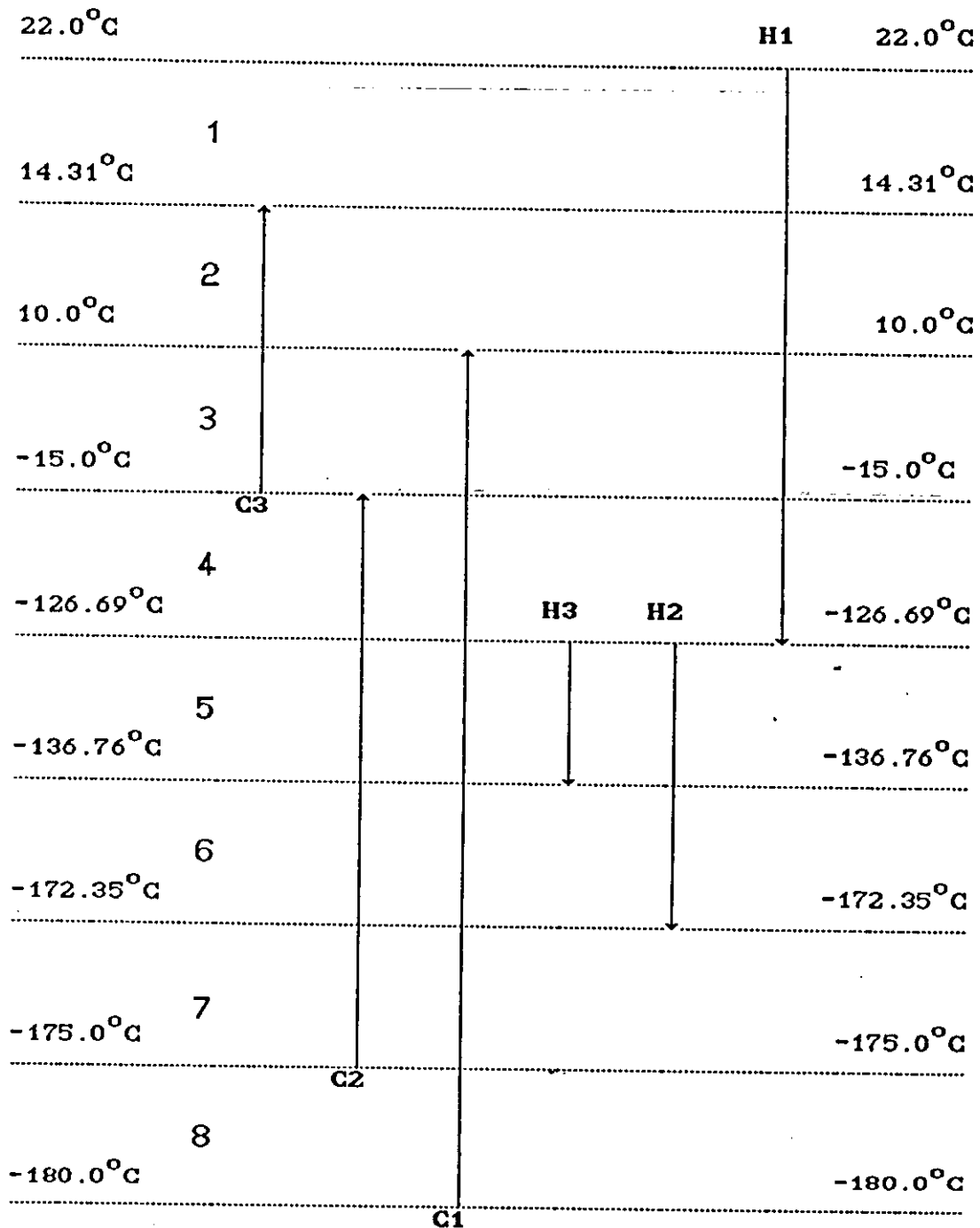


Figure A.1 : Temperature interval analysis

TABLE A.1 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 0.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|------------------------------|--------------------|
| 22.0 | 1 | 7.69 | - 0.4151 | -3.1921 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 111.69 | - 0.0315 | -3.5182 | Surplus |
| -126.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -136.76 | 6 | 35.59 | + 0.2364 | +8.4135 | Deficit |
| -172.35 | 7 | 2.65 | + 0.3836 | +1.0165 | Deficit |
| -175.0 | 8 | 5.0 | + 0.1149 | +0.5745 | Deficit |
| -180.0 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.8788 | |

$$\Delta T = 1.0^{\circ}\text{C}$$

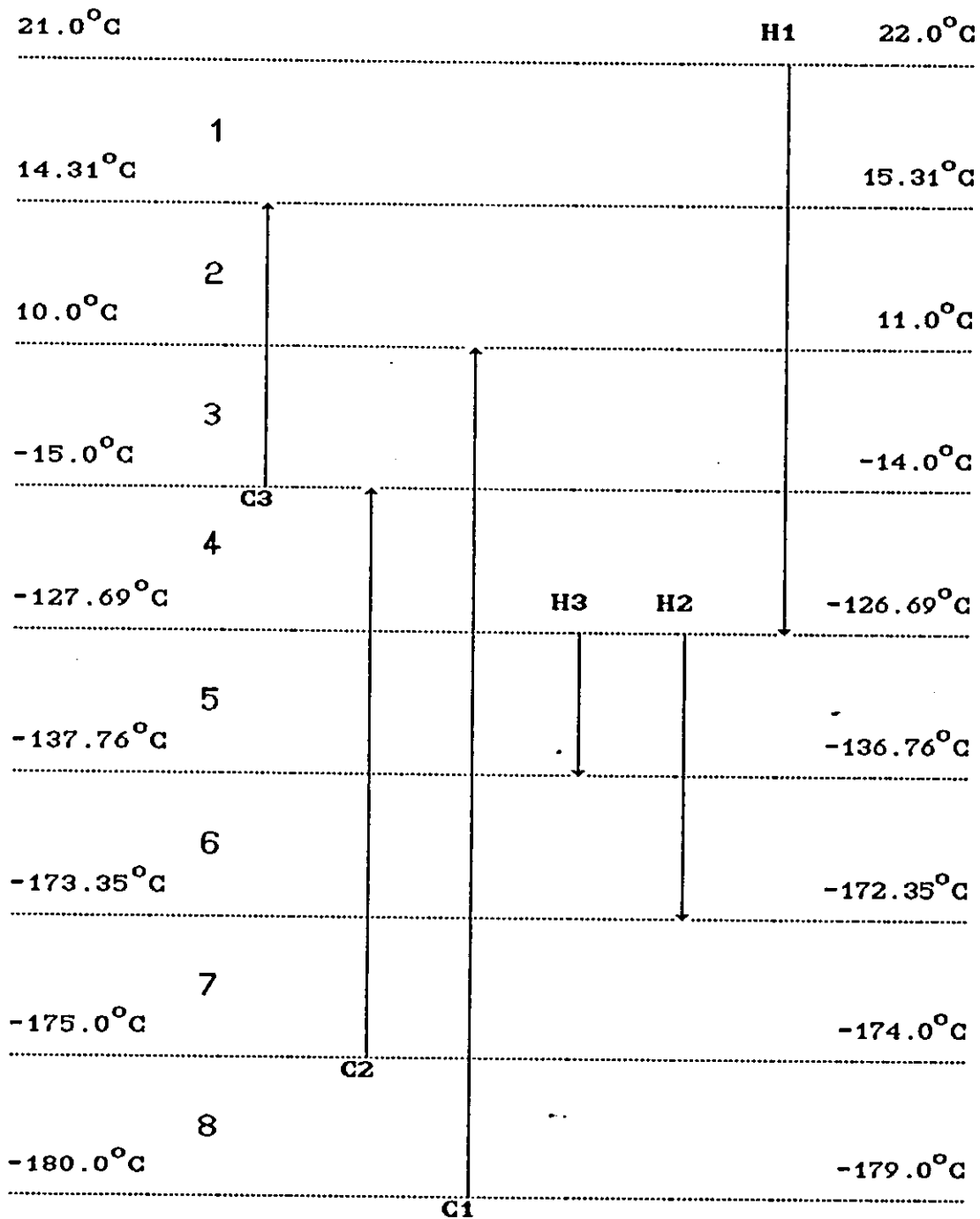


Figure A.2 : Temperature interval analysis

TABLE A.2 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 1.0^{\circ}\text{C}$

| $^{\circ}\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^{\circ}\text{C}$) | $\Sigma \text{CP}_{\text{cold}} - \Sigma \text{CP}_{\text{hot}}$ ($\text{kW}/^{\circ}\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|--------------------|---------------------------|--|---|------------------------------|--------------------|
| 21.0 | 1 | 6.69 | - 0.4151 | -2.7770 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 111.69 | - 0.0315 | -3.5497 | Surplus |
| -127.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -137.76 | 6 | 35.59 | + 0.2364 | +8.4135 | Deficit |
| -173.35 | 7 | 2.65 | + 0.3836 | +0.6329 | Deficit |
| -175.0 | 8 | 5.0 | + 0.1149 | +0.5745 | Deficit |
| -180.0 | $E_{\text{min}} = \Sigma$ | | | 5.8788 | |

$$\Delta T = 2.0^{\circ}\text{C}$$

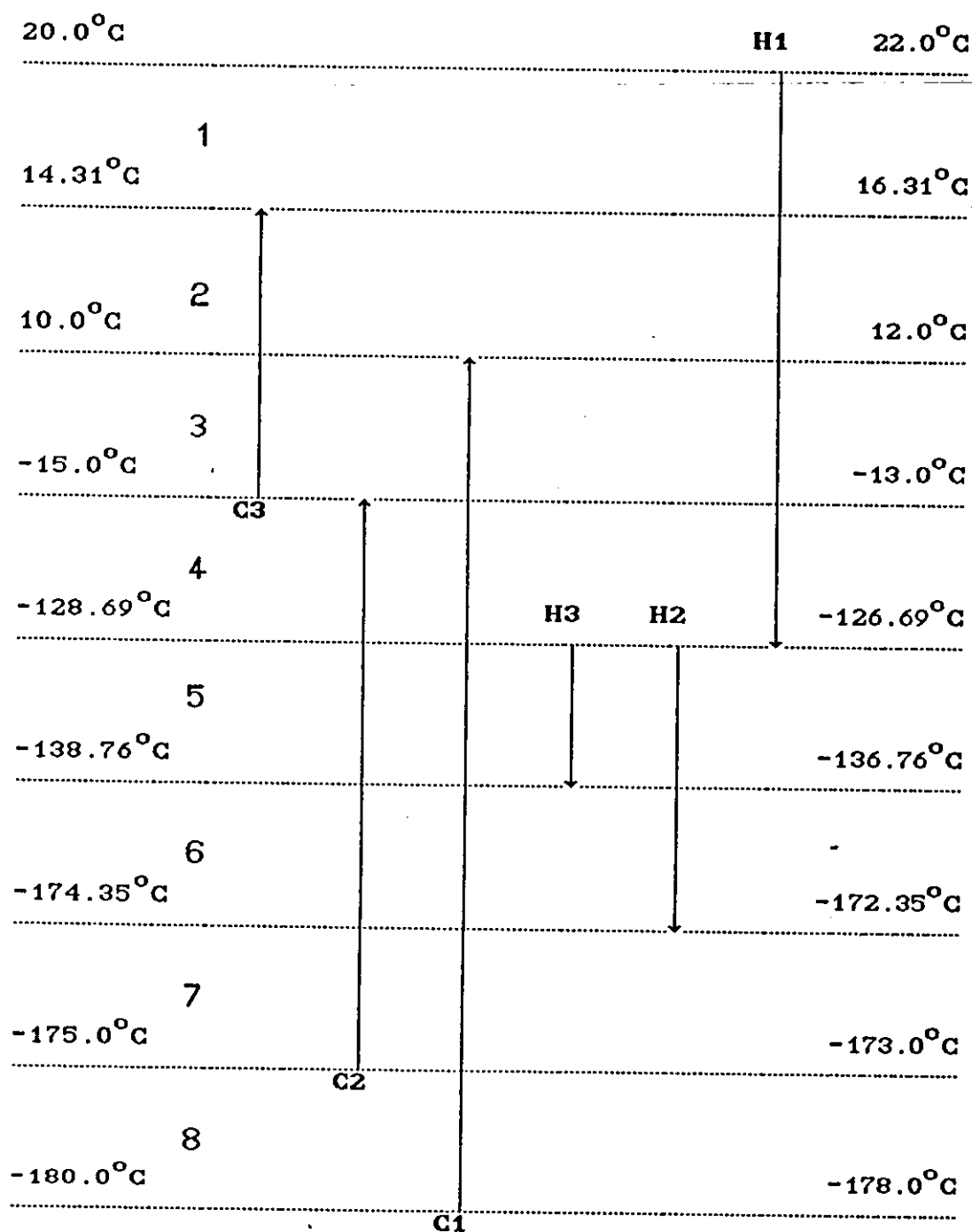


Figure A.3 : Temperature interval analysis

TABLE A.3 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 2.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|-------------------|--------------------|
| 20.0 | 1 | 5.69 | - 0.4151 | -2.3619 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 113.69 | - 0.0315 | -3.5182 | Surplus |
| -128.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -138.76 | 6 | 35.59 | + 0.2364 | +8.4135 | Deficit |
| -174.35 | 7 | 0.65 | + 0.3836 | +0.2647 | Deficit |
| -175.0 | 8 | 5.0 | + 0.1149 | +0.5745 | Deficit |
| -180.0 | | | $E_{\text{min}} = \Sigma$ | 5.8634 | |

$$\Delta T = 3.0^{\circ}\text{C}$$

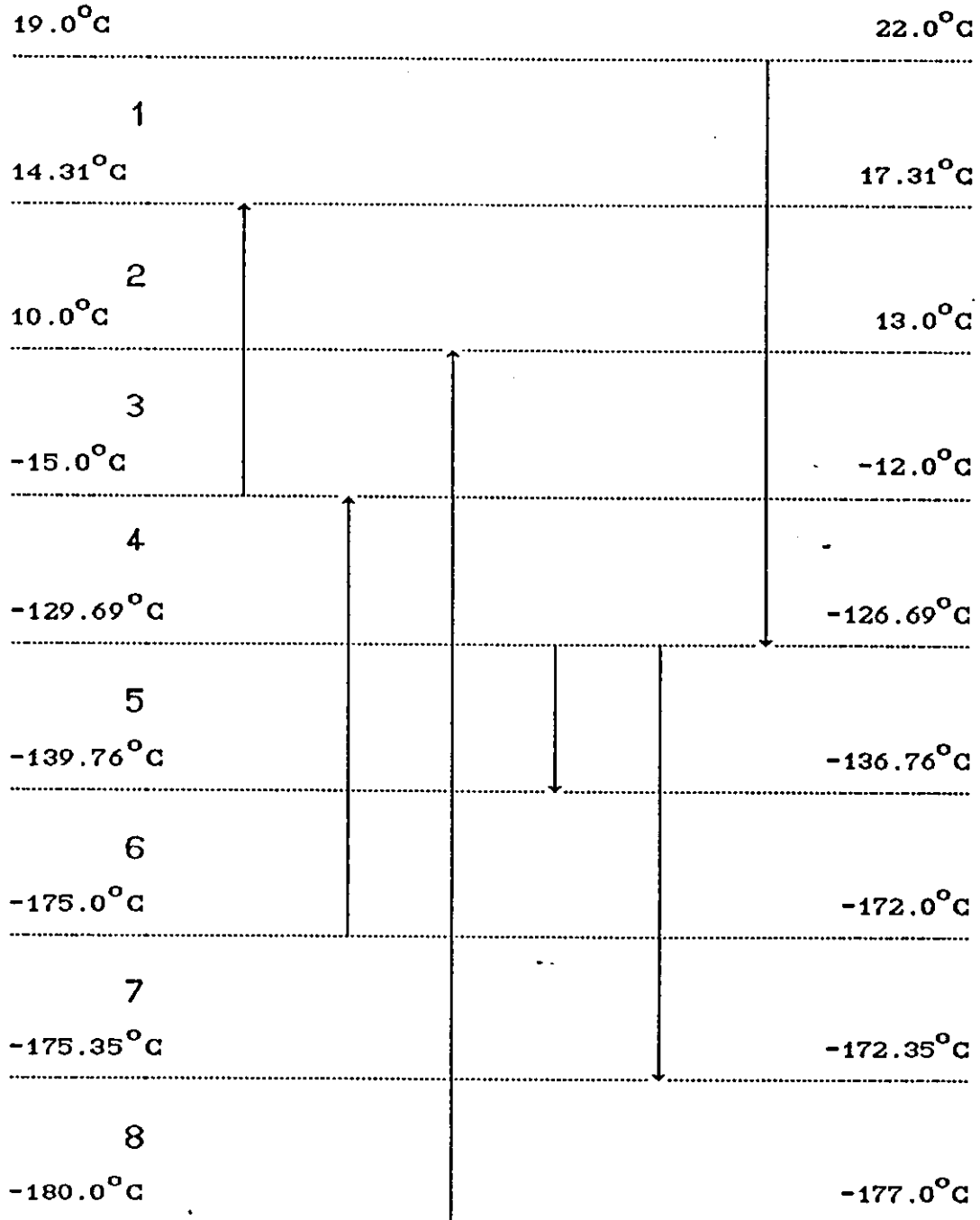


Figure A.4 : Temperature interval analysis

TABLE A.4 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 3.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|-------------------|--------------------|
| 19.0 | 1 | 4.69 | - 0.4151 | -1.9468 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 114.69 | - 0.0315 | -3.6127 | Surplus |
| -129.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -139.76 | 6 | 35.24 | + 0.2364 | +8.3307 | Deficit |
| -175.0 | 7 | 0.35 | - 0.0323 | -0.0113 | Surplus |
| -175.35 | 8 | 4.65 | + 0.1149 | +0.5343 | Deficit |
| -180.0 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.8788 | |

$$\Delta T = 4.0^{\circ}\text{C}$$

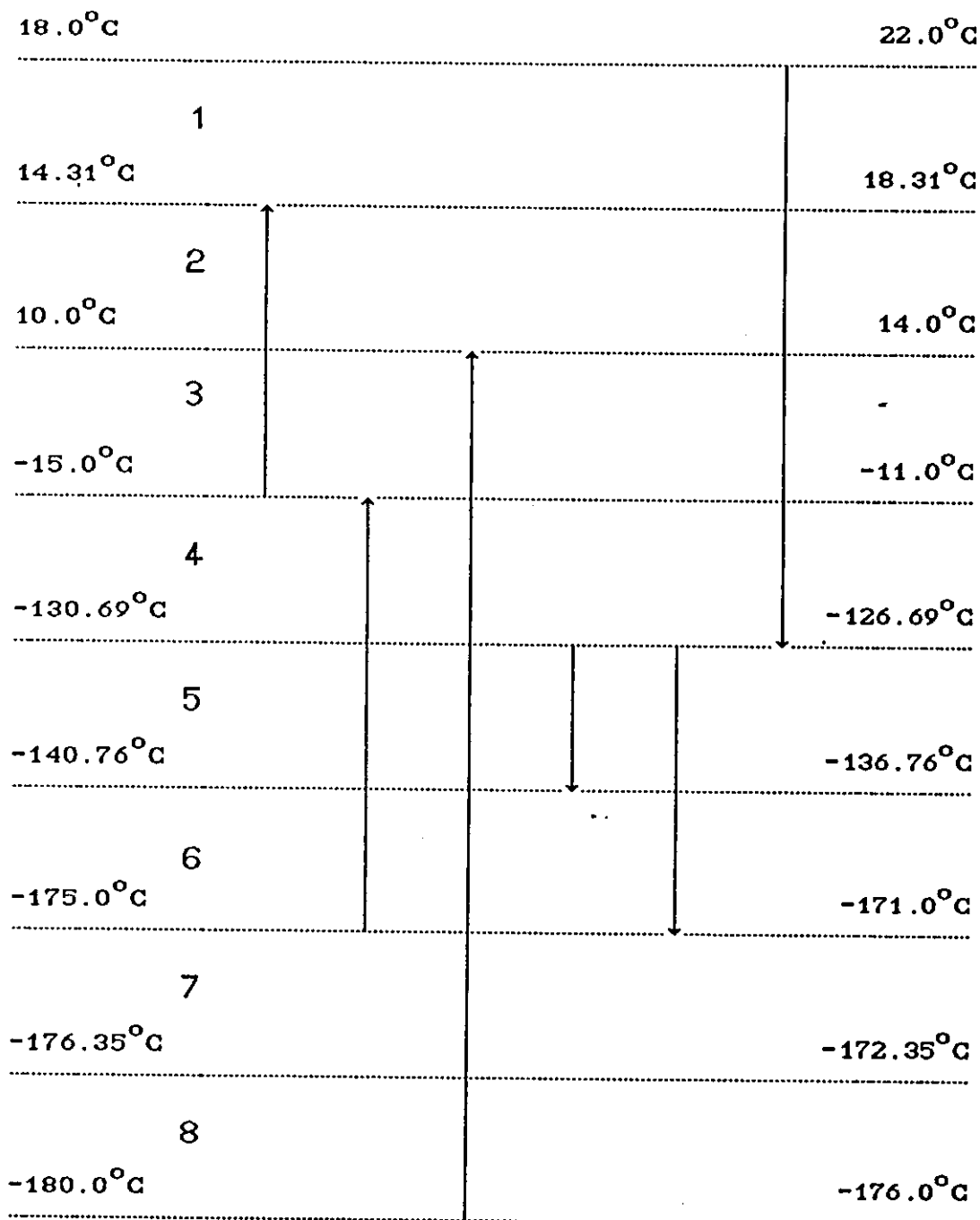


Figure A.5 : Temperature interval analysis

TABLE A.5 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 4.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|------------------------------|--------------------|
| 18.0 | 1 | 3.69 | - 0.4151 | -1.5317 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 115.69 | - 0.0315 | -3.6442 | Surplus |
| -130.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -140.76 | 6 | 34.24 | + 0.2364 | +8.0943 | Deficit |
| -175.0 | 7 | 1.35 | - 0.0323 | -0.0436 | Surplus |
| -176.35 | 8 | 3.65 | + 0.1149 | +0.4194 | Deficit |
| -180.0 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.8788 | |

$$\Delta T = 5.0^{\circ}\text{C}$$

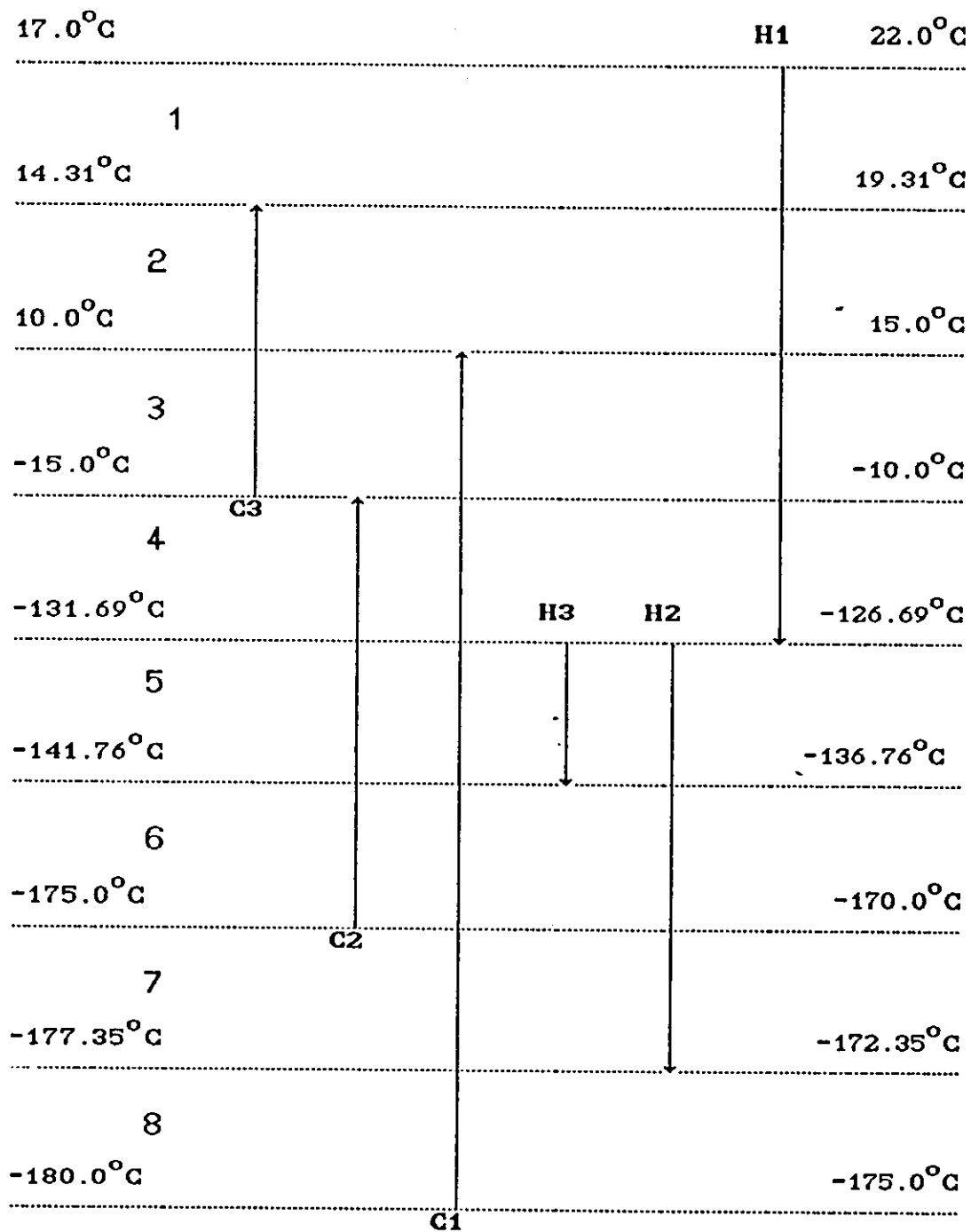


Figure A.6 : Temperature interval analysis

TABLE A.6 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 5.0^{\circ}\text{C}$

| $^{\circ}\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^{\circ}\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^{\circ}\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|--------------------|------------------|--|---|------------------------------|--------------------|
| 17.0 | 1 | 2.69 | - 0.4151 | -1.1166 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 116.69 | - 0.0315 | -3.6757 | Surplus |
| -131.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -141.76 | 6 | 33.24 | + 0.2364 | +7.8579 | Deficit |
| -175.0 | 7 | 2.35 | - 0.0323 | -0.0759 | Surplus |
| -177.35 | 8 | 2.65 | + 0.1149 | +0.3045 | Deficit |
| -180.0 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.8788 | |

$$\Delta T = 6.0^{\circ}\text{C}$$

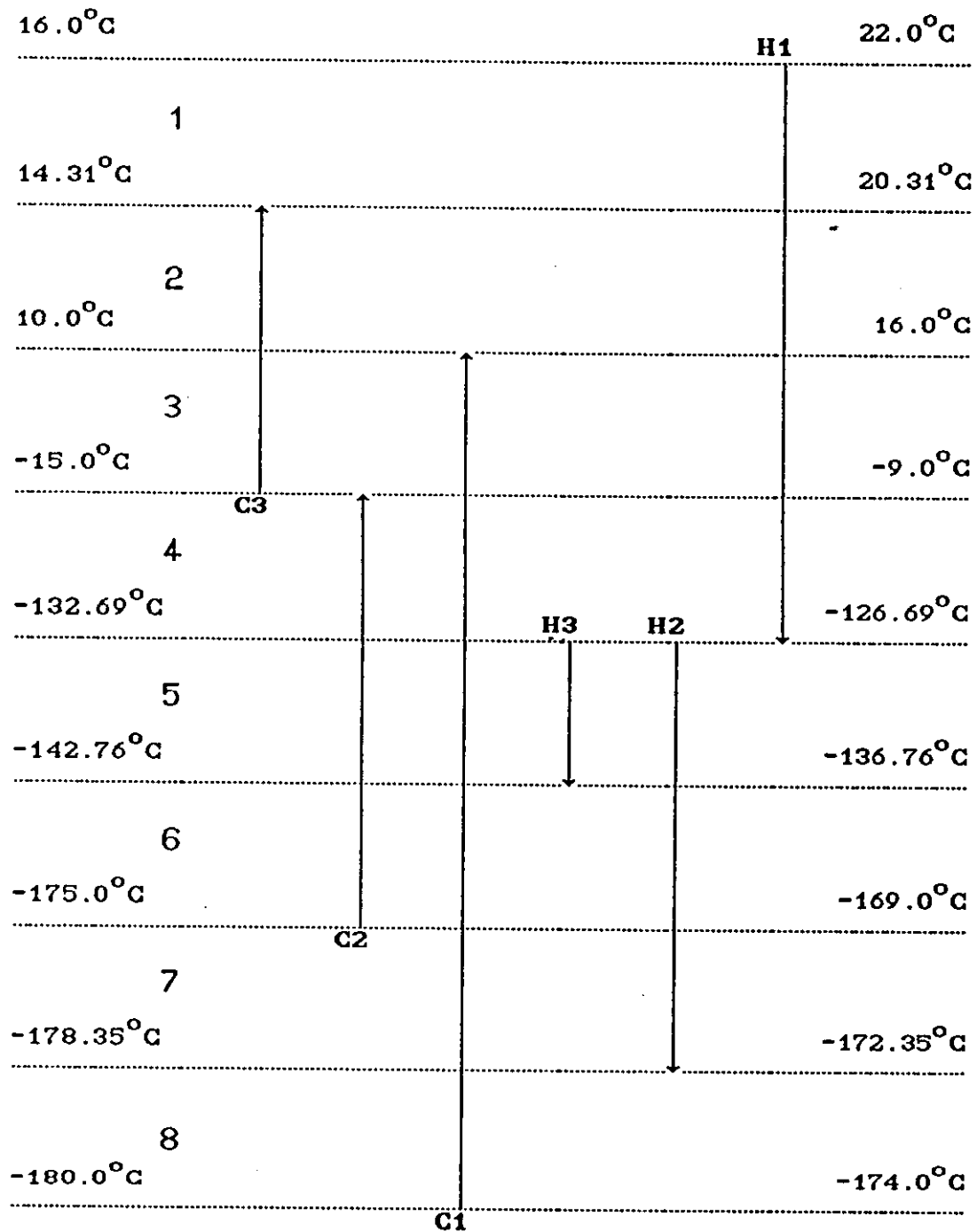


Figure A.7 : Temperature interval analysis

TABLE A.7 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 6.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|-------------------|--------------------|
| 16.0 | | | | | |
| | 1 | 1.69 | - 0.4151 | -0.7015 | Surplus |
| 14.31 | | | | | |
| | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | | | | | |
| | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | | | | | |
| | 4 | 117.69 | - 0.0315 | -3.7072 | Surplus |
| -132.69 | | | | | |
| | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -142.76 | | | | | |
| | 6 | 32.24 | + 0.2364 | +7.6215 | Deficit |
| -175.0 | | | | | |
| | 7 | 3.35 | - 0.0323 | -0.1082 | Surplus |
| -178.35 | | | | | |
| | 8 | 1.65 | + 0.1149 | +0.1896 | Deficit |
| -180.0 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.8788 | |

$$\Delta T = 7.0^{\circ}\text{C}$$

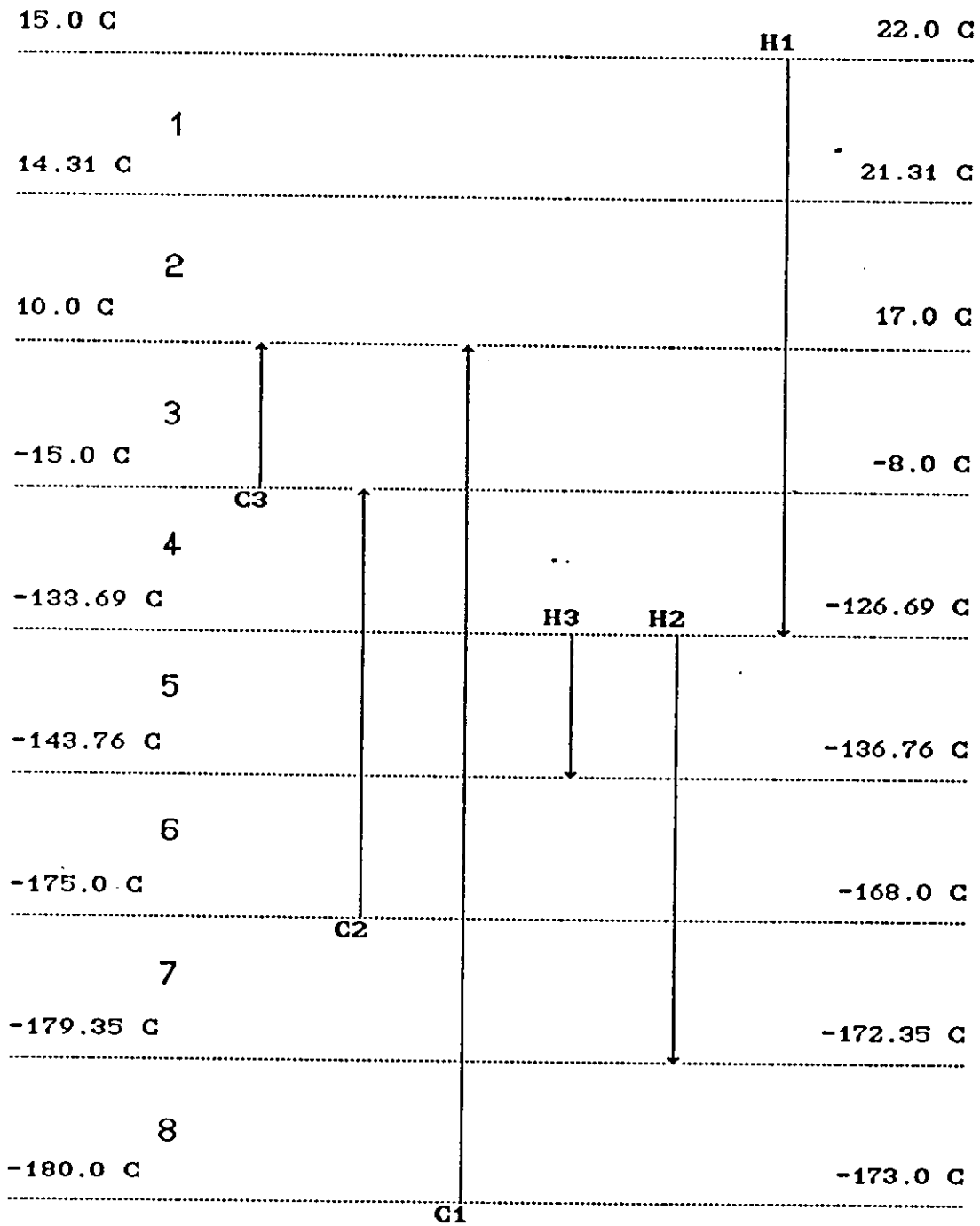


Figure A.8 : Temperature interval analysis

TABLE A.8 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 7.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|-------------------|--------------------|
| 15.0 | 1 | 0.69 | - 0.4151 | -0.2864 | Surplus |
| 14.31 | 2 | 4.31 | - 0.3281 | -1.4141 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 118.69 | - 0.0315 | -3.7387 | Surplus |
| -133.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -143.76 | 6 | 31.24 | + 0.2364 | +7.3851 | Deficit |
| -175.0 | 7 | 4.35 | - 0.0323 | -0.1405 | Surplus |
| -179.35 | 8 | 0.65 | + 0.1149 | +0.0747 | Deficit |
| -180.0 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.8788 | |

$\Delta T = 8.0^{\circ}\text{C}$

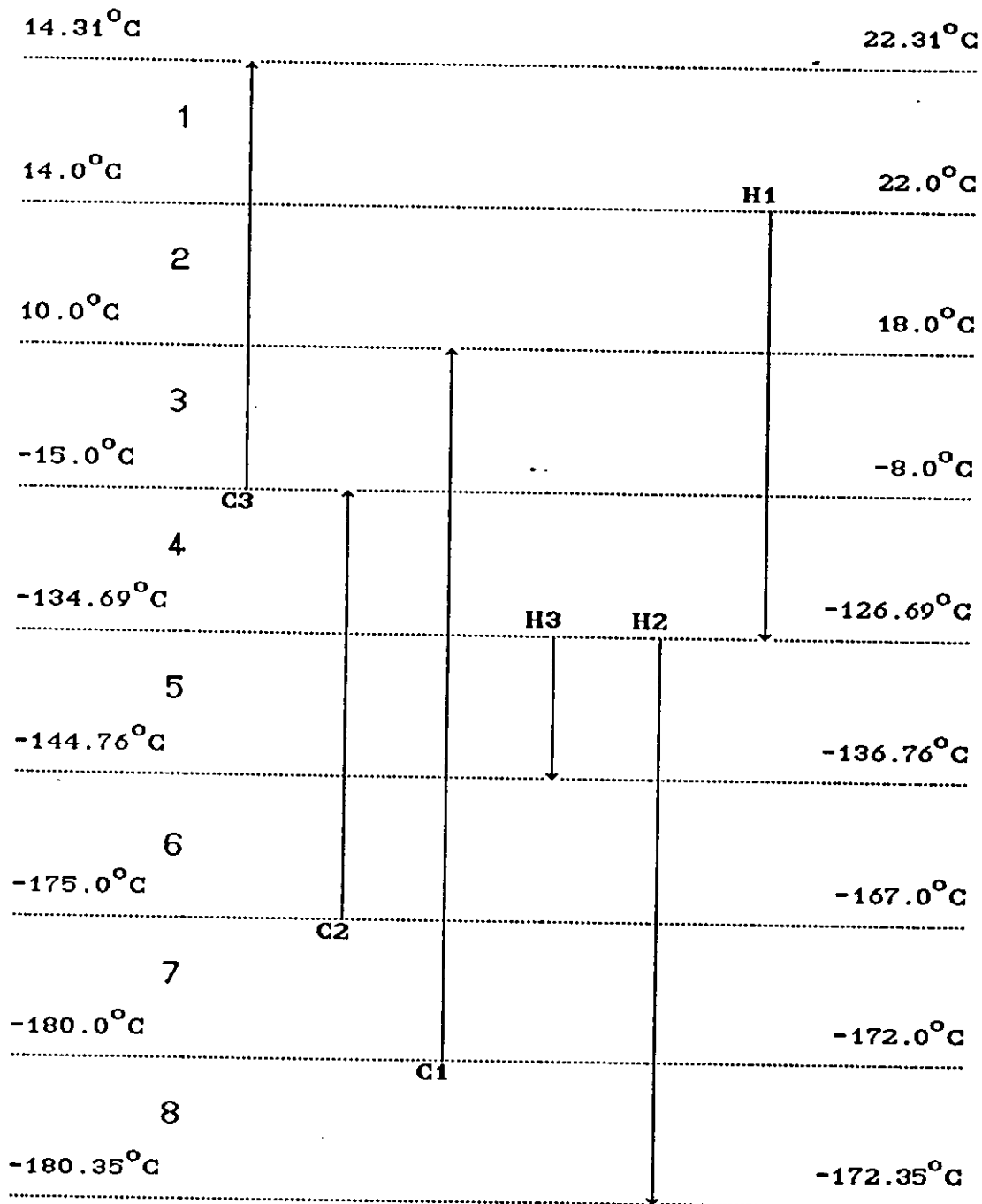


Figure A-9 : Temperature - interval analysis

TABLE A.9 : TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 8.0^{\circ}\text{C}$

| $^{\circ}\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^{\circ}\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^{\circ}\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|--------------------|------------------|--|---|------------------------------|--------------------|
| 14.31 | 1 | 0.31 | + 0.0870 | +0.0270 | Deficit |
| 14.0 | 2 | 4.0 | - 0.3281 | -1.3124 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 119.69 | - 0.0315 | -3.7702 | Surplus |
| -134.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -144.76 | 6 | 30.24 | + 0.2364 | +7.1487 | Deficit |
| -175.0 | 7 | 5.0 | - 0.0323 | -0.1615 | Surplus |
| -180.0 | 8 | 0.35 | - 0.4151 | -0.1453 | Surplus |
| -180.35 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 5.9726 | |

$$\Delta T = 9.0^{\circ}\text{C}$$

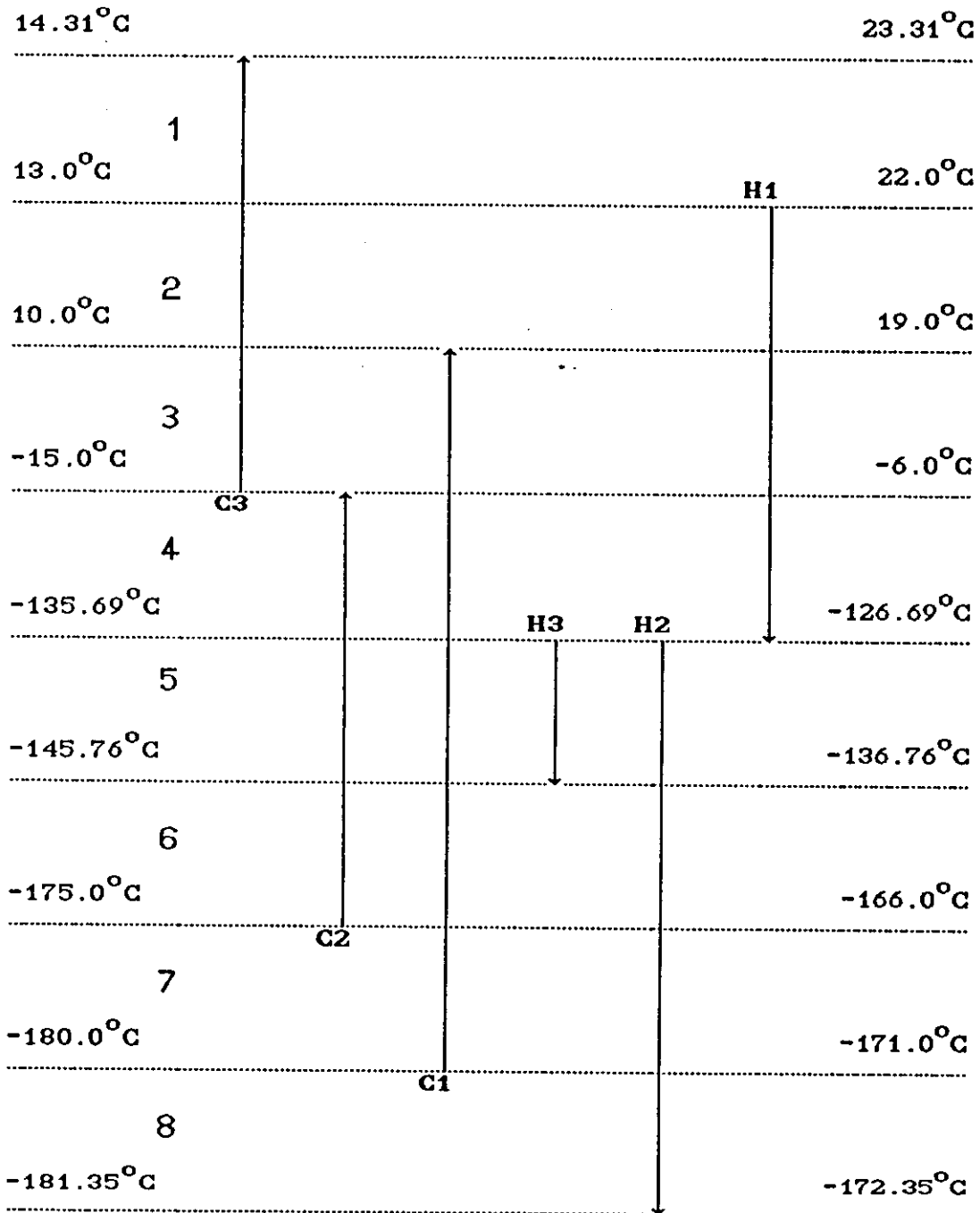


Figure A-10 : Temperature - interval analysis

TABLE A.10: TEMPERATURE-INTERVAL ANALYSIS, $\Delta T = 9.0^\circ\text{C}$

| $^\circ\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^\circ\text{C}$) | $\Sigma CP_{\text{cold}} - \Sigma CP_{\text{hot}}$ ($\text{kW}/^\circ\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|------------------|------------------|--------------------------------------|---|------------------------------|--------------------|
| 14.31 | 1 | 1.31 | + 0.0870 | +0.1140 | Deficit |
| 13.0 | 2 | 3.0 | - 0.3281 | -0.9843 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 120.69 | - 0.0315 | -3.8017 | Surplus |
| -135.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -145.76 | 6 | 29.24 | + 0.2364 | +6.9123 | Deficit |
| -175.0 | 7 | 5.0 | - 0.0323 | -0.1615 | Surplus |
| -180.0 | 8 | 1.35 | - 0.4151 | -0.5604 | Surplus |
| -181.35 | | | | | |
| | | | $E_{\text{min}} = \Sigma$ | 6.2405 | |

$$\Delta T = 10.0^{\circ}\text{C}$$

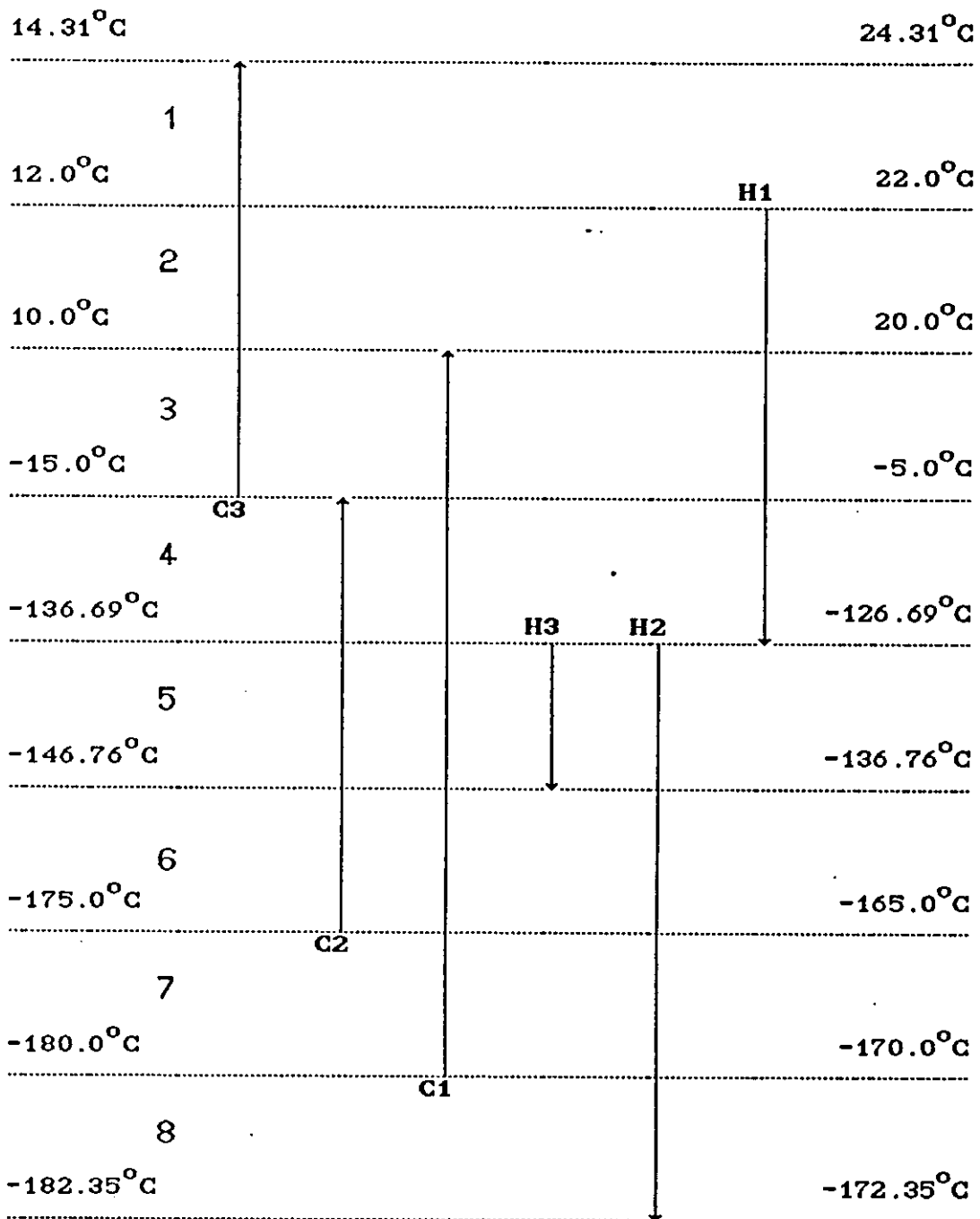


Figure A-11 : Temperature - interval analysis

TABLE A.11: TEMPERATURE-INTERVAL ANALYSIS, $\Delta T=10.0^{\circ}\text{C}$

| $^{\circ}\text{C}$ | Interval No. (i) | $T_i - T_{i+1}$ ($^{\circ}\text{C}$) | $\Sigma \text{CP}_{\text{cold}} - \Sigma \text{CP}_{\text{hot}}$ ($\text{kW}/^{\circ}\text{C}$) | ΔH_i (kW) | Surplus or Deficit |
|--------------------|------------------|--|---|-------------------|--------------------|
| 14.31 | 1 | 2.31 | + 0.0870 | +0.2010 | Deficit |
| 14.0 | 2 | 2.0 | - 0.3281 | -0.6562 | Surplus |
| 10.0 | 3 | 25.0 | - 0.2132 | -5.33 | Surplus |
| -15.0 | 4 | 121.69 | - 0.0315 | -3.8332 | Surplus |
| -136.69 | 5 | 10.07 | - 0.2412 | -2.4289 | Surplus |
| -146.76 | 6 | 28.24 | + 0.2364 | +6.6759 | Deficit |
| -175.0 | 7 | 5.0 | - 0.0323 | -0.1615 | Surplus |
| -180.0 | 8 | 2.35 | - 0.4151 | -0.9755 | Surplus |
| -182.35 | | | $E_{\text{min}} = \Sigma$ | 6.5084 | |

Appendix B

Computer results of the simulating flowsheet of the oxygen plant of type K-0.15

PLANT.REP

CODE: Chemical Engineering Simulation System
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TOPOLOGY

| Equipment | Stream Numbers | | | |
|-----------|----------------|-----|-----|-----|
| 1 ENTM | 1 | -2 | 0 | 0 |
| 2 ENTM | 3 | -4 | 0 | 0 |
| 3 ENTM | 5 | -6 | 0 | 0 |
| 4 ENTM | 7 | -8 | 0 | 0 |
| 5 HXER | 2 | -3 | 0 | 0 |
| 6 HXER | 4 | -5 | 0 | 0 |
| 7 HXER | 6 | -7 | 0 | 0 |
| 8 HXER | 8 | -9 | 0 | 0 |
| 9 HXER | 9 | 48 | -10 | -49 |
| 10 HXER | 10 | 36 | -11 | -38 |
| 11 HXER | 13 | 44 | -15 | -47 |
| 12 HXER | 14 | 45 | -16 | -46 |
| 13 HXER | 11 | -12 | 0 | 0 |
| 14 DVDR | 12 | -13 | -14 | 0 |
| 15 HXER | 46 | 49 | -51 | -36 |
| 16 MIXR | 15 | 16 | -17 | 0 |
| 17 DVDR | 17 | -18 | -19 | 0 |
| 18 ENTM | 19 | -26 | 0 | 0 |
| 19 DVDR | 18 | -20 | -21 | 0 |
| 20 HXER | 43 | 20 | -44 | -23 |
| 21 HXER | 42 | 21 | -45 | -22 |
| 22 MIXR | 23 | 22 | -24 | 0 |
| 23 VALV | 24 | -25 | 0 | 0 |
| 24 TOWR | 25 | 26 | -27 | -28 |
| 25 HXER | 27 | 34 | -29 | -39 |
| 26 HXER | 28 | 39 | -30 | -40 |
| 27 HXER | 31 | 35 | -33 | -37 |
| 28 VALV | 29 | -32 | 0 | 0 |
| 29 VALV | 30 | -31 | 0 | 0 |
| 30 TOWR | 32 | 33 | -34 | -35 |
| 31 PUMP | 37 | -41 | 0 | 0 |
| 32 DVDR | 47 | -48 | -50 | 0 |
| 33 HXER | 40 | -43 | 0 | 0 |
| 34 HXER | 41 | -42 | 0 | 0 |
| 35 MIXR | 38 | 50 | -52 | 0 |

Stream Connections

| Stream | Equipment | |
|--------|-----------|----|
| | From | To |
| 1 | 0 | 1 |
| 2 | 1 | 5 |
| 3 | 5 | 2 |
| 4 | 2 | 6 |
| 5 | 6 | 3 |
| 6 | 3 | 7 |

CODE REPORT

Stream Connections

| Stream | Equipment | |
|--------|-----------|----|
| | From | To |
| 7 | 7 | 4 |
| 8 | 4 | 8 |
| 9 | 8 | 9 |
| 10 | 9 | 10 |
| 11 | 10 | 13 |
| 12 | 13 | 14 |
| 13 | 14 | 11 |
| 14 | 14 | 12 |
| 15 | 11 | 16 |
| 16 | 12 | 16 |
| 17 | 16 | 17 |
| 18 | 17 | 19 |
| 19 | 17 | 18 |
| 20 | 19 | 20 |
| 21 | 19 | 21 |
| 22 | 21 | 22 |
| 23 | 20 | 22 |
| 24 | 22 | 23 |
| 25 | 23 | 24 |
| 26 | 18 | 24 |
| 27 | 24 | 25 |
| 28 | 24 | 26 |
| 29 | 25 | 28 |
| 30 | 26 | 29 |
| 31 | 29 | 27 |
| 32 | 28 | 30 |
| 33 | 27 | 30 |
| 34 | 30 | 25 |
| 35 | 30 | 27 |
| 36 | 15 | 10 |
| 37 | 27 | 31 |
| 38 | 10 | 35 |
| 39 | 25 | 26 |
| 40 | 26 | 33 |
| 41 | 31 | 34 |
| 42 | 34 | 21 |
| 43 | 33 | 20 |
| 44 | 20 | 11 |
| 45 | 21 | 12 |
| 46 | 12 | 15 |
| 47 | 11 | 32 |
| 48 | 32 | 9 |
| 49 | 9 | 15 |
| 50 | 32 | 35 |
| 51 | 15 | 0 |
| 52 | 35 | 0 |

COMPONENTS 2
 ID numbers 46, 47,
 CODE REPORT

THERMODYNAMICS

Kvalue option: Peng-Robinson
 Enthalpy option: Peng-Robinson

MISCELLANEOUS

Recycle calculations are converged.

Recycle equipment list (KE2): 13, 14, 17, 18, 19, 33, 20, 11,
 31, 34, 21, 22, 23, 24, 12, 15,
 25, 26, 28, 29, 27, 30,

Streams used in conv. routine (KE4):(0)
 ()=Delay factor

Preferred cut stream list (KE3): 11, 17, 40, 37, 34, 35,

Convergence tolerances, Error
 Flowrates: .00100000
 Vapor fraction: .00100000
 Temperature: .00100000
 Pressure: .00100000
 Enthalpy: .00100000
 Flash calcs: .00005000

Max. loops in recycle calc.: 30
 in flash calcs: 75

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*** DIVIDERS ***

| Equipment no. | 14 | 17 | 19 | 32 |
|---------------|--------|--------|--------|--------|
| External name | | | | |
| Fraction/flow | | | | |
| 1 | .68750 | .40000 | .71000 | .33000 |
| 2 | .31250 | .60000 | .29000 | .67000 |
| 3 | .00000 | .00000 | .00000 | .00000 |
| 4 | .00000 | .00000 | .00000 | .00000 |
| 5 | .00000 | .00000 | .00000 | .00000 |
| 6 | .00000 | .00000 | .00000 | .00000 |
| Mode | .0 | .0 | .0 | .0 |
| Stream # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |
| Comp. ID # | .0 | .0 | .0 | .0 |

.....

*** MIXERS-W/FLASH ***

| Equipment no. | 16 | 22 | 35 |
|---------------|----|----|----|
| External name | | | |

.....

*** VALVES ***

| Equipment no. | 23 | 28 | 29 | 140 |
|----------------------|--------|--------|--------|-----|
| External name | | | | |
| Outlet pressure bars | 6.6132 | 1.4006 | 1.4572 | |

*****EXCHANGER/CONDENSERS****

| Equipment no. | 5 | 6 | 7 | 8 |
|-----------------------|---------|---------|---------|---------|
| External name | | | | |
| Heat transfer coeff. | .00000 | .00000 | .00000 | .00000 |
| Area | .00000 | .00000 | .00000 | .00000 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 5.0 | 5.0 | 5.0 | 5.0 |
| Min. delta T or T-out | 20.00 | 20.00 | 20.00 | 22.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | -158.52 | -183.56 | -164.72 | -106.13 |
| Water usage, DM3/hr | .00000 | .00000 | .00000 | .00000 |
| Corrected delta T | .00 | .00 | .00 | .00 |
| Equipment no. | 9 | 10 | 11 | 12 |
| External name | | | | |
| Heat transfer coeff. | 300.00 | 300.00 | 300.00 | 300.00 |
| Area | 1.5385 | 4.4356 | 15.772 | 6.3643 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 3.0 | 3.0 | 3.0 | 3.0 |
| Min. delta T or T-out | 10.00 | 1.00 | 25.00 | 28.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | -8.4539 | -9.8046 | -142.49 | -64.454 |
| Water usage, DM3/hr | .00000 | .00000 | .00000 | .00000 |
| Corrected delta T | 18.32 | 7.37 | 30.11 | 33.76 |
| Equipment no. | 13 | 15 | 20 | 21 |
| External name | | | | |
| Heat transfer coeff. | .00000 | 300.00 | 300.00 | 300.00 |
| Area | .00000 | 20.847 | 1.1028 | .40436 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 5.0 | 3.0 | 3.0 | 3.0 |
| Min. delta T or T-out | 10.00 | 1.00 | 36.00 | 40.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | 3.0318 | 9.0809 | 12.279 | 5.0450 |
| Water usage, DM3/hr | .00000 | .00000 | .00000 | .00000 |
| Corrected delta T | 8.63 | 1.45 | 37.11 | 41.59 |
| Equipment no. | 25 | 26 | 27 | 33 |
| External name | | | | |
| Heat transfer coeff. | 300.00 | 300.00 | 300.00 | .00000 |
| Area | 5.7545 | 5.8885 | .53237 | .00000 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 3.0 | 3.0 | 3.0 | 5.0 |
| Min. delta T or T-out | 6.00 | 3.00 | 7.00 | -175.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | -10.610 | -7.1362 | 1.3775 | .15206 |

| | | | | | |
|-----------------------|---------|---------|---------|--------|-----|
| Water usage, DM3/hr | .00000 | 1.00000 | 1.00000 | .00000 | 111 |
| Corrected delta T | 6.15 | 4.04 | 8.63 | 8.63 | |
| Equipment no. | 34 | | | | |
| External name | | | | | |
| Heat transfer coeff. | .00000 | | | | |
| Area | .00000 | | | | |
| Number of shells | .0 | | | | |
| Shell passes | .0 | | | | |
| Tube passes | .0 | | | | |
| Mode | 5.0 | | | | |
| Min. delta T or T-out | -180.00 | | | | |
| Delta P, stream 1 | .00000 | | | | |
| Delta P, stream 2 | .00000 | | | | |
| Q, stream 1 MJ/hr | 1.1303 | | | | |
| Water usage, DM3/hr | .00000 | | | | |
| Corrected delta T | 18.32 | | | | |

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*** PUMPS/COMPRESSORS ***

| | |
|-----------------------|--------|
| Equipment no. | 31 |
| External name | |
| Number of stages | .0 |
| Work capacity MJ/hr | .00000 |
| Outlet pressure bars | 190.00 |
| Power type: | .0 |
| (+) steam | |
| (0) electricity | |
| (-) fuel gas | |
| H, steam out KJ / kg | .00000 |
| Fuel usage, M3 /hr | .00000 |
| Water usage, DM3/hr | .00000 |
| Steam usage Tonnes/hr | .00000 |
| Kilowatt usage | 1.1632 |

*** ENTROPY MACHINES ***

| Equipment no. | 1 | 2 | 3 | 4 |
|----------------------|---------|--------|--------|--------|
| External name | | | | |
| Mode | .0 | .0 | .0 | .0 |
| Outlet pressure bars | 2.7100 | 8.2300 | 22.300 | 43.600 |
| Adiabatic efficiency | .70000 | .70000 | .70000 | .70000 |
| Theoretical hp | 41.181 | 47.389 | 41.786 | 26.671 |
| Actual horsepower | 58.831 | 67.699 | 59.694 | 38.101 |
| Entropy in KJ/deg C | 1140.9 | 812.34 | 438.03 | 94.006 |
| Entropy out, ideal | 1140.9 | 812.33 | 438.02 | 93.919 |
| Entropy out, actual | 1257.2 | 940.77 | 555.43 | 177.31 |
| Equipment no. | 18 | | | |
| External name | | | | |
| Mode | .0 | | | |
| Outlet pressure bars | 6.6065 | | | |
| Adiabatic efficiency | .85000 | | | |
| Theoretical hp | -10.517 | | | |
| Actual horsepower | -8.9396 | | | |
| Entropy in KJ/deg C | -733.70 | | | |
| Entropy out, ideal | -733.72 | | | |

Entropy out, actual -693.70

142

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*** RIGOROUS TOWERS ***

| Equipment no. | 24 | 30 |
|------------------------|------------|---------|
| External name | | |
| Number of stages | 21.0 | 57.0 |
| Feed 1, stage # | 15.0 | 1.0 |
| Feed 2, stage # | 21.0 | 17.0 |
| Feed 3, stage # | .0 | .0 |
| Feed 4, stage # | .0 | .0 |
| Feed 5, stage # | .0 | .0 |
| Sidestream # 1 stage | .0 | .0 |
| Sidestream # 2 stage | .0 | .0 |
| Sidestream # 3 stage | .0 | .0 |
| Sidestream # 4 stage | .0 | .0 |
| Cond. pressure bars | 6.7131 | 1.4006 |
| Cond. delta P bars | .00000 | .00000 |
| Colm. delta P bars | .19400E-01 | .19850 |
| Condenser type | .0 | 1.0 |
| Condenser mode | 4.0 | .0 |
| Value of cond. spec. | 16.000 | .00000 |
| Cond comp 1 position | 1.0 | .0 |
| Cond comp 2 position | .0 | .0 |
| Cond. deg. subcooled | 1.00 | .00 |
| Reboiler mode | .0 | 4.0 |
| Val. of reboiler spec | .00000 | 7.6000 |
| Rebr comp 1 position | .0 | 2.0 |
| Rebr comp 2 position | .0 | .0 |
| Damping ratio | .00000 | 1.0000 |
| Sidestream 1 mode | .0 | .0 |
| Sidestream 2 mode | .0 | .0 |
| Sidestream 3 mode | .0 | .0 |
| Sidestream 4 mode | .0 | .0 |
| Sidestream # 1 spec | .00000 | .00000 |
| Sidestream # 2 spec | .00000 | .00000 |
| Sidestream # 3 spec | .00000 | .00000 |
| Sidestream # 4 spec | .00000 | .00000 |
| Sidestrm 1 comp posn | .0 | .0 |
| Sidestrm 2 comp posn | .0 | .0 |
| Sidestrm 3 comp posn | .0 | .0 |
| Sidestrm 4 comp posn | .0 | .0 |
| Cond. duty MJ/hr | -163.51 | .00000 |
| Rebr duty MJ/hr | .00000 | 153.21 |
| Est dist rate Kgmol/hr | 16.000 | .00000 |
| Est. reflux Kgmol/hr | .00000 | .00000 |
| Est. side draw rate 1 | .00000 | .00000 |
| Est. side draw rate 2 | .00000 | .00000 |
| Est. side draw rate 3 | .00000 | .00000 |
| Est. side draw rate 4 | .00000 | .00000 |
| Est. temp stg 1 C | -178.00 | -193.00 |
| Est. temp stg N C | -174.00 | -183.00 |

CODEREPORT

*** Stream no. 1 ***

| | | |
|--------------------------------------|----------|-------------|
| | | All Vapor |
| Temperature deg C. | | 20.0000 |
| Pressure bars. | | 1.01325 |
| Enthalpy MJ/hr | | 812.759 |
| Entropy MJ/hr*K | | 1.14091 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m3 | | 1.19674 |
| Viscosity centipoise | | .180405E-01 |
| Thermal cond. cal/cm*s*K | | .628029E-04 |
| Specific heat kJ/kg*K | | 1.01667 |
| Z factor | | .999419 |
| m3/hr (15.6 deg C & 1 atm) | | 947.608 |
| Vol. flowrate m3/hr | | 961.641 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 32.4000 |
| Oxygen | .190000 | 7.60000 |

*** Stream no. 2 ***

| | | |
|--------------------------------------|----------|-------------|
| | | All Vapor |
| Temperature deg C. | | 154.633 |
| Pressure bars. | | 2.71000 |
| Enthalpy MJ/hr | | 970.718 |
| Entropy MJ/hr*K | | 1.25721 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m3 | | 2.19114 |
| Viscosity centipoise | | .239542E-01 |
| Thermal cond. cal/cm*s*K | | .907807E-04 |
| Specific heat kJ/kg*K | | 1.02916 |
| Z factor | | 1.00045 |
| m3/hr (15.6 deg C & 1 atm) | | 947.608 |
| Vol. flowrate m3/hr | | 525.220 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 32.4000 |
| Oxygen | .190000 | 7.60000 |

CODE REPORT

*** Stream no. 3 ***

| | | |
|------------------------------------|--|-------------|
| | | All Vapor |
| Temperature deg C. | | 20.0000 |
| Pressure bars. | | 2.71000 |
| Enthalpy MJ/hr | | 812.202 |
| Entropy MJ/hr*K | | .812340 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m3 | | 3.20381 |
| Viscosity centipoise | | .180405E-01 |
| Thermal cond. cal/cm*s*K | | .628029E-04 |
| Specific heat kJ/kg*K | | 1.02047 |
| Z factor | | .998463 |

| | |
|--|----------|
| m ³ /hr (15.6 deg C & 1 atm) . | 947.608 |
| Vol. flowrate m ³ /hr | 359.206 |
| Vapor | Vapor |
| mole | flowrate |
| fraction | kgmol/hr |
| Nitrogen .810000 | 32.4000 |
| Oxygen .190000 | 7.60000 |

*** Stream no. 4 ***

| | | |
|--|-----------|-------------|
| Temperature deg C. | All Vapor | 174.770 |
| Pressure bars. | | 8.23000 |
| Enthalpy MJ/hr | | 993.971 |
| Entropy MJ/hr*K | | .940765 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m ³ | | 6.34707 |
| Viscosity centipoise | | .247552E-01 |
| Thermal cond. cal/cm*s*K | | .957600E-04 |
| Specific heat kJ/kg*K | | 1.03568 |
| Z factor | | 1.00172 |
| m ³ /hr (15.6 deg C & 1 atm) . | | 947.608 |
| Vol. flowrate m ³ /hr | | 181.317 |
| Vapor | Vapor | |
| mole | flowrate | |
| fraction | kgmol/hr | |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

CODE REPORT

*** Stream no. 5 ***

| | | |
|--|-----------|-------------|
| Temperature deg C. | All Vapor | 20.0000 |
| Pressure bars. | | 8.23000 |
| Enthalpy MJ/hr | | 810.408 |
| Entropy MJ/hr*K | | .438028 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m ³ | | 9.75871 |
| Viscosity centipoise | | .180405E-01 |
| Thermal cond. cal/cm*s*K | | .628029E-04 |
| Specific heat kJ/kg*K | | 1.03134 |
| Z factor | | .995489 |
| m ³ /hr (15.6 deg C & 1 atm) . | | 947.608 |
| Vol. flowrate m ³ /hr | | 117.928 |
| Vapor | Vapor | |
| mole | flowrate | |
| fraction | kgmol/hr | |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

*** Stream no. 6 ***

| | | |
|----------------------------|-----------|---------|
| Temperature deg C. | All Vapor | 156.639 |
| Pressure bars. | | 22.3000 |
| Enthalpy MJ/hr | | 970.685 |
| Entropy MJ/hr*K | | .555435 |
| Ave. mol. wt. | | 28.7703 |

| | | |
|---|-------------|----------|
| Total flow kg/hr. | 1150.81 | |
| kgmol/hr | 40.0000 | |
| Density kg/m ³ | 17.8789 | |
| Viscosity centipoise | .240468E-01 | |
| Thermal cond. cal/cm*s*K | .912667E-04 | |
| Specific heat kJ/kg*K | 1.04437 | |
| Z factor | 1.00422 | |
| m ³ /hr (15.6 deg C & 1 atm) | 947.608 | |
| Vol. flowrate m ³ /hr | 64.3682 | |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

CODE REPORT

*** Stream no. 7 ***

| | | |
|---|-------------|-----------|
| | | All Vapor |
| Temperature deg C. | 20.0000 | |
| Pressure bars. | 22.3000 | |
| Enthalpy MJ/hr | 805.964 | |
| Entropy MJ/hr*K | .940061E-01 | |
| Ave. mol. wt. | 28.7703 | |
| Total flow kg/hr. | 1150.81 | |
| kgmol/hr | 40.0000 | |
| Density kg/m ³ | 26.6192 | |
| Viscosity centipoise | .180657E-01 | |
| Thermal cond. cal/cm*s*K | .628029E-04 | |
| Specific heat kJ/kg*K | 1.05903 | |
| Z factor | .988871 | |
| m ³ /hr (15.6 deg C & 1 atm) | 947.608 | |
| Vol. flowrate m ³ /hr | 43.2331 | |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

*** Stream no. 8 ***

| | | |
|---|-------------|-----------|
| | | All Vapor |
| Temperature deg C. | 107.532 | |
| Pressure bars. | 43.6000 | |
| Enthalpy MJ/hr | 908.265 | |
| Entropy MJ/hr*K | .177305 | |
| Ave. mol. wt. | 28.7703 | |
| Total flow kg/hr. | 1150.81 | |
| kgmol/hr | 40.0000 | |
| Density kg/m ³ | 39.4742 | |
| Viscosity centipoise | .220565E-01 | |
| Thermal cond. cal/cm*s*K | .799859E-04 | |
| Specific heat kJ/kg*K | 1.06555 | |
| Z factor | 1.00399 | |
| m ³ /hr (15.6 deg C & 1 atm) | 947.608 | |
| Vol. flowrate m ³ /hr | 29.1540 | |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

CODE REPORT

*** Stream no. 9 ***

| | | All Vapor |
|----------------------------|---------------------|-------------------------|
| Temperature deg C. | | 22.0000 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 802.137 |
| Entropy MJ/hr*K | | -.138655 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| | kgmol/hr | 40.0000 |
| Density kg/m3 | | 52.0371 |
| Viscosity centipoise | | .182234E-01 |
| Thermal cond. cal/cm*s*K | | .631572E-04 |
| Specific heat kJ/kg*K | | 1.09814 |
| Z factor | | .982313 |
| m3/hr (15.6 deg C & 1 atm) | | 947.608 |
| Vol. flowrate m3/hr | | 22.1156 |
| | Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen | .810000 | 32.4000 |
| Oxygen | .190000 | 7.60000 |

*** Stream no. 10 ***

| | | All Vapor |
|----------------------------|---------------------|-------------------------|
| Temperature deg C. | | 15.3137 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 793.683 |
| Entropy MJ/hr*K | | -.167679 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| | kgmol/hr | 40.0000 |
| Density kg/m3 | | 53.4060 |
| Viscosity centipoise | | .179041E-01 |
| Thermal cond. cal/cm*s*K | | .619794E-04 |
| Specific heat kJ/kg*K | | 1.10248 |
| Z factor | | .979320 |
| m3/hr (15.6 deg C & 1 atm) | | 947.608 |
| Vol. flowrate m3/hr | | 21.5487 |
| | Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen | .810000 | 32.4000 |
| Oxygen | .190000 | 7.60000 |

CODE REPORT

*** Stream no. 11 ***

| | | All Vapor |
|--------------------------|----------|-------------|
| Temperature deg C. | | 7.59766 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 783.879 |
| Entropy MJ/hr*K | | -.202191 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| | kgmol/hr | 40.0000 |
| Density kg/m3 | | 55.0894 |
| Viscosity centipoise | | .175318E-01 |
| Thermal cond. cal/cm*s*K | | .606436E-04 |
| Specific heat kJ/kg*K | | 1.10845 |
| Z factor | | .975487 |

m3/hr (15.6 deg C & 1 atm) . 947.608
 Vol. flowrate m3/hr 20.8902
 Vapor Vapor
 mole flowrate
 fraction kgmol/hr
 Nitrogen .810000 32.4000
 Oxygen .190000 7.60000

*** Stream no. 12 ***

All Vapor
 Temperature deg C. 10.0000
 Pressure bars. 43.6000
 Enthalpy MJ/hr 786.911
 Entropy MJ/hr*K -.191324
 Ave. mol. wt. 28.7703
 Total flow kg/hr. 1150.81
 kgmol/hr 40.0000
 Density kg/m3 54.5527
 Viscosity centipoise176482E-01
 Thermal cond. cal/cm*s*K610568E-04
 Specific heat kJ/kg*K 1.10737
 Z factor976727
 m3/hr (15.6 deg C & 1 atm) . 947.608
 Vol. flowrate m3/hr 21.0957
 Vapor Vapor
 mole flowrate
 fraction kgmol/hr
 Nitrogen .810000 32.4000
 Oxygen .190000 7.60000
 CODE REPORT

*** Stream no. 13 ***

All Vapor
 Temperature deg C. 10.0000
 Pressure bars. 43.6000
 Enthalpy MJ/hr 541.001
 Entropy MJ/hr*K -.131536
 Ave. mol. wt. 28.7703
 Total flow kg/hr. 791.184
 kgmol/hr 27.5000
 Density kg/m3 54.5527
 Viscosity centipoise176482E-01
 Thermal cond. cal/cm*s*K610568E-04
 Specific heat kJ/kg*K 1.10752
 Z factor976727
 m3/hr (15.6 deg C & 1 atm) . 651.480
 Vol. flowrate m3/hr 14.5033
 Vapor Vapor
 mole flowrate
 fraction kgmol/hr
 Nitrogen .810000 22.2750
 Oxygen .190000 5.22500

*** Stream no. 14 ***

All Vapor
 Temperature deg C. 10.0000
 Pressure bars. 43.6000
 Enthalpy MJ/hr 245.910
 Entropy MJ/hr*K -.597889E-01
 Ave. mol. wt. 28.7703

| | |
|--------------------------------------|-------------|
| Total flow kg/hr. | 359.629 |
| kgmol/hr , | 12.5000 |
| Density kg/m3 | 54.5527 |
| Viscosity centipoise | .176482E-01 |
| Thermal cond. cal/cm*s*K | .610568E-04 |
| Specific heat kJ/kg*K | 1.10704 |
| Z factor | .976727 |
| m3/hr (15.6 deg C & 1 atm) | 296.127 |
| Vol. flowrate m3/hr | 6.59242 |
| | Vapor |
| | mole |
| | fraction |
| Nitrogen .810000 | 10.1250 |
| Oxygen .190000 | 2.37500 |
| CODE REPORT | |

*** Stream no. 15 ***

| | |
|--------------------------------------|-------------|
| | All Vapor |
| Temperature deg C. | -126.812 |
| Pressure bars. | 43.6000 |
| Enthalpy MJ/hr | 398.507 |
| Entropy MJ/hr*K | -.842187 |
| Ave. mol. wt. | 28.7703 |
| Total flow kg/hr. | 791.184 |
| kgmol/hr | 27.5000 |
| Density kg/m3 | 166.452 |
| Viscosity centipoise | .106017E-01 |
| Thermal cond. cal/cm*s*K | .409996E-04 |
| Specific heat kJ/kg*K | 2.37539 |
| Z factor | .619385 |
| m3/hr (15.6 deg C & 1 atm) | 651.480 |
| Vol. flowrate m3/hr | 4.75330 |
| | Vapor |
| | mole |
| | fraction |
| Nitrogen .810000 | 22.2750 |
| Oxygen .190000 | 5.22500 |

*** Stream no. 16 ***

| | |
|--------------------------------------|-------------|
| | All Vapor |
| Temperature deg C. | -126.440 |
| Pressure bars. | 43.6000 |
| Enthalpy MJ/hr | 181.456 |
| Entropy MJ/hr*K | -.380657 |
| Ave. mol. wt. | 28.7703 |
| Total flow kg/hr. | 359.629 |
| kgmol/hr | 12.5000 |
| Density kg/m3 | 164.835 |
| Viscosity centipoise | .106149E-01 |
| Thermal cond. cal/cm*s*K | .410453E-04 |
| Specific heat kJ/kg*K | 2.33661 |
| Z factor | .623874 |
| m3/hr (15.6 deg C & 1 atm) | 296.127 |
| Vol. flowrate m3/hr | 2.18179 |
| | Vapor |
| | mole |
| | fraction |
| Nitrogen .810000 | 10.1250 |
| Oxygen .190000 | 2.37500 |
| CODE REPORT | |

*** Stream no. 17 ***

| | | |
|--------------------------------------|--------------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -126.696 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 579.963 |
| Entropy MJ/hr*K | | -1.22284 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| | kgmol/hr | 40.0000 |
| Density kg/m3 | | 165.942 |
| Viscosity centipoise | | .106058E-01 |
| Thermal cond. cal/cm*s*K | | .410139E-04 |
| Specific heat kJ/kg*K | | 2.36246 |
| Z factor | | .620796 |
| m3/hr (15.6 deg C & 1 atm) | | 947.608 |
| Vol. flowrate m3/hr | | 6.93515 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 32.4000 |
| Oxygen | .190000 | 7.60000 |

*** Stream no. 18 ***

| | | |
|--------------------------------------|--------------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -126.695 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 231.985 |
| Entropy MJ/hr*K | | -.489127 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 460.325 |
| | kgmol/hr | 16.0000 |
| Density kg/m3 | | 165.937 |
| Viscosity centipoise | | .106058E-01 |
| Thermal cond. cal/cm*s*K | | .410140E-04 |
| Specific heat kJ/kg*K | | 2.36314 |
| Z factor | | .620808 |
| m3/hr (15.6 deg C & 1 atm) | | 379.043 |
| Vol. flowrate m3/hr | | 2.77413 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 12.9600 |
| Oxygen | .190000 | 3.04000 |

CODE REPORT

*** Stream no. 19 ***

| | | |
|------------------------------------|--------------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -126.695 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 347.978 |
| Entropy MJ/hr*K | | -.733690 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 690.488 |
| | kgmol/hr | 24.0000 |
| Density kg/m3 | | 165.937 |
| Viscosity centipoise | | .106058E-01 |
| Thermal cond. cal/cm*s*K | | .410140E-04 |
| Specific heat kJ/kg*K | | 2.36291 |
| Z factor | | .620808 |

| | |
|---|----------|
| m ³ /hr (15.6 deg C & 1 atm) . | 568.565 |
| Vol. flowrate m ³ /hr | 4.16120 |
| | Vapor |
| | flowrate |
| | kgmol/hr |
| Nitrogen | .810000 |
| Oxygen | .190000 |
| | 4.56000 |

*** Stream no. 20 ***

| | | |
|---|-----------|-------------|
| Temperature deg C. | All Vapor | -126.695 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 164.710 |
| Entropy MJ/hr*K | | -0.347280 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 326.831 |
| kgmol/hr | | 11.3600 |
| Density kg/m ³ | | 165.937 |
| Viscosity centipoise | | .106058E-01 |
| Thermal cond. cal/cm*s*K | | .410140E-04 |
| Specific heat kJ/kg*K | | 2.36313 |
| Z factor | | .620808 |
| m ³ /hr (15.6 deg C & 1 atm) . | | 269.121 |
| Vol. flowrate m ³ /hr | | 1.96963 |
| | Vapor | |
| | flowrate | |
| | kgmol/hr | |
| Nitrogen | .810000 | 9.20160 |
| Oxygen | .190000 | 2.15840 |

CODE REPORT

*** Stream no. 21 ***

| | | |
|---|-----------|-------------|
| Temperature deg C. | All Vapor | -126.695 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 67.2758 |
| Entropy MJ/hr*K | | -0.141847 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 133.494 |
| kgmol/hr | | 4.64000 |
| Density kg/m ³ | | 165.937 |
| Viscosity centipoise | | .106058E-01 |
| Thermal cond. cal/cm*s*K | | .410140E-04 |
| Specific heat kJ/kg*K | | 2.36258 |
| Z factor | | .620808 |
| m ³ /hr (15.6 deg C & 1 atm) . | | 109.922 |
| Vol. flowrate m ³ /hr | | .804498 |
| | Vapor | |
| | flowrate | |
| | kgmol/hr | |
| Nitrogen | .810000 | 3.75840 |
| Oxygen | .190000 | .881600 |

*** Stream no. 22 ***

| | | |
|----------------------------|-----------|-----------|
| Temperature deg C. | All Vapor | -136.781 |
| Pressure bars. | | 43.6000 |
| Enthalpy MJ/hr | | 62.2307 |
| Entropy MJ/hr*K | | -0.177787 |
| Ave. mol. wt. | | 28.7703 |

| | |
|---|-------------------------|
| Total flow kg/hr | 133.494 |
| kgmol/hr | 4.64000 |
| Density kg/m ³ | 267.904 |
| Viscosity centipoise | .106456E-01 |
| Thermal cond. cal/cm*s*K | .397891E-04 |
| Specific heat kJ/kg*K | 7.77801 |
| Z factor | .412963 |
| m ³ /hr (15.6 deg C & 1 atm) | 109.922 |
| Vol. flowrate m ³ /hr | .498299 |
| Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen .810000 | 3.75840 |
| Oxygen .190000 | .881600 |

CODE REPORT

*** Stream no. 23 ***

| | |
|---|-------------------------|
| Temperature deg C | -136.752 |
| Pressure bars | 43.6000 |
| Enthalpy MJ/hr | 152.431 |
| Entropy MJ/hr*K | -.434724 |
| Ave. mol. wt. | 28.7703 |
| Total flow kg/hr | 326.831 |
| kgmol/hr | 11.3600 |
| Density kg/m ³ | 267.071 |
| Viscosity centipoise | .106420E-01 |
| Thermal cond. cal/cm*s*K | .397925E-04 |
| Specific heat kJ/kg*K | 7.70562 |
| Z factor | .414162 |
| m ³ /hr (15.6 deg C & 1 atm) | 269.121 |
| Vol. flowrate m ³ /hr | 1.22378 |
| Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen .810000 | 9.20160 |
| Oxygen .190000 | 2.15840 |

*** Stream no. 24 ***

| | |
|---|-------------------------|
| Temperature deg C | -136.760 |
| Pressure bars | 43.6000 |
| Enthalpy MJ/hr | 214.662 |
| Entropy MJ/hr*K | -.612499 |
| Ave. mol. wt. | 28.7703 |
| Total flow kg/hr | 460.325 |
| kgmol/hr | 16.0000 |
| Density kg/m ³ | 267.300 |
| Viscosity centipoise | .106430E-01 |
| Thermal cond. cal/cm*s*K | .397916E-04 |
| Specific heat kJ/kg*K | 7.72551 |
| Z factor | .413833 |
| m ³ /hr (15.6 deg C & 1 atm) | 379.043 |
| Vol. flowrate m ³ /hr | 1.72216 |
| Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen .810000 | 12.9600 |
| Oxygen .190000 | 3.04000 |

CODE REPORT

*** Stream no. 25 ***

| | Overall | Vapor | Liquid |
|----------------------------|---------------------|----------------------|--------------------------|
| Temperature deg C. | -172.366 | | |
| Pressure bars. | 6.61325 | | |
| Vapor fraction | .817598 | | |
| Enthalpy MJ/hr | 214.662 | 187.666 | 27.0110 |
| Entropy MJ/hr*K | -.474266 | -.269560 | -.204705 |
| Ave. mol. wt. | 28.7703 | 28.6655 | 29.2409 |
| Total flow kg/hr | 460.325 | 374.990 | 85.3375 |
| kgmol/hr | 16.0000 | 13.0816 | 2.91843 |
| Density kg/m3 | | 26.7024 | 1406.48 |
| Viscosity centipoise | | .690154E-02 | .103313 |
| Thermal cond. cal/cm*s*K | | .357732E-04 | .505024E-03 |
| Specific heat kJ/kg*K | | 1.25170 | 2.17381 |
| Z factor | | .847052 | |
| m3/hr (15.6 deg C & 1 atm) | | 309.974 | |
| Vol. flowrate m3/hr | | 14.0435 | |
| Surface tension dyne/cm. | | | |
| S. G. (60/60) | | | 5.67519 |
| m3/hr (15.6 deg C & 1 atm) | | | .915033 |
| Vol. flowrate m3/hr | | | .934078E-01 |
| | | | .606751E-01 |
| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen | .83630 | .69196 | 10.9401 |
| Oxygen | .16370 | .30804 | 2.14142 |
| | | | Liquid flowrate kgmol/hr |
| | | | 2.01943 |
| | | | .899001 |

*** Stream no. 26 ***

| | Overall | Vapor | Liquid |
|----------------------------|---------------------|----------------------|--------------------------|
| Temperature deg C. | -172.347 | | |
| Pressure bars. | 6.60647 | | |
| Vapor fraction | .832393 | | |
| Enthalpy MJ/hr | 323.794 | 286.507 | 37.2739 |
| Entropy MJ/hr*K | -.693828 | -.411175 | -.282652 |
| Ave. mol. wt. | 28.7703 | 28.6730 | 29.2536 |
| Total flow kg/hr | 690.488 | 572.812 | 117.675 |
| kgmol/hr | 24.0000 | 19.9774 | 4.02257 |
| Density kg/m3 | | 26.6790 | 1407.54 |
| Viscosity centipoise | | .690418E-02 | .103845 |
| Thermal cond. cal/cm*s*K | | .357657E-04 | .504985E-03 |
| Specific heat kJ/kg*K | | 1.24986 | 2.17363 |
| Z factor | | .847282 | |
| m3/hr (15.6 deg C & 1 atm) | | 473.210 | |
| Vol. flowrate m3/hr | | 21.4708 | |
| Surface tension dyne/cm. | | | |
| S. G. (60/60) | | | 5.69054 |
| m3/hr (15.6 deg C & 1 atm) | | | .915375 |
| Vol. flowrate m3/hr | | | .128755 |
| | | | .836040E-01 |
| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen | .83443 | .68876 | 16.6698 |
| Oxygen | .16557 | .31124 | 3.30767 |
| | | | Liquid flowrate kgmol/hr |
| | | | 2.77060 |
| | | | 1.25197 |

*** Stream no. 27 ***

| | All Liquid |
|--------------------|------------|
| Temperature deg C. | -175.941 |
| Pressure bars. | 6.71314 |

CODE REPORT

| | |
|--------------------------------------|-----------------|
| Enthalpy MJ/hr | 152.101 |
| Entropy MJ/hr*K | -1.12251 |
| Ave. mol. wt. | 28.0883 |
| Total flow kg/hr. | 449.412 |
| kgmol/hr | 15.9999 |
| Density kg/m3 | 1329.92 |
| Viscosity centipoise | .947307E-01 |
| Thermal cond. cal/cm*s*K | .510531E-03 |
| Specific heat kJ/kg*K | 2.34647 |
| Surface tension dyne/cm. | 4.74317 |
| S. G. (60/60) | .883885 |
| m3/hr (15.6 deg C & 1 atm) | .509248 |
| Vol. flowrate m3/hr | .337928 |
| Liquid mole fraction | Liquid flowrate |
| Nitrogen .981097 | kgmol/hr |
| Oxygen .189026E-01 | 15.6975 |
| | .302440 |

*** Stream no. 28 ***

| | | All Liquid |
|--------------------------------------|--|-----------------|
| Temperature deg C. | | -172.151 |
| Pressure bars. | | 6.73254 |
| Enthalpy MJ/hr | | 222.843 |
| Entropy MJ/hr*K | | -1.68107 |
| Ave. mol. wt. | | 29.2250 |
| Total flow kg/hr. | | 701.402 |
| kgmol/hr | | 24.0001 |
| Density kg/m3 | | 1402.47 |
| Viscosity centipoise | | .102868 |
| Thermal cond. cal/cm*s*K | | .504666E-03 |
| Specific heat kJ/kg*K | | 2.18357 |
| Surface tension dyne/cm. | | 5.60304 |
| S. G. (60/60) | | .914607 |
| m3/hr (15.6 deg C & 1 atm) | | .768091 |
| Vol. flowrate m3/hr | | .500125 |
| Liquid mole fraction | | Liquid flowrate |
| Nitrogen .695936 | | kgmol/hr |
| Oxygen .304064 | | 16.7025 |
| | | 7.29756 |

CODE REPORT

*** Stream no. 29 ***

| | | All Liquid |
|--------------------------------------|--|-------------|
| Temperature deg C. | | -186.647 |
| Pressure bars. | | 6.71314 |
| Enthalpy MJ/hr | | 141.492 |
| Entropy MJ/hr*K | | -1.23802 |
| Ave. mol. wt. | | 28.0883 |
| Total flow kg/hr. | | 449.412 |
| kgmol/hr | | 15.9999 |
| Density kg/m3 | | 1445.97 |
| Viscosity centipoise | | .123409 |
| Thermal cond. cal/cm*s*K | | .527857E-03 |
| Specific heat kJ/kg*K | | 2.09301 |
| Surface tension dyne/cm. | | 6.98401 |
| S. G. (60/60) | | .883885 |
| m3/hr (15.6 deg C & 1 atm) | | .509248 |
| Vol. flowrate m3/hr | | .310805 |

| | Liquid mole fraction | Liquid flowrate kgmol/hr |
|----------|----------------------------|--------------------------------|
| Nitrogen | .981097 | 15.6975 |
| Oxygen | .189026E-01 | .302440 |

*** Stream no. 30 ***

| | All Liquid |
|--------------------------------------|-------------|
| Temperature deg C. | -176.939 |
| Pressure bars. | 6.73254 |
| Enthalpy MJ/hr | 215.707 |
| Entropy MJ/hr*K | -1.75344 |
| Ave. mol. wt. | 29.2250 |
| Total flow kg/hr. | 701.402 |
| kgmol/hr | 24.0001 |
| Density kg/m3 | 1454.69 |
| Viscosity centipoise | .113785 |
| Thermal cond. cal/cm*s*K | .512414E-03 |
| Specific heat kJ/kg*K | 2.07018 |
| Surface tension dyne/cm. | 6.67743 |
| S. G. (60/60) | .914607 |
| m3/hr (15.6 deg C & 1 atm) | .768091 |
| Vol. flowrate m3/hr | .482172 |

| | Liquid mole fraction | Liquid flowrate kgmol/hr |
|----------|----------------------------|--------------------------------|
| Nitrogen | .695936 | 16.7025 |
| Oxygen | .304064 | 7.29756 |

CODE REPORT

*** Stream no. 31 ***

| | Overall | Vapor | Liquid |
|--------------------------------------|----------|--------------|-------------|
| Temperature deg C. | -190.027 | | |
| Pressure bars. | 1.45725 | | |
| Vapor fraction | .138541 | | |
| Enthalpy MJ/hr | 215.707 | 46.6821 | 168.992 |
| Entropy MJ/hr*K | -1.73074 | -.409657E-01 | -1.68978 |
| Ave. mol. wt. | 29.2250 | 28.5267 | 29.3371 |
| Total flow kg/hr | 701.402 | 94.8512 | 606.546 |
| kgmol/hr | 24.0001 | 3.32499 | 20.6751 |
| Density kg/m3 | | 6.34647 | 1590.31 |
| Viscosity centipoise | | .566974E-02 | .161615 |
| Thermal cond. cal/cm*s*K | | .339249E-04 | .533619E-03 |
| Specific heat kJ/kg*K | | 1.10370 | 1.84549 |
| Z factor | | .949507 | |
| m3/hr (15.6 deg C & 1 atm) | | 78.6264 | |
| Vol. flowrate m3/hr | | 14.9457 | |
| Surface tension dyne/cm. | | | 9.92894 |
| S. G. (60/60) | | | .917617 |
| m3/hr (15.6 deg C & 1 atm) | | | .662037 |
| Vol. flowrate m3/hr | | | .381406 |

| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr | Liquid flowrate kgmol/hr |
|----------|---------------------------|----------------------------|-------------------------------|--------------------------------|
| Nitrogen | .87111 | .66782 | 2.89644 | 13.8073 |
| Oxygen | .12889 | .33218 | .428552 | 6.86778 |

*** Stream no. 32 ***

| | Overall | Vapor | Liquid |
|----------------------------|----------|-------|--------|
| Temperature deg C. | -192.652 | | |

| | | | | | |
|--------------------------------------|-------------|------------|--------------|----------|-------------|
| Pressure bars. . . | 1.40055 | | | | |
| Vapor fraction . . | .668986E-01 | | | | |
| Enthalpy MJ/hr . . | 141.492 | | 14.7390 | | 126.654 |
| Entropy MJ/hr*K . . | -1.23346 | | -.138828E-01 | | -1.21957 |
| Ave. mol. wt. . . | 28.0883 | | 28.0376 | | 28.0918 |
| Total flow kg/hr . . | 449.412 | | 30.0129 | | 419.398 |
| kgmol/hr . . | 15.9999 | | 1.07037 | | 14.9296 |
| Density kg/m3 | | | 6.29450 | | 1503.80 |
| Viscosity centipoise | | | .541943E-02 | | .148024 |
| Thermal cond. cal/cm*s*K | | | .336861E-04 | | .537568E-03 |
| Specific heat kJ/kg*K | | | 1.13005 | | 1.97940 |
| Z factor | | | .947868 | | |
| m3/hr (15.6 deg C & 1 atm) | | | 24.9376 | | |
| Vol. flowrate m3/hr | | | 4.76818 | | |
| Surface tension dyne/cm. | | | | | 8.31469 |
| S. G. (60/60) | | | | | .883978 |
| m3/hr (15.6 deg C & 1 atm) | | | | | .475188 |
| Vol. flowrate m3/hr | | | | | .278895 |
| | Vapor | Liquid | Vapor | Liquid | |
| | mole | mole | flowrate | flowrate | |
| | fraction | fraction | kgmol/hr | kgmol/hr | |
| Nitrogen | .99332 | .98024 | 1.06322 | 14.6345 | |
| Oxygen | .66830E-02 | .19763E-01 | .715335E-02 | .295055 | |

CODE REPORT

*** Stream no. 33 ***

| | Overall | | Vapor | | Liquid |
|--------------------------------------|----------|----------|--------------|----------|-------------|
| Temperature deg C. | -190.008 | | | | |
| Pressure bars. . . | 1.45725 | | | | |
| Vapor fraction . . | .148894 | | | | |
| Enthalpy MJ/hr . . | 217.084 | | 50.2428 | | 166.874 |
| Entropy MJ/hr*K . . | -1.71320 | | -.440183E-01 | | -1.66918 |
| Ave. mol. wt. . . | 29.2250 | | 28.5310 | | 29.3463 |
| Total flow kg/hr . . | 701.402 | | 101.955 | | 599.446 |
| kgmol/hr . . | 24.0001 | | 3.57346 | | 20.4266 |
| Density kg/m3 | | | 6.33689 | | 1590.93 |
| Viscosity centipoise | | | .567168E-02 | | .161666 |
| Thermal cond. cal/cm*s*K | | | .339457E-04 | | .533592E-03 |
| Specific heat kJ/kg*K | | | 1.10343 | | 1.84441 |
| Z factor | | | .949532 | | |
| m3/hr (15.6 deg C & 1 atm) | | | 84.6209 | | |
| Vol. flowrate m3/hr | | | 16.0893 | | |
| Surface tension dyne/cm. | | | | | 9.94126 |
| S. G. (60/60) | | | | | .917866 |
| m3/hr (15.6 deg C & 1 atm) | | | | | .654110 |
| Vol. flowrate m3/hr | | | | | .376793 |
| | Vapor | Liquid | Vapor | Liquid | |
| | mole | mole | flowrate | flowrate | |
| | fraction | fraction | kgmol/hr | kgmol/hr | |
| Nitrogen | .87004 | .66549 | 3.10905 | 13.5938 | |
| Oxygen | .12996 | .33451 | .464419 | 6.83284 | |

*** Stream no. 34 ***

| | All Vapor |
|----------------------------|-----------|
| Temperature deg C. | -192.647 |
| Pressure bars. | 1.40055 |
| Enthalpy MJ/hr | 453.661 |
| Entropy MJ/hr*K | -.421952 |
| Ave. mol. wt. | 28.0407 |
| Total flow kg/hr. | 908.518 |

| | | |
|---|------------------------------|-------------|
| | kgmol/hr | 32.4000 |
| Density | kg/m ³ | 6.19011 |
| Viscosity | centipoise | .541992E-02 |
| Thermal cond. | cal/cm*s*K | .339356E-04 |
| Specific heat | kJ/kg*K | 1.13027 |
| Z factor | | .947875 |
| m ³ /hr (15.6 deg C & 1 atm) | | 767.562 |
| Vol. flowrate | m ³ /hr | 146.771 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .993053 | 32.1749 |
| Oxygen | .694701E-02 | .225083 |
| CODE REPORT | | |

*** Stream no. 35 ***

| | | |
|---|------------------------------|-------------|
| | | All Liquid |
| Temperature | deg C. | -179.524 |
| Pressure | bars. | 1.59905 |
| Enthalpy | MJ/hr | 58.1288 |
| Entropy | MJ/hr*K | -.604788 |
| Ave. mol. wt. | | 31.8810 |
| Total flow | kg/hr. | 242.295 |
| | kgmol/hr | 7.60000 |
| Density | kg/m ³ | 1708.81 |
| Viscosity | centipoise | .175474 |
| Thermal cond. | cal/cm*s*K | .517224E-03 |
| Specific heat | kJ/kg*K | 1.63250 |
| Surface tension | dyne/cm. | 12.0762 |
| S. G. (60/60) | | .985094 |
| m ³ /hr (15.6 deg C & 1 atm) | | .246347 |
| Vol. flowrate | m ³ /hr | .141794 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .296160E-01 | .225082 |
| Oxygen | .970384 | 7.37492 |

*** Stream no. 36 ***

| | | |
|---|------------------------------|-------------|
| | | All Vapor |
| Temperature | deg C. | -17.0000 |
| Pressure | bars. | 1.40055 |
| Enthalpy | MJ/hr | 206.062 |
| Entropy | MJ/hr*K | .234685 |
| Ave. mol. wt. | | 28.0407 |
| Total flow | kg/hr. | 299.812 |
| | kgmol/hr | 10.6920 |
| Density | kg/m ³ | 1.84668 |
| Viscosity | centipoise | .157820E-01 |
| Thermal cond. | cal/cm*s*K | .571445E-04 |
| Specific heat | kJ/kg*K | 1.04649 |
| Z factor | | .998569 |
| m ³ /hr (15.6 deg C & 1 atm) | | 253.296 |
| Vol. flowrate | m ³ /hr | 162.355 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .993056 | 10.6178 |
| Oxygen | .694353E-02 | .742405E-01 |
| CODE REPORT | | |

*** Stream no. 37 ***

| | | All Liquid |
|----------------------------|----------------------|--------------------------|
| Temperature deg C. | | -183.027 |
| Pressure bars. | | 1.59905 |
| Enthalpy MJ/hr | | 56.7509 |
| Entropy MJ/hr*K | | -.619822 |
| Ave. mol. wt. | | 31.8809 |
| Total flow kg/hr. | | 242.295 |
| kgmol/hr | | 7.60000 |
| Density kg/m3 | | 1736.78 |
| Viscosity centipoise | | .190476 |
| Thermal cond. cal/cm*s*K | | .522893E-03 |
| Specific heat kJ/kg*K | | 1.61428 |
| Surface tension dyne/cm. | | 12.9412 |
| S. G. (60/60) | | .985094 |
| m3/hr (15.6 deg C & 1 atm) | | .246347 |
| Vol. flowrate m3/hr | | .139510 |
| | Liquid mole fraction | Liquid flowrate kgmol/hr |
| Nitrogen | .296180E-01 | .225097 |
| Oxygen | .970382 | 7.37490 |

*** Stream no. 38 ***

| | | All Vapor |
|----------------------------|---------------------|-------------------------|
| Temperature deg C. | | 14.3137 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 215.867 |
| Entropy MJ/hr*K | | .270798 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 299.812 |
| kgmol/hr | | 10.6920 |
| Density kg/m3 | | 1.64442 |
| Viscosity centipoise | | .172909E-01 |
| Thermal cond. cal/cm*s*K | | .624492E-04 |
| Specific heat kJ/kg*K | | 1.04284 |
| Z factor | | .999233 |
| m3/hr (15.6 deg C & 1 atm) | | 253.296 |
| Vol. flowrate m3/hr | | 182.323 |
| | Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen | .993056 | 10.6178 |
| Oxygen | .694353E-02 | .742405E-01 |

CODE REPORT

*** Stream no. 39 ***

| | | All Vapor |
|--------------------------|--|-------------|
| Temperature deg C. | | -182.235 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 464.271 |
| Entropy MJ/hr*K | | -.297990 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 908.519 |
| kgmol/hr | | 32.4000 |
| Density kg/m3 | | 5.40076 |
| Viscosity centipoise | | .612474E-02 |
| Thermal cond. cal/cm*s*K | | .350410E-04 |
| Specific heat kJ/kg*K | | 1.11342 |

| | | |
|--|----------|----------|
| Z factor | .961993 | |
| m ³ /hr (15.6 deg C & 1 atm) . | 767.562 | |
| Vol. flowrate m ³ /hr | 168.223 | |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .993052 | | 32.1749 |
| Oxygen .694790E-02 | | .225112 |

*** Stream no. 40 ***

| | | |
|--|--------------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -175.151 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 471.407 |
| Entropy MJ/hr*K | | -.222393 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 908.519 |
| | kgmol/hr | 32.4000 |
| Density kg/m ³ | | 4.97527 |
| Viscosity centipoise | | .660189E-02 |
| Thermal cond. cal/cm*s*K | | .358104E-04 |
| Specific heat kJ/kg*K | | 1.10482 |
| Z factor | | .968776 |
| m ³ /hr (15.6 deg C & 1 atm) . | | 767.562 |
| Vol. flowrate m ³ /hr | | 182.609 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .993052 | | 32.1749 |
| Oxygen .694790E-02 | | .225112 |

CODE REPORT

*** Stream no. 41 ***

| | | |
|--|--------------------|-------------|
| | | All Liquid |
| Temperature deg C. | | -183.027 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 59.0735 |
| Entropy MJ/hr*K | | -.632921 |
| Ave. mol. wt. | | 31.8810 |
| Total flow kg/hr. | | 242.296 |
| | kgmol/hr | 7.60001 |
| Density kg/m ³ | | 1851.30 |
| Viscosity centipoise | | .190477 |
| Thermal cond. cal/cm*s*K | | .522893E-03 |
| Specific heat kJ/kg*K | | 1.53818 |
| Surface tension dyne/cm. | | 12.9162 |
| S. G. (60/60) | | .985095 |
| m ³ /hr (15.6 deg C & 1 atm) . | | .246348 |
| Vol. flowrate m ³ /hr | | .130880 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .296015E-01 | | .224972 |
| Oxygen .970398 | | 7.37504 |

*** Stream no. 42 ***

| | | |
|----------------------------|--|------------|
| | | All Liquid |
| Temperature deg C. | | -180.000 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 60.2039 |

```

Entropy MJ/hr*K . . . . . -620586
Ave. mol. wt. . . . . 31.8810
Total flow kg/hr. . . . . 242.296
      kgmol/hr . . . . . 7.60001
Density kg/m3 . . . . . 1832.14
Viscosity centipoise . . . . . 1.177378
Thermal cond. cal/cm*s*K . . . . . 5.17794E-03
Specific heat kJ/kg*K . . . . . 1.54479
Surface tension dyne/cm. . . . . 12.1671
S. G. (60/60) . . . . . .985095
m3/hr (15.6 deg C & 1 atm) . . . . . 246348
Vol. flowrate m3/hr . . . . . 132249
      Liquid
      mole
      fraction
Nitrogen .296015E-01 .224972
Oxygen .970398 7.37504
CODE REPORT
  
```

*** Stream no. 43 ***

```

All Vapor
Temperature deg C. . . . . -175.000
Pressure bars. . . . . 1.40055
Enthalpy MJ/hr . . . . . 471.559
Entropy MJ/hr*K . . . . . -220847
Ave. mol. wt. . . . . 28.0407
Total flow kg/hr. . . . . 908.517
      kgmol/hr . . . . . 32.4000
Density kg/m3 . . . . . 4.96696
Viscosity centipoise . . . . . 6.661203E-02
Thermal cond. cal/cm*s*K . . . . . 3.58270E-04
Specific heat kJ/kg*K . . . . . 1.10413
Z factor . . . . . .968902
m3/hr (15.6 deg C & 1 atm) . . . . . 767.562
Vol. flowrate m3/hr . . . . . 182.915
      Vapor
      mole
      fraction
Nitrogen .993056 32.1750
Oxygen .694356E-02 .224971
  
```

*** Stream no. 44 ***

```

All Vapor
Temperature deg C. . . . . -162.695
Pressure bars. . . . . 1.40055
Enthalpy MJ/hr . . . . . 483.838
Entropy MJ/hr*K . . . . . -102970
Ave. mol. wt. . . . . 28.0407
Total flow kg/hr. . . . . 908.517
      kgmol/hr . . . . . 32.4000
Density kg/m3 . . . . . 4.37578
Viscosity centipoise . . . . . 7.43164E-02
Thermal cond. cal/cm*s*K . . . . . 3.71982E-04
Specific heat kJ/kg*K . . . . . 1.09313
Z factor . . . . . .977283
m3/hr (15.6 deg C & 1 atm) . . . . . 767.562
Vol. flowrate m3/hr . . . . . 207.627
      Vapor
      mole
      fraction
  
```

Nitrogen .993056 32.1750
 Oxygen .694356E-02 .224971

CODE REPORT

*** Stream no. 45 ***

| | | |
|--------------------------------------|----------|-------------|
| | | All Liquid |
| Temperature deg C. | | -166.695 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 65.2489 |
| Entropy MJ/hr*K | | -.569975 |
| Ave. mol. wt. | | 31.8810 |
| Total flow kg/hr. | | 242.296 |
| kgmol/hr | | 7.60001 |
| Density kg/m3 | | 1747.94 |
| Viscosity centipoise | | .136068 |
| Thermal cond. cal/cm*s*K | | .496463E-03 |
| Specific heat kJ/kg*K | | 1.58880 |
| Surface tension dyne/cm. | | 8.96505 |
| S. G. (60/60) | | .985095 |
| m3/hr (15.6 deg C & 1 atm) | | .246348 |
| Vol. flowrate m3/hr | | .138620 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .296015E-01 | | .224972 |
| Oxygen .970398 | | 7.37504 |

*** Stream no. 46 ***

| | | |
|--------------------------------------|----------|-------------|
| | | All Vapor |
| Temperature deg C. | | -18.0000 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 129.703 |
| Entropy MJ/hr*K | | -.190834 |
| Ave. mol. wt. | | 31.8810 |
| Total flow kg/hr. | | 242.296 |
| kgmol/hr | | 7.60001 |
| Density kg/m3 | | 337.460 |
| Viscosity centipoise | | .189521E-01 |
| Thermal cond. cal/cm*s*K | | .540524E-04 |
| Specific heat kJ/kg*K | | 1.41163 |
| Z factor | | .846140 |
| m3/hr (15.6 deg C & 1 atm) | | 180.046 |
| Vol. flowrate m3/hr | | .718010 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .296015E-01 | | .224972 |
| Oxygen .970398 | | 7.37504 |

CODE REPORT

*** Stream no. 47 ***

| | | |
|----------------------------|--|-----------|
| | | All Vapor |
| Temperature deg C. | | -15.0000 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 626.332 |
| Entropy MJ/hr*K | | .718553 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 908.517 |
| kgmol/hr | | 32.4000 |
| Density kg/m3 | | 1.83226 |

Viscosity centipoise158808E-01
 Thermal cond. cal/cm*s*K574716E-04
 Specific heat kJ/kg*K1.04566
 Z factor998621
 m3/hr (15.6 deg C & 1 atm)767.562
 Vol. flowrate m3/hr495.851
 Vapor
 mole
 fraction Vapor
 flowrate
 Nitrogen .993056 32.1750
 Oxygen .694356E-02 .224971

*** Stream no. 48 ***

All Vapor
 Temperature deg C. -15.0000
 Pressure bars. 1.40055
 Enthalpy MJ/hr 206.689
 Entropy MJ/hr*K237124
 Ave. mol. wt. 28.0407
 Total flow kg/hr. 299.812
 kgmol/hr 10.6920
 Density kg/m3 1.83227
 Viscosity centipoise158808E-01
 Thermal cond. cal/cm*s*K574715E-04
 Specific heat kJ/kg*K 1.04545
 Z factor998621
 m3/hr (15.6 deg C & 1 atm)253.296
 Vol. flowrate m3/hr 163.631
 Vapor
 mole
 fraction Vapor
 flowrate
 Nitrogen .993056 10.6178
 Oxygen .694353E-02 .742405E-01
 CODE REPORT

*** Stream no. 49 ***

All Vapor
 Temperature deg C. 12.0000
 Pressure bars. 1.40055
 Enthalpy MJ/hr 215.143
 Entropy MJ/hr*K268271
 Ave. mol. wt. 28.0407
 Total flow kg/hr. 299.812
 kgmol/hr 10.6920
 Density kg/m3 1.65783
 Viscosity centipoise171821E-01
 Thermal cond. cal/cm*s*K620435E-04
 Specific heat kJ/kg*K 1.04336
 Z factor999193
 m3/hr (15.6 deg C & 1 atm)253.296
 Vol. flowrate m3/hr 180.849
 Vapor
 mole
 fraction Vapor
 flowrate
 Nitrogen .993056 10.6178
 Oxygen .694353E-02 .742405E-01

*** Stream no. 50 ***

All Vapor
 Temperature deg C. -15.0000

| | | | |
|----------|-------------|----------|-----|
| | fraction | kgmol/hr | |
| Nitrogen | .003056 | 32.1750 | 163 |
| Oxygen | .694356E+02 | .224971 | |

CODE REPORT

TOWER # 1 Data file: PLANT.OUT Profile file: link.prf

Column Summary

| Stg | Temp C | Pres bars | Net Flow Rates kgmols/hr | | | Duties MJ/hr | |
|-----|-----------|--------------|-----------------------------|--------|--------|-----------------|---------|
| | | | Liquid | Vapor | Feed | | |
| 1 | -175.9 | 6.713 | 18.302 | | | 16.000 | -163.51 |
| 2 | -174.8 | 6.713 | 18.437 | 34.301 | | | |
| 3 | -174.6 | 6.714 | 18.315 | 34.437 | | | |
| 4 | -174.4 | 6.715 | 18.186 | 34.315 | | | |
| 5 | -174.1 | 6.716 | 18.053 | 34.186 | | | |
| 6 | -173.9 | 6.717 | 17.920 | 34.053 | | | |
| 7 | -173.7 | 6.718 | 17.788 | 33.920 | | | |
| 8 | -173.5 | 6.719 | 17.664 | 33.788 | | | |
| 9 | -173.2 | 6.720 | 17.548 | 33.664 | | | |
| 10 | -173.0 | 6.721 | 17.441 | 33.548 | | | |
| 11 | -172.9 | 6.722 | 17.345 | 33.441 | | | |
| 12 | -172.7 | 6.723 | 17.260 | 33.345 | | | |
| 13 | -172.5 | 6.724 | 17.188 | 33.260 | | | |
| 14 | -172.4 | 6.725 | 17.125 | 33.188 | | | |
| 15 | -172.3 | 6.726 | 20.019 | 33.125 | 16.000 | | |
| 16 | -172.3 | 6.727 | 20.017 | 20.019 | | | |
| 17 | -172.3 | 6.728 | 20.013 | 20.017 | | | |
| 18 | -172.3 | 6.729 | 20.007 | 20.013 | | | |
| 19 | -172.2 | 6.731 | 19.995 | 20.006 | | | |
| 20 | -172.2 | 6.732 | 19.977 | 19.995 | | | |
| 21 | -172.2 | 6.733 | | 19.977 | 24.000 | 24.000 | |

Stream # 25 fed to Stg 15 is 81.760 % Vapor
Stream # 26 fed to Stg 21 is 83.239 % Vapor

Stream # 27 is Liquid Distillate from Stg 1
Stream # 28 is Liquid Bottoms from Stg 21

Condenser duty is -163.509 MJ/hr
Reboiler duty is .000000 MJ/hr
CODE REPORT

TOWER # 1 Data file: PLANT.OUT Profile file: link.prf
Tray Liquid Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|
| 1 | 514.1 | 28.09 | .58 | .39 | 1329.90 | .0947 |
| 2 | 519.3 | 28.17 | .59 | .39 | 1324.17 | .0934 |
| 3 | 517.4 | 28.25 | .58 | .39 | 1330.77 | .0941 |
| 4 | 515.4 | 28.34 | .58 | .39 | 1337.73 | .0949 |
| 5 | 513.4 | 28.44 | .58 | .38 | 1344.89 | .0957 |
| 6 | 511.3 | 28.53 | .57 | .38 | 1352.12 | .0966 |

| | | | | | | |
|----|-------|-------|-----|-----|---------|-------|
| 7 | 509.2 | 28.63 | .57 | .37 | 1359.24 | .0974 |
| 8 | 507.3 | 28.72 | .56 | .37 | 1366.10 | .0983 |
| 9 | 505.5 | 28.81 | .56 | .37 | 1372.55 | .0991 |
| 10 | 503.8 | 28.89 | .56 | .37 | 1378.48 | .0998 |
| 11 | 502.3 | 28.96 | .55 | .36 | 1383.83 | .1005 |
| 12 | 501.0 | 29.03 | .55 | .36 | 1388.54 | .1011 |
| 13 | 499.9 | 29.08 | .55 | .36 | 1392.62 | .1016 |
| 14 | 498.9 | 29.13 | .55 | .36 | 1396.12 | .1021 |
| 15 | 584.0 | 29.17 | .64 | .42 | 1399.05 | .1024 |
| 16 | 584.0 | 29.18 | .64 | .42 | 1399.15 | .1024 |
| 17 | 584.0 | 29.18 | .64 | .42 | 1399.33 | .1025 |
| 18 | 583.9 | 29.18 | .64 | .42 | 1399.65 | .1025 |
| 19 | 583.7 | 29.19 | .64 | .42 | 1400.19 | .1026 |
| 20 | 583.4 | 29.20 | .64 | .42 | 1401.05 | .1027 |
| 21 | 701.4 | 29.23 | .77 | .50 | 1402.45 | .1029 |

Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|---|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 1 | *** Total Condenser : No Vapor Outlet *** | | | | | |
| 2 | 963.5 | 28.09 | 812.6 | 34.93 | .8356 | 27.5836 |
| 3 | 968.7 | 28.13 | 815.8 | 35.16 | .8364 | 27.5500 |
| 4 | 966.8 | 28.18 | 812.9 | 35.14 | .8372 | 27.5144 |
| 5 | 964.8 | 28.22 | 809.9 | 35.11 | .8380 | 27.4771 |
| 6 | 962.8 | 28.27 | 806.7 | 35.09 | .8388 | 27.4393 |
| 7 | 960.7 | 28.32 | 803.6 | 35.06 | .8397 | 27.4012 |
| 8 | 958.6 | 28.37 | 800.4 | 35.03 | .8405 | 27.3650 |
| 9 | 956.7 | 28.42 | 797.5 | 35.01 | .8413 | 27.3303 |
| 10 | 954.9 | 28.46 | 794.8 | 34.98 | .8420 | 27.2985 |
| 11 | 953.2 | 28.50 | 792.2 | 34.96 | .8427 | 27.2699 |
| 12 | 951.7 | 28.54 | 789.9 | 34.93 | .8432 | 27.2448 |
| 13 | 950.4 | 28.58 | 787.9 | 34.91 | .8438 | 27.2235 |
| 14 | 949.3 | 28.60 | 786.2 | 34.89 | .8442 | 27.2061 |
| 15 | 948.3 | 28.63 | 784.7 | 34.88 | .8446 | 27.1917 |
| 16 | 573.1 | 28.63 | 474.3 | 21.08 | .8446 | 27.1946 |
| 17 | 573.1 | 28.63 | 474.2 | 21.07 | .8446 | 27.1974 |
| 18 | 573.1 | 28.63 | 474.1 | 21.07 | .8446 | 27.1993 |
| 19 | 573.0 | 28.64 | 474.0 | 21.06 | .8446 | 27.2003 |
| 20 | 572.8 | 28.65 | 473.7 | 21.06 | .8448 | 27.1985 |
| 21 | 572.5 | 28.66 | 473.3 | 21.05 | .8449 | 27.1935 |

CODE: Chemical Engineering Simulation System
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TOWER # 1 Data file: PLANT.TSZ Profile file: link.prf

Smith-Dresser-Ohlswager Shortcut Technique

User Provided Input Data

Tray spacing (in. or cm) 7.0000
Downcomer area (ft2 or m2) .0151
Weir length (in. or cm) 24.0000
Weir height (in. or cm) 3.0000

Liquid Vapor Liquid Vapor Flooding Se

| Stg | Diameter meter | Vol. flow m3/min | Vol. flow m3/sec | density kg/m3 | density kg/m3 | velocity m/sec | height meter |
|-----|---------------------------------|---------------------|---------------------|------------------|------------------|-------------------|-----------------|
| 1 | ***Condenser: No tray sizing*** | | | | | | |
| 2 | .3051 | .01 | .01 | 1324.1680 | 27.5840 | .1673 | .0361 |
| 3 | .3053 | .01 | .01 | 1330.7740 | 27.5504 | .1681 | .0361 |
| 4 | .3047 | .01 | .01 | 1337.7290 | 27.5148 | .1689 | .0361 |
| 5 | .3041 | .01 | .01 | 1344.8930 | 27.4775 | .1696 | .0361 |
| 6 | .3034 | .01 | .01 | 1352.1240 | 27.4397 | .1704 | .0362 |
| 7 | .3028 | .01 | .01 | 1359.2350 | 27.4016 | .1711 | .0362 |
| 8 | .3022 | .01 | .01 | 1366.1010 | 27.3654 | .1718 | .0362 |
| 9 | .3017 | .01 | .01 | 1372.5490 | 27.3307 | .1725 | .0362 |
| 10 | .3012 | .01 | .01 | 1378.4840 | 27.2989 | .1731 | .0362 |
| 11 | .3007 | .01 | .01 | 1383.8270 | 27.2703 | .1736 | .0363 |
| 12 | .3003 | .01 | .01 | 1388.5370 | 27.2452 | .1741 | .0363 |
| 13 | .3000 | .01 | .01 | 1392.6240 | 27.2239 | .1745 | .0363 |
| 14 | .2997 | .01 | .01 | 1396.1170 | 27.2065 | .1749 | .0363 |
| 15 | .3029 | .01 | .01 | 1399.0490 | 27.1921 | .1701 | .0359 |
| 16 | .2615 | .01 | .01 | 1399.1460 | 27.1950 | .1517 | .0359 |
| 17 | .2615 | .01 | .01 | 1399.3340 | 27.1978 | .1517 | .0359 |
| 18 | .2614 | .01 | .01 | 1399.6510 | 27.1997 | .1517 | .0359 |
| 19 | .2614 | .01 | .01 | 1400.1900 | 27.2007 | .1517 | .0359 |
| 20 | .2613 | .01 | .01 | 1401.0490 | 27.1989 | .1518 | .0359 |
| 21 | .2661 | .01 | .01 | 1402.4480 | 27.1939 | .1444 | .0354 |

CODE REPORT

TOWER # 2

Data file: PLANT.OUT

Profile file: pool.prf

Column Summary

| Stg | Temp C | Pres bars | Net Flow Rates kgmols/hr | | | | Duties MJ/hr |
|-----|-----------|--------------|-----------------------------|--------|--------|---------|-----------------|
| | | | Liquid | Vapor | Feed | Product | |
| 1 | -192.6 | 1.401 | 14.924 | | 16.000 | 32.400 | |
| 2 | -192.6 | 1.404 | 14.920 | 31.324 | | | |
| 3 | -192.6 | 1.408 | 14.915 | 31.320 | | | |
| 4 | -192.5 | 1.411 | 14.907 | 31.315 | | | |
| 5 | -192.5 | 1.415 | 14.896 | 31.307 | | | |
| 6 | -192.5 | 1.418 | 14.881 | 31.296 | | | |
| 7 | -192.4 | 1.422 | 14.861 | 31.281 | | | |
| 8 | -192.3 | 1.425 | 14.832 | 31.261 | | | |
| 9 | -192.2 | 1.429 | 14.793 | 31.232 | | | |
| 10 | -192.1 | 1.432 | 14.742 | 31.194 | | | |
| 11 | -192.0 | 1.436 | 14.674 | 31.142 | | | |
| 12 | -191.8 | 1.440 | 14.587 | 31.074 | | | |
| 13 | -191.6 | 1.443 | 14.478 | 30.987 | | | |
| 14 | -191.3 | 1.447 | 14.348 | 30.878 | | | |
| 15 | -191.0 | 1.450 | 14.198 | 30.748 | | | |
| 16 | -190.6 | 1.454 | 14.037 | 30.598 | | | |
| 17 | -190.2 | 1.457 | 34.459 | 30.437 | 24.000 | | |
| 18 | -190.2 | 1.461 | 34.464 | 26.859 | | | |
| 19 | -190.2 | 1.464 | 34.469 | 26.864 | | | |
| 20 | -190.2 | 1.468 | 34.474 | 26.869 | | | |
| 21 | -190.2 | 1.471 | 34.479 | 26.874 | | | |
| 22 | -190.1 | 1.475 | 34.484 | 26.879 | | | |
| 23 | -190.1 | 1.479 | 34.489 | 26.884 | | | |
| 24 | -190.1 | 1.482 | 34.494 | 26.889 | | | |
| 25 | -190.1 | 1.486 | 34.499 | 26.894 | | | |

| | | | | | | |
|----|--------|-------|--------|--------|--|-----|
| 26 | -190.0 | 1.489 | 34.504 | 26.899 | | |
| 27 | -190.0 | 1.493 | 34.509 | 26.904 | | 166 |
| 28 | -190.0 | 1.496 | 34.514 | 26.909 | | |
| 29 | -190.0 | 1.500 | 34.519 | 26.914 | | |
| 30 | -189.9 | 1.503 | 34.524 | 26.919 | | |
| 31 | -189.9 | 1.507 | 34.529 | 26.924 | | |
| 32 | -189.9 | 1.510 | 34.534 | 26.929 | | |
| 33 | -189.9 | 1.514 | 34.539 | 26.934 | | |
| 34 | -189.8 | 1.518 | 34.544 | 26.939 | | |
| 35 | -189.8 | 1.521 | 34.549 | 26.944 | | |
| 36 | -189.8 | 1.525 | 34.554 | 26.949 | | |
| 37 | -189.8 | 1.528 | 34.559 | 26.954 | | |
| 38 | -189.8 | 1.532 | 34.564 | 26.959 | | |
| 39 | -189.7 | 1.535 | 34.569 | 26.964 | | |
| 40 | -189.7 | 1.539 | 34.574 | 26.969 | | |
| 41 | -189.7 | 1.542 | 34.578 | 26.973 | | |
| 42 | -189.7 | 1.546 | 34.583 | 26.978 | | |
| 43 | -189.6 | 1.549 | 34.588 | 26.983 | | |
| 44 | -189.6 | 1.553 | 34.592 | 26.988 | | |
| 45 | -189.6 | 1.557 | 34.596 | 26.992 | | |
| 46 | -189.6 | 1.560 | 34.599 | 26.996 | | |
| 47 | -189.5 | 1.564 | 34.602 | 26.999 | | |

CODE REPORT

| | | Liquid | Vapor | Feed | Product | |
|----|--------|--------|--------|--------|---------|--------|
| 48 | -189.5 | 1.567 | 34.600 | 27.002 | | |
| 49 | -189.5 | 1.571 | 34.589 | 27.000 | | |
| 50 | -189.4 | 1.574 | 34.553 | 26.989 | | |
| 51 | -189.3 | 1.578 | 34.451 | 26.953 | | |
| 52 | -189.0 | 1.581 | 34.183 | 26.851 | | |
| 53 | -188.3 | 1.585 | 33.566 | 26.583 | | |
| 54 | -186.7 | 1.588 | 32.488 | 25.966 | | |
| 55 | -184.1 | 1.592 | 31.382 | 24.888 | | |
| 56 | -181.2 | 1.596 | 30.829 | 23.782 | | |
| 57 | -179.5 | 1.599 | 23.229 | | 7.6000 | 153.21 |

Stream # 32 fed to Stg 1 is 6.690 % Vapor
 Stream # 33 fed to Stg 17 is 14.889 % Vapor

Stream # 34 is Vapor Distillate from Stg 1
 Stream # 35 is Liquid Bottoms from Stg 57

Condenser duty is .000000 MJ/hr
 Reboiler duty is 153.215 MJ/hr

CODE REPORT

TOWER # 2 Data file: PLANT.OUT Profile file: pool.prf
 Tray Liquid Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise | Surface tension dyne/cm |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|
| 1 | 419.3 | 28.09 | .48 | .28 | 1504.02 | .1477 | 8.32 |
| 2 | 419.2 | 28.10 | .47 | .28 | 1504.13 | .1477 | 8.32 |
| 3 | 419.2 | 28.11 | .47 | .28 | 1504.38 | .1476 | 8.32 |
| 4 | 419.1 | 28.11 | .47 | .28 | 1504.79 | .1476 | 8.33 |
| 5 | 419.0 | 28.12 | .47 | .28 | 1505.46 | .1477 | 8.34 |
| 6 | 418.8 | 28.14 | .47 | .28 | 1506.44 | .1477 | 8.36 |

| | | | | | | | |
|----|--------|-------|------|-----|---------|-------|------|
| 7 | 418.5 | 28.16 | .47 | .28 | 1507.86 | .1479 | 8.38 |
| 8 | 418.1 | 28.19 | .47 | .28 | 1509.88 | .1482 | 8.42 |
| 9 | 417.6 | 28.23 | .47 | .28 | 1512.68 | .1485 | 8.47 |
| 10 | 417.0 | 28.28 | .47 | .27 | 1516.48 | .1491 | 8.53 |
| 11 | 416.1 | 28.35 | .47 | .27 | 1521.53 | .1499 | 8.63 |
| 12 | 414.9 | 28.45 | .47 | .27 | 1528.10 | .1509 | 8.75 |
| 13 | 413.5 | 28.56 | .46 | .27 | 1536.34 | .1522 | 8.90 |
| 14 | 411.8 | 28.70 | .46 | .27 | 1546.31 | .1539 | 9.08 |
| 15 | 409.8 | 28.86 | .45 | .26 | 1557.79 | .1558 | 9.30 |
| 16 | 407.7 | 29.04 | .45 | .26 | 1570.25 | .1580 | 9.54 |
| 17 | 1007.2 | 29.23 | 1.10 | .64 | 1582.90 | .1602 | 9.78 |
| 18 | 1007.3 | 29.23 | 1.10 | .64 | 1582.70 | .1601 | 9.78 |
| 19 | 1007.5 | 29.23 | 1.10 | .64 | 1582.51 | .1600 | 9.77 |
| 20 | 1007.6 | 29.23 | 1.10 | .64 | 1582.31 | .1598 | 9.77 |
| 21 | 1007.8 | 29.23 | 1.10 | .64 | 1582.10 | .1597 | 9.76 |
| 22 | 1007.9 | 29.23 | 1.10 | .64 | 1581.91 | .1596 | 9.76 |
| 23 | 1008.1 | 29.23 | 1.10 | .64 | 1581.71 | .1595 | 9.75 |
| 24 | 1008.2 | 29.23 | 1.10 | .64 | 1581.51 | .1594 | 9.75 |
| 25 | 1008.4 | 29.23 | 1.10 | .64 | 1581.31 | .1593 | 9.74 |
| 26 | 1008.5 | 29.23 | 1.10 | .64 | 1581.12 | .1592 | 9.74 |
| 27 | 1008.7 | 29.23 | 1.10 | .64 | 1580.92 | .1591 | 9.73 |
| 28 | 1008.8 | 29.23 | 1.10 | .64 | 1580.72 | .1590 | 9.72 |
| 29 | 1009.0 | 29.23 | 1.10 | .64 | 1580.53 | .1589 | 9.72 |
| 30 | 1009.1 | 29.23 | 1.10 | .64 | 1580.33 | .1588 | 9.71 |
| 31 | 1009.3 | 29.23 | 1.11 | .64 | 1580.14 | .1587 | 9.71 |
| 32 | 1009.4 | 29.23 | 1.11 | .64 | 1579.94 | .1586 | 9.70 |
| 33 | 1009.6 | 29.23 | 1.11 | .64 | 1579.75 | .1584 | 9.70 |
| 34 | 1009.7 | 29.23 | 1.11 | .64 | 1579.55 | .1583 | 9.69 |
| 35 | 1009.9 | 29.23 | 1.11 | .64 | 1579.36 | .1582 | 9.69 |
| 36 | 1010.0 | 29.23 | 1.11 | .64 | 1579.16 | .1581 | 9.68 |
| 37 | 1010.2 | 29.23 | 1.11 | .64 | 1578.97 | .1580 | 9.68 |
| 38 | 1010.3 | 29.23 | 1.11 | .64 | 1578.77 | .1579 | 9.67 |
| 39 | 1010.5 | 29.23 | 1.11 | .64 | 1578.58 | .1578 | 9.67 |
| 40 | 1010.6 | 29.23 | 1.11 | .64 | 1578.38 | .1577 | 9.66 |
| 41 | 1010.8 | 29.23 | 1.11 | .64 | 1578.19 | .1576 | 9.66 |
| 42 | 1010.9 | 29.23 | 1.11 | .64 | 1578.00 | .1575 | 9.65 |
| 43 | 1011.0 | 29.23 | 1.11 | .64 | 1577.81 | .1574 | 9.65 |
| 44 | 1011.2 | 29.23 | 1.11 | .64 | 1577.62 | .1573 | 9.64 |
| 45 | 1011.3 | 29.23 | 1.11 | .64 | 1577.44 | .1572 | 9.63 |
| 46 | 1011.4 | 29.23 | 1.11 | .64 | 1577.28 | .1571 | 9.63 |
| 47 | 1011.5 | 29.23 | 1.11 | .64 | 1577.15 | .1570 | 9.63 |
| 48 | 1011.6 | 29.24 | 1.11 | .64 | 1577.13 | .1569 | 9.62 |
| 49 | 1011.5 | 29.24 | 1.11 | .64 | 1577.43 | .1569 | 9.63 |

CODE REPORT

TOWR # 2 Data file: PLANT.OUT
Tray Liquid Properties

Profile file: pool.prf

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise | Surface tension dyne/cm |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|
| 50 | 1011.1 | 29.26 | 1.11 | .64 | 1578.51 | .1571 | 9.65 |
| 51 | 1009.8 | 29.31 | 1.10 | .64 | 1581.73 | .1576 | 9.71 |
| 52 | 1006.4 | 29.44 | 1.10 | .63 | 1590.22 | .1591 | 9.87 |
| 53 | 998.6 | 29.75 | 1.08 | .62 | 1610.17 | .1627 | 10.26 |
| 54 | 986.0 | 30.35 | 1.05 | .60 | 1646.33 | .1692 | 10.98 |
| 55 | 976.1 | 31.10 | 1.01 | .58 | 1684.68 | .1753 | 11.72 |
| 56 | 975.4 | 31.64 | 1.00 | .57 | 1703.76 | .1764 | 12.04 |

57 242.3 31.88 .25 .14 1708.78 .1753 12.08
 CODE REPORT

TOWER # 2 Data file: PLANT.OUT Profile file: pool.prf
 Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|--------------------|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 1 | 908.5 | 28.04 | 767.6 | 146.77 | .9479 | 6.1900 |
| 2 | 878.4 | 28.04 | 742.1 | 141.58 | .9478 | 6.2042 |
| 3 | 878.3 | 28.04 | 742.0 | 141.25 | .9477 | 6.2183 |
| 4 | 878.3 | 28.05 | 741.8 | 140.93 | .9476 | 6.2322 |
| 5 | 878.2 | 28.05 | 741.7 | 140.60 | .9476 | 6.2461 |
| 6 | 878.1 | 28.06 | 741.4 | 140.28 | .9475 | 6.2595 |
| 7 | 877.9 | 28.06 | 741.1 | 139.95 | .9474 | 6.2726 |
| 8 | 877.6 | 28.07 | 740.6 | 139.63 | .9474 | 6.2850 |
| 9 | 877.2 | 28.09 | 739.9 | 139.31 | .9474 | 6.2969 |
| 10 | 876.7 | 28.11 | 739.0 | 139.00 | .9475 | 6.3077 |
| 11 | 876.1 | 28.13 | 737.8 | 138.68 | .9475 | 6.3174 |
| 12 | 875.2 | 28.16 | 736.2 | 138.36 | .9477 | 6.3256 |
| 13 | 874.0 | 28.21 | 734.1 | 138.03 | .9479 | 6.3322 |
| 14 | 872.6 | 28.26 | 731.5 | 137.70 | .9481 | 6.3369 |
| 15 | 870.9 | 28.32 | 728.4 | 137.36 | .9484 | 6.3399 |
| 16 | 868.9 | 28.40 | 724.9 | 137.02 | .9488 | 6.3416 |
| 17 | 866.8 | 28.48 | 721.1 | 136.66 | .9492 | 6.3427 |
| 18 | 764.9 | 28.48 | 636.3 | 120.33 | .9491 | 6.3569 |
| 19 | 765.0 | 28.48 | 636.4 | 120.08 | .9490 | 6.3712 |
| 20 | 765.2 | 28.48 | 636.5 | 119.83 | .9489 | 6.3855 |
| 21 | 765.3 | 28.48 | 636.7 | 119.59 | .9488 | 6.3997 |
| 22 | 765.5 | 28.48 | 636.8 | 119.35 | .9488 | 6.4141 |
| 23 | 765.6 | 28.48 | 636.9 | 119.10 | .9487 | 6.4283 |
| 24 | 765.8 | 28.48 | 637.0 | 118.86 | .9486 | 6.4426 |
| 25 | 765.9 | 28.48 | 637.1 | 118.62 | .9485 | 6.4568 |
| 26 | 766.1 | 28.48 | 637.2 | 118.39 | .9484 | 6.4712 |
| 27 | 766.2 | 28.48 | 637.4 | 118.15 | .9483 | 6.4854 |
| 28 | 766.4 | 28.48 | 637.5 | 117.91 | .9482 | 6.4997 |
| 29 | 766.5 | 28.48 | 637.6 | 117.68 | .9481 | 6.5139 |
| 30 | 766.7 | 28.48 | 637.7 | 117.44 | .9480 | 6.5282 |
| 31 | 766.8 | 28.48 | 637.8 | 117.21 | .9479 | 6.5425 |
| 32 | 767.0 | 28.48 | 638.0 | 116.98 | .9478 | 6.5568 |
| 33 | 767.1 | 28.48 | 638.1 | 116.74 | .9478 | 6.5710 |
| 34 | 767.3 | 28.48 | 638.2 | 116.51 | .9477 | 6.5853 |
| 35 | 767.4 | 28.48 | 638.3 | 116.28 | .9476 | 6.5995 |
| 36 | 767.6 | 28.48 | 638.4 | 116.06 | .9475 | 6.6138 |
| 37 | 767.7 | 28.48 | 638.5 | 115.83 | .9474 | 6.6280 |
| 38 | 767.9 | 28.48 | 638.7 | 115.60 | .9473 | 6.6423 |
| 39 | 768.0 | 28.48 | 638.8 | 115.38 | .9472 | 6.6565 |
| 40 | 768.2 | 28.48 | 638.9 | 115.16 | .9471 | 6.6707 |
| 41 | 768.3 | 28.48 | 639.0 | 114.93 | .9470 | 6.6850 |
| 42 | 768.5 | 28.48 | 639.1 | 114.71 | .9469 | 6.6992 |
| 43 | 768.6 | 28.48 | 639.2 | 114.49 | .9469 | 6.7135 |
| 44 | 768.8 | 28.49 | 639.3 | 114.27 | .9468 | 6.7277 |
| 45 | 768.9 | 28.49 | 639.4 | 114.04 | .9467 | 6.7419 |
| 46 | 769.0 | 28.49 | 639.5 | 113.82 | .9466 | 6.7561 |
| 47 | 769.1 | 28.49 | 639.6 | 113.60 | .9465 | 6.7703 |
| 48 | 769.2 | 28.49 | 639.7 | 113.39 | .9464 | 6.7842 |
| 49 | 769.3 | 28.49 | 639.6 | 113.16 | .9463 | 6.7980 |

TOWER # 2 Data file: PLANT.OUT Profile file: pool.prf
Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|--------------------|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 50 | 769.2 | 28.50 | 639.4 | 112.94 | .9463 | 6.8107 |
| 51 | 768.8 | 28.52 | 638.5 | 112.71 | .9464 | 6.8211 |
| 52 | 767.5 | 28.58 | 636.1 | 112.45 | .9467 | 6.8252 |
| 53 | 764.1 | 28.74 | 629.8 | 112.12 | .9475 | 6.8151 |
| 54 | 756.3 | 29.13 | 615.1 | 111.52 | .9494 | 6.7821 |
| 55 | 743.7 | 29.88 | 589.6 | 110.28 | .9524 | 6.7435 |
| 56 | 733.8 | 30.86 | 563.4 | 108.76 | .9549 | 6.7468 |
| 57 | 733.1 | 31.56 | 550.3 | 108.14 | .9562 | 6.7793 |

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TOWER # 2 Data file: PLANT.TSZ Profile file: pool.prf

Smith-Dresser-Dhlswager Shortcut Technique

User Provided Input Data

Tray spacing (in. or cm) 7.0000
Downcomer area (ft2 or m2) .0236
Weir length (in. or cm) 30.0000
Weir height (in. or cm) 3.0000

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|-------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 1 | .3980 | .00 | .04 | 1504.0210 | 6.1901 | .4043 | .0373 |
| 2 | .3922 | .00 | .04 | 1504.1320 | 6.2043 | .4046 | .0373 |
| 3 | .3920 | .00 | .04 | 1504.3760 | 6.2184 | .4042 | .0373 |
| 4 | .3918 | .00 | .04 | 1504.7910 | 6.2323 | .4038 | .0373 |
| 5 | .3915 | .00 | .04 | 1505.4570 | 6.2462 | .4035 | .0373 |
| 6 | .3913 | .00 | .04 | 1506.4410 | 6.2596 | .4032 | .0373 |
| 7 | .3910 | .00 | .04 | 1507.8640 | 6.2727 | .4029 | .0373 |
| 8 | .3907 | .00 | .04 | 1509.8790 | 6.2851 | .4028 | .0373 |
| 9 | .3904 | .00 | .04 | 1512.6780 | 6.2970 | .4028 | .0373 |
| 10 | .3899 | .00 | .04 | 1516.4810 | 6.3078 | .4029 | .0373 |
| 11 | .3894 | .00 | .04 | 1521.5340 | 6.3175 | .4033 | .0373 |
| 12 | .3889 | .00 | .04 | 1528.0950 | 6.3257 | .4038 | .0373 |
| 13 | .3882 | .00 | .04 | 1536.3390 | 6.3323 | .4046 | .0374 |
| 14 | .3874 | .00 | .04 | 1546.3100 | 6.3370 | .4057 | .0374 |
| 15 | .3865 | .00 | .04 | 1557.7890 | 6.3400 | .4070 | .0374 |
| 16 | .3856 | .00 | .04 | 1570.2530 | 6.3417 | .4085 | .0374 |
| 17 | .3935 | .01 | .04 | 1582.9040 | 6.3428 | .3874 | .0353 |
| 18 | .3775 | .01 | .03 | 1582.7020 | 6.3570 | .3785 | .0353 |
| 19 | .3774 | .01 | .03 | 1582.5090 | 6.3713 | .3780 | .0353 |
| 20 | .3773 | .01 | .03 | 1582.3070 | 6.3856 | .3775 | .0353 |
| 21 | .3772 | .01 | .03 | 1582.1040 | 6.3998 | .3769 | .0353 |

| | | | | | | | |
|----|-------|-----|-----|-----------|--------|-------|-------|
| 22 | .3771 | .01 | .03 | 1581.9110 | 6.4142 | .3764 | .0353 |
| 23 | .3770 | .01 | .03 | 1581.7080 | 6.4284 | .3759 | .0353 |
| 24 | .3769 | .01 | .03 | 1581.5140 | 6.4427 | .3754 | .0353 |
| 25 | .3768 | .01 | .03 | 1581.3120 | 6.4569 | .3748 | .0353 |
| 26 | .3767 | .01 | .03 | 1581.1170 | 6.4713 | .3743 | .0353 |
| 27 | .3766 | .01 | .03 | 1580.9240 | 6.4855 | .3738 | .0353 |
| 28 | .3765 | .01 | .03 | 1580.7210 | 6.4998 | .3733 | .0353 |

CODE REPORT

Smith-Dresser-Ohlswager Shortcut Technique

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|--------------------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 29 | .3764 | .01 | .03 | 1580.5260 | 6.5140 | .3728 | .0353 |
| 30 | .3763 | .01 | .03 | 1580.3320 | 6.5283 | .3723 | .0353 |
| 31 | .3762 | .01 | .03 | 1580.1370 | 6.5426 | .3718 | .0353 |
| 32 | .3761 | .01 | .03 | 1579.9430 | 6.5569 | .3713 | .0353 |
| 33 | .3761 | .01 | .03 | 1579.7490 | 6.5711 | .3708 | .0353 |
| 34 | .3760 | .01 | .03 | 1579.5550 | 6.5854 | .3703 | .0353 |
| 35 | .3759 | .01 | .03 | 1579.3600 | 6.5996 | .3697 | .0353 |
| 36 | .3758 | .01 | .03 | 1579.1650 | 6.6139 | .3692 | .0353 |
| 37 | .3757 | .01 | .03 | 1578.9690 | 6.6281 | .3687 | .0353 |
| 38 | .3756 | .01 | .03 | 1578.7750 | 6.6423 | .3683 | .0353 |
| 39 | .3755 | .01 | .03 | 1578.5800 | 6.6566 | .3678 | .0353 |
| 40 | .3754 | .01 | .03 | 1578.3850 | 6.6708 | .3673 | .0353 |
| 41 | .3753 | .01 | .03 | 1578.1900 | 6.6851 | .3668 | .0353 |
| 42 | .3752 | .01 | .03 | 1578.0040 | 6.6993 | .3663 | .0353 |
| 43 | .3752 | .01 | .03 | 1577.8130 | 6.7136 | .3658 | .0353 |
| 44 | .3751 | .01 | .03 | 1577.6250 | 6.7278 | .3653 | .0353 |
| 45 | .3750 | .01 | .03 | 1577.4420 | 6.7420 | .3648 | .0353 |
| 46 | .3749 | .01 | .03 | 1577.2790 | 6.7562 | .3643 | .0353 |
| 47 | .3748 | .01 | .03 | 1577.1480 | 6.7704 | .3639 | .0353 |
| 48 | .3747 | .01 | .03 | 1577.1340 | 6.7843 | .3634 | .0353 |
| 49 | .3746 | .01 | .03 | 1577.4270 | 6.7981 | .3630 | .0353 |
| 50 | .3744 | .01 | .03 | 1578.5150 | 6.8108 | .3628 | .0353 |
| 51 | .3740 | .01 | .03 | 1581.7290 | 6.8212 | .3630 | .0353 |
| 52 | .3732 | .01 | .03 | 1590.2230 | 6.8253 | .3642 | .0353 |
| 53 | .3714 | .01 | .03 | 1610.1710 | 6.8152 | .3675 | .0354 |
| 54 | .3682 | .01 | .03 | 1646.3300 | 6.7822 | .3738 | .0355 |
| 55 | .3643 | .01 | .03 | 1684.6800 | 6.7436 | .3799 | .0356 |
| 56 | .3618 | .01 | .03 | 1703.7650 | 6.7469 | .3814 | .0356 |
| 57 | ***Reboiler: No tray sizing*** | | | | | | |

Appendix C

Computer results of the optimized exchanger network of the oxygen plant

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TOPOLOGY

| Equipment | Stream Numbers |
|-----------|----------------|
| 1 HXER | 5 16 -7 -17 |
| 2 HXER | 4 15 -6 -18 |
| 3 HXER | 9 14 -12 -15 |
| 4 HXER | 19 -3 0 0 |
| 5 DVDR | 3 -5 -4 0 |
| 6 DVDR | 8 -9 -10 0 |
| 7 MIXR | 7 6 -8 0 |
| 8 ENTM | 10 -11 0 0 |
| 9 VALV | 12 -13 0 0 |
| 10 HXER | 1 17 -2 -20 |
| 11 HXER | 2 18 -19 -21 |

Stream Connections

| Stream | Equipment From | Equipment To |
|--------|----------------|--------------|
| 1 | 0 | 10 |
| 2 | 10 | 11 |
| 3 | 4 | 5 |
| 4 | 5 | 2 |
| 5 | 5 | 1 |
| 6 | 2 | 7 |
| 7 | 1 | 7 |
| 8 | 7 | 6 |
| 9 | 6 | 3 |
| 10 | 6 | 8 |
| 11 | 8 | 0 |
| 12 | 3 | 9 |
| 13 | 9 | 0 |
| 14 | 0 | 3 |
| 15 | 3 | 2 |
| 16 | 0 | 1 |
| 17 | 1 | 10 |
| 18 | 2 | 11 |
| 19 | 11 | 4 |
| 20 | 10 | 0 |
| 21 | 11 | 0 |

COMPONENTS 2
 ID numbers 46, 47.

THERMODYNAMICS

Kvalue option: Peng-Robinson
 Enthalpy option: Peng-Robinson
 Density option: API method
 CODE REPORT

MISCELLANEOUS

Recycle calculations are converged.

Recycle equipment list (KE2): 4, 5, 1, 10, 6, 3, 2, 7, 1

Preferred cut stream list (KE3): 19, 8,

| | |
|-------------------------|-----------|
| Convergence tolerances, | Error |
| Flowrates: | .00100000 |
| Vapor fraction: | .00100000 |
| Temperature: | .00100000 |
| Pressure: | .00100000 |
| Enthalpy: | .00100000 |
| Flash calcs: | .00005000 |

| | |
|------------------------------|----|
| Max. loops in recycle calc.: | 30 |
| in flash calcs: | 75 |

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```

*** DIVIDERS ***
Equipment no.           5           6
External name
Fraction/flow  1      .33200      .40000
                2      .66800      .60000
                3      .00000      .00000
                4      .00000      .00000
                5      .00000      .00000
                6      .00000      .00000
Mode
Stream #           .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
Comp. ID #         .0           .0
  
```

```

.....
*** MIXERS-W/FLASH ***
Equipment no.           7
External name
  
```

```

.....
*** VALVES ***
Equipment no.           9
External name
Outlet pressure bars  6.6132
  
```

```

.....
***EXCHANGER/CONDENSERS***
  
```

| Equipment no. | 1 | 2 | 3 | 4 |
|-----------------------|---------|---------|---------|--------|
| External name | | | | |
| Heat transfer coeff. | 300.00 | 300.00 | 300.00 | .00000 |
| Area | 6.6210 | 20.686 | 1.8796 | .00000 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 3.0 | 3.0 | 3.0 | 5.0 |
| Min. delta T or T-out | 24.00 | 19.00 | 28.00 | 12.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | -71.526 | -144.00 | -18.371 | 2.9531 |
| Water usage, DM3/hr | .00000 | .00000 | .00000 | .00000 |
| Corrected delta T | 36.01 | 23.20 | 32.58 | .00 |
| Equipment no. | 10 | 11 | | |
| External name | | | | |
| Heat transfer coeff. | 300.00 | 300.00 | | |
| Area | 1.2357 | 1.8388 | | |
| Number of shells | .0 | .0 | | |
| Shell passes | .0 | .0 | | |
| Tube passes | .0 | .0 | | |
| Mode | 3.0 | 3.0 | | |
| Min. delta T or T-out | 12.00 | 14.40 | | |
| Delta P, stream 1 | .00000 | .00000 | | |
| Delta P, stream 2 | .00000 | .00000 | | |
| Q, stream 1 MJ/hr | -7.0601 | -8.5576 | | |
| Water usage, DM3/hr | .00000 | .00000 | | |
| Corrected delta T | 19.04 | 15.51 | | |

174

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*** ENTROPY MACHINES ***

| | |
|----------------------|---------|
| Equipment no. | B |
| External name | |
| Mode | .0 |
| Outlet pressure bars | 6.6065 |
| Adiabatic efficiency | .92000 |
| Theoretical hp | -10.158 |
| Actual horsepower | -9.3453 |
| Entropy in KJ/deg C | -760.17 |
| Entropy out, ideal | -760.68 |
| Entropy out, actual | -739.87 |

CODE REPORT

*** Stream no. 1 ***

| | |
|-------------------|---------|
| Temperature deg C | 22.0000 |
| Pressure bars | 44.0000 |
| Enthalpy MJ/hr | 802.024 |
| Entropy MJ/hr*K | -142020 |
| Ave. mol. wt. | 28.7703 |
| Total flow kg/hr | 1150.81 |
| kgmol/hr | 40.0000 |
| Density kg/m3 | 52.5200 |

All Vapor

| | | |
|------------------------------|-------------|----------|
| Viscosity centipoise | .162249E-01 | |
| Thermal cond. cal/cm*s*K . . | .631572E-04 | |
| Specific heat kJ/kg*K . . . | 1.09868 | |
| Z factor | .982210 | |
| m3/hr (15.6 deg C & 1 atm) . | 947.608 | |
| Vol. flowrate m3/hr | 21.9122 | |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

*** Stream no. 2 ***

| | | |
|------------------------------|-----------|-------------|
| Temperature deg C. | All Vapor | 16.4189 |
| Pressure bars. | | 44.0000 |
| Enthalpy MJ/hr | | 794.964 |
| Entropy MJ/hr*K | | -.166208 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m3 | | 53.6688 |
| Viscosity centipoise | | .179587E-01 |
| Thermal cond. cal/cm*s*K . . | | .621728E-04 |
| Specific heat kJ/kg*K . . . | | 1.10302 |
| Z factor | | .979712 |
| m3/hr (15.6 deg C & 1 atm) . | | 947.608 |
| Vol. flowrate m3/hr | | 21.4432 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

CODE REPORT

*** Stream no. 3 ***

| | | |
|------------------------------|-----------|-------------|
| Temperature deg C. | All Vapor | 12.0000 |
| Pressure bars. | | 44.0000 |
| Enthalpy MJ/hr | | 789.335 |
| Entropy MJ/hr*K | | -.185758 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| kgmol/hr | | 40.0000 |
| Density kg/m3 | | 54.6189 |
| Viscosity centipoise | | .177463E-01 |
| Thermal cond. cal/cm*s*K . . | | .614027E-04 |
| Specific heat kJ/kg*K . . . | | 1.10628 |
| Z factor | | .977588 |
| m3/hr (15.6 deg C & 1 atm) . | | 947.608 |
| Vol. flowrate m3/hr | | 21.0702 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

*** Stream no. 4 ***

| | | |
|----------------------------|-----------|---------|
| Temperature deg C. | All Vapor | 12.0000 |
|----------------------------|-----------|---------|

| | | | |
|--------------------------------------|-------------|----------|--|
| Pressure bars. | 44.0000 | | |
| Enthalpy MJ/hr | 527.276 | | |
| Entropy MJ/hr*K | -.124086 | | |
| Ave. mol. wt. | 28.7703 | | |
| Total flow kg/hr. | 768.743 | | |
| kgmol/hr | 26.7200 | | |
| Density kg/m3 | 54.6189 | | |
| Viscosity centipoise | .177463E-01 | | |
| Thermal cond. cal/cm*s*K | .614027E-04 | | |
| Specific heat kJ/kg*K | 1.10651 | | |
| Z factor | .977588 | | |
| m3/hr (15.6 deg C & 1 atm) | 633.002 | | |
| Vol. flowrate m3/hr | 14.0749 | | |
| | Vapor | Vapor | |
| | mole | flowrate | |
| | fraction | kgmol/hr | |
| Nitrogen .810000 | | 21.6432 | |
| Oxygen .190000 | | 5.07680 | |

CODE REPORT

*** Stream no. 5 ***

| | | | |
|--------------------------------------|--------------|-----------|--|
| | | All Vapor | |
| Temperature deg C. | 12.0000 | | |
| Pressure bars. | 44.0000 | | |
| Enthalpy MJ/hr | 262.059 | | |
| Entropy MJ/hr*K | -.616716E-01 | | |
| Ave. mol. wt. | 28.7703 | | |
| Total flow kg/hr. | 382.070 | | |
| kgmol/hr | 13.2800 | | |
| Density kg/m3 | 54.6189 | | |
| Viscosity centipoise | .177463E-01 | | |
| Thermal cond. cal/cm*s*K | .614027E-04 | | |
| Specific heat kJ/kg*K | 1.10704 | | |
| Z factor | .977588 | | |
| m3/hr (15.6 deg C & 1 atm) | 314.606 | | |
| Vol. flowrate m3/hr | 6.99530 | | |
| | Vapor | Vapor | |
| | mole | flowrate | |
| | fraction | kgmol/hr | |
| Nitrogen .810000 | | 10.7568 | |
| Oxygen .190000 | | 2.52320 | |

*** Stream no. 6 ***

| | | | |
|--------------------------------------|-------------|-----------|--|
| | | All Vapor | |
| Temperature deg C. | -128.560 | | |
| Pressure bars. | 44.0000 | | |
| Enthalpy MJ/hr | 383.278 | | |
| Entropy MJ/hr*K | -.846519 | | |
| Ave. mol. wt. | 28.7703 | | |
| Total flow kg/hr. | 768.743 | | |
| kgmol/hr | 26.7200 | | |
| Density kg/m3 | 177.787 | | |
| Viscosity centipoise | .105647E-01 | | |
| Thermal cond. cal/cm*s*K | .407851E-04 | | |
| Specific heat kJ/kg*K | 2.63376 | | |
| Z factor | .592288 | | |
| m3/hr (15.6 deg C & 1 atm) | 633.002 | | |
| Vol. flowrate m3/hr | 4.32401 | | |
| | Vapor | Vapor | |
| | mole | flowrate | |

| | | |
|----------|----------|----------|
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 21.6432 |
| Oxygen | .190000 | 5.07680 |

*** Stream no. 7 ***

| | | |
|----------------------------|----------|-------------|
| | | All Vapor |
| Temperature deg C. | | -128.519 |
| Pressure bars. | | 44.0000 |
| Enthalpy MJ/hr | | 190.533 |
| Entropy MJ/hr*K | | -.420439 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 382.070 |
| | kgmol/hr | 13.2800 |
| Density kg/m3 | | 177.565 |
| Viscosity centipoise | | .105659E-01 |
| Thermal cond. cal/cm*s*K | | .407901E-04 |
| Specific heat kJ/kg*K | | 2.62877 |
| Z factor | | .592862 |
| m3/hr (15.6 deg C & 1 atm) | | 314.606 |
| Vol. flowrate m3/hr | | 2.15175 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 10.7568 |
| Oxygen | .190000 | 2.52320 |

*** Stream no. 8 ***

| | | |
|----------------------------|----------|-------------|
| | | All Vapor |
| Temperature deg C. | | -128.546 |
| Pressure bars. | | 44.0000 |
| Enthalpy MJ/hr | | 573.811 |
| Entropy MJ/hr*K | | -1.26695 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 1150.81 |
| | kgmol/hr | 40.0000 |
| Density kg/m3 | | 177.711 |
| Viscosity centipoise | | .105651E-01 |
| Thermal cond. cal/cm*s*K | | .407868E-04 |
| Specific heat kJ/kg*K | | 2.63183 |
| Z factor | | .592484 |
| m3/hr (15.6 deg C & 1 atm) | | 947.608 |
| Vol. flowrate m3/hr | | 6.47584 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .810000 | 32.4000 |
| Oxygen | .190000 | 7.60000 |

CODE REPORT

*** Stream no. 9 ***

| | | |
|--------------------|----------|-----------|
| | | All Vapor |
| Temperature deg C. | | -128.546 |
| Pressure bars. | | 44.0000 |
| Enthalpy MJ/hr | | 229.525 |
| Entropy MJ/hr*K | | -.506780 |
| Ave. mol. wt. | | 28.7703 |
| Total flow kg/hr. | | 460.325 |
| | kgmol/hr | 16.0000 |
| Density kg/m3 | | 177.711 |

Viscosity centipoise105651E-01
 Thermal cond. cal/cm*s*K407868E-04
 Specific heat kJ/kg*K2.63231
 Z factor592484
 m3/hr (15.6 deg C & 1 atm)379.043
 Vol. flowrate m3/hr2.59034
 Vapor mole fraction
 Vapor flowrate kgmol/hr
 Nitrogen .810000 12.9600
 Oxygen .190000 3.04000

*** Stream no. 10 ***

All Vapor
 Temperature deg C. -128.546
 Pressure bars. 44.0000
 Enthalpy MJ/hr 344.287
 Entropy MJ/hr*K -760170
 Ave. mol. wt. 28.7703
 Total flow kg/hr. 690.488
 kgmol/hr 24.0000
 Density kg/m3 177.711
 Viscosity centipoise105651E-01
 Thermal cond. cal/cm*s*K407868E-04
 Specific heat kJ/kg*K2.63220
 Z factor592484
 m3/hr (15.6 deg C & 1 atm)568.565
 Vol. flowrate m3/hr3.88550
 Vapor mole fraction
 Vapor flowrate kgmol/hr
 Nitrogen .810000 19.4400
 Oxygen .190000 4.56000

CODE REPORT

*** Stream no. 11 ***

| | Overall | Vapor | Liquid |
|--------------------------------------|---------------------|----------------------|--------------------------|
| Temperature deg C. | -172.433 | | |
| Pressure bars. | 6.60650 | | |
| Vapor fraction . . . | .794075 | | |
| Enthalpy MJ/hr . . . | 319.118 | 273.333 | 45.7936 |
| Entropy MJ/hr*K . . | -739788 | -392903 | -346885 |
| Ave. mol. wt. . . . | 28.7703 | 28.6535 | 29.2210 |
| Total flow kg/hr . . | 690.488 | 546.073 | 144.416 |
| kgmol/hr | 24.0000 | 19.0578 | 4.94220 |
| Density kg/m3 | | 26.6876 | 1405.25 |
| Viscosity centipoise | | .689482E-02 | .103319 |
| Thermal cond. cal/cm*s*K | | .357702E-04 | .505124E-03 |
| Specific heat kJ/kg*K | | 1.25212 | 2.17687 |
| Z factor | | .846983 | |
| m3/hr (15.6 deg C & 1 atm) | | 451.521 | |
| Vol. flowrate m3/hr | | 20.4619 | |
| Surface tension dyne/cm. | | | 5.65960 |
| S. G. (60/60) | | | .914499 |
| m3/hr (15.6 deg C & 1 atm) | | | .158166 |
| Vol. flowrate m3/hr | | | .102770 |
| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen | .83931 | .69694 | 15.9954 |
| | | | Liquid flowrate kgmol/hr |
| | | | 3.44440 |

Oxygen .16069 .30306 3.06243 1.49780 179

*** Stream no. 12 ***

All Vapor
 Temperature deg C. -137.366
 Pressure bars. 44.0000
 Enthalpy MJ/hr 211.154
 Entropy MJ/hr*K -.638783
 Ave. mol. wt. 28.7703
 Total flow kg/hr. 460.325
 kgmol/hr 16.0000
 Density kg/m3 297.981
 Viscosity centipoise108017E-01
 Thermal cond. cal/cm*s*K397190E-04
 Specific heat kJ/kg*K 9.94371
 Z factor376301
 m3/hr (15.6 deg C & 1 atm) 379.043
 Vol. flowrate m3/hr 1.54484

| | Vapor mole fraction | Vapor flowrate kgmol/hr |
|----------|---------------------------|-------------------------------|
| Nitrogen | .810000 | 12.9600 |
| Oxygen | .190000 | 3.04000 |

CODE REPORT

*** Stream no. 13 ***

| | Overall | Vapor | Liquid |
|--------------------------------------|----------|-------------|-------------|
| Temperature deg C. | -172.462 | | |
| Pressure bars. . . | 6.61320 | | |
| Vapor fraction . . . | .774389 | | |
| Enthalpy MJ/hr . . . | 211.154 | 177.671 | 33.4807 |
| Entropy MJ/hr*K . . . | -.509091 | -.255681 | -.253410 |
| Ave. mol. wt. . . . | 28.7703 | 28.6438 | 29.2045 |
| Total flow kg/hr . . | 460.325 | 354.904 | 105.422 |
| kgmol/hr | 16.0000 | 12.3902 | 3.60978 |
| Density kg/m3 | | 26.7247 | 1403.92 |
| Viscosity centipoise | | .689110E-02 | .103236 |
| Thermal cond. cal/cm*s*K | | .357706E-04 | .505164E-03 |
| Specific heat kJ/kg*K | | 1.25342 | 2.18061 |
| Z factor | | .846719 | |
| m3/hr (15.6 deg C & 1 atm) | | 293.518 | |
| Vol. flowrate m3/hr | | 13.2802 | |
| Surface tension dyne/cm. | | | 5.64067 |
| S. G. (60/60) | | | .914055 |
| m3/hr (15.6 deg C & 1 atm) | | | .115515 |
| Vol. flowrate m3/hr | | | .750916E-01 |

| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr | Liquid flowrate kgmol/hr |
|----------|---------------------------|----------------------------|-------------------------------|--------------------------------|
| Nitrogen | .84174 | .70109 | 10.4293 | 2.53077 |
| Oxygen | .15826 | .29891 | 1.96094 | 1.07901 |

*** Stream no. 14 ***

All Vapor
 Temperature deg C. -175.000
 Pressure bars. 1.40055
 Enthalpy MJ/hr 471.559
 Entropy MJ/hr*K -.220848
 Ave. mol. wt. 28.0407
 Total flow kg/hr. 908.518

| | | |
|--------------------------------------|-------------|----------|
| kgmol/hr | 32.4000 | |
| Density kg/m3 | 4.96697 | |
| Viscosity centipoise | .661202E-02 | |
| Thermal cond. cal/cm*s*K | .358270E-04 | |
| Specific heat kJ/kg*K | 1.10482 | |
| Z factor | .968902 | |
| m3/hr (15.6 deg C & 1 atm) | 767.562 | |
| Vol. flowrate m3/hr | 182.915 | |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .993061 | | 32.1752 |
| Oxygen .693858E-02 | | .224810 |
| CODE REPORT | | |

*** Stream no. 15 ***

| | | |
|--------------------------------------|----------|--------------|
| | | All Vapor |
| Temperature deg C. | | -156.546 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 489.930 |
| Entropy MJ/hr*K | | -.492974E-01 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 908.518 |
| kgmol/hr | | 32.4000 |
| Density kg/m3 | | 4.13194 |
| Viscosity centipoise | | .783564E-02 |
| Thermal cond. cal/cm*s*K | | .378999E-04 |
| Specific heat kJ/kg*K | | 1.08797 |
| Z factor | | .980378 |
| m3/hr (15.6 deg C & 1 atm) | | 767.562 |
| Vol. flowrate m3/hr | | 219.880 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .993061 | | 32.1752 |
| Oxygen .693858E-02 | | .224810 |

*** Stream no. 16 ***

| | | |
|--------------------------------------|----------|-------------|
| | | All Liquid |
| Temperature deg C. | | -180.000 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 60.2035 |
| Entropy MJ/hr*K | | -.620586 |
| Ave. mol. wt. | | 31.8811 |
| Total flow kg/hr. | | 242.296 |
| kgmol/hr | | 7.60000 |
| Density kg/m3 | | 1832.15 |
| Viscosity centipoise | | .177380 |
| Thermal cond. cal/cm*s*K | | .517994E-03 |
| Specific heat kJ/kg*K | | 1.54479 |
| Surface tension dyne/cm. | | 12.1673 |
| S. G. (60/60) | | .985098 |
| m3/hr (15.6 deg C & 1 atm) | | .246347 |
| Vol. flowrate m3/hr | | .132248 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen .295803E-01 | | .224810 |
| Oxygen .970420 | | 7.37519 |
| CODE REPORT | | |

*** Stream no. 17 ***

| | | | |
|--------------------------------------|----------|-------------|----------|
| Temperature deg C. | | All Vapor | |
| Pressure bars. | | -12.0000 | |
| Enthalpy MJ/hr | | 190.000 | |
| Entropy MJ/hr*K | | 131.730 | |
| Ave. mol. wt. | | -.182981 | |
| Total flow kg/hr. | | 31.6811 | |
| kgmol/hr | | 242.296 | |
| Density kg/m3 | | 7.60000 | |
| Viscosity centipoise | | 324.183 | |
| Thermal cond. cal/cm*s*K | | .192427E-01 | |
| Specific heat kJ/kg*K | | .549925E-04 | |
| Z factor | | 1.37680 | |
| m3/hr (15.6 deg C & 1 atm) | | .860560 | |
| Vol. flowrate m3/hr | | 180.045 | |
| | Vapor | | Vapor |
| | mole | | flowrate |
| | fraction | | kgmol/hr |
| Nitrogen .295803E-01 | | .224810 | |
| Oxygen .970420 | | 7.37519 | |

*** Stream no. 18 ***

| | | | |
|--------------------------------------|----------|-------------|----------|
| Temperature deg C. | | All Vapor | |
| Pressure bars. | | -7.00000 | |
| Enthalpy MJ/hr | | 1.40055 | |
| Entropy MJ/hr*K | | 633.928 | |
| Ave. mol. wt. | | .747534 | |
| Total flow kg/hr. | | 28.0407 | |
| kgmol/hr | | 908.518 | |
| Density kg/m3 | | 32.4000 | |
| Viscosity centipoise | | 1.77685 | |
| Thermal cond. cal/cm*s*K | | .162726E-01 | |
| Specific heat kJ/kg*K | | .587952E-04 | |
| Z factor | | 1.04497 | |
| m3/hr (15.6 deg C & 1 atm) | | .978815 | |
| Vol. flowrate m3/hr | | 767.562 | |
| | Vapor | | Vapor |
| | mole | | flowrate |
| | fraction | | kgmol/hr |
| Nitrogen .993061 | | 32.1752 | |
| Oxygen .693858E-02 | | .224810 | |

CODE REPORT

*** Stream no. 19 ***

| | | | |
|------------------------------------|--|-------------|--|
| Temperature deg C. | | All Vapor | |
| Pressure bars. | | 9.68271 | |
| Enthalpy MJ/hr | | 44.0000 | |
| Entropy MJ/hr*K | | 786.406 | |
| Ave. mol. wt. | | -.196156 | |
| Total flow kg/hr. | | 28.7703 | |
| kgmol/hr | | 1150.81 | |
| Density kg/m3 | | 40.0000 | |
| Viscosity centipoise | | 55.1324 | |
| Thermal cond. cal/cm*s*K | | .176345E-01 | |
| Specific heat kJ/kg*K | | .610021E-04 | |
| Z factor | | 1.10737 | |
| | | .976418 | |

| | | |
|------------------------------|---------------------|-------------------------|
| m3/hr (15.6 deg C & 1 atm) . | | 947.608 |
| Vol. flowrate m3/hr | | 20.0737 |
| | Vapor mole fraction | Vapor flowrate kgmol/hr |
| Nitrogen .810000 | | 32.4000 |
| Oxygen .190000 | | 7.60000 |

*** Stream no. 20 ***

| | | | |
|------------------------------------|---------------------|-------------------------|-------------|
| Temperature deg C. | | All Vapor | 10.0000 |
| Pressure bars. | | | 190.000 |
| Enthalpy MJ/hr | | | 138.790 |
| Entropy MJ/hr*K | | | -1.157012 |
| Ave. mol. wt. | | | 31.8811 |
| Total flow kg/hr. | | | 242.296 |
| kgmol/hr | | | 7.60000 |
| Density kg/m3 | | | 284.517 |
| Viscosity centipoise | | | .203271E-01 |
| Thermal cond. cal/cm*s*K | | | .585597E-04 |
| Specific heat kJ/kg*K | | | 1.27878 |
| Z factor | | | .904349 |
| m3/hr (15.6 deg C & 1 atm) . | | | 180.045 |
| Vol. flowrate m3/hr | | | .851617 |
| | Vapor mole fraction | Vapor flowrate kgmol/hr | |
| Nitrogen .295803E-01 | | | .224810 |
| Oxygen .970420 | | | 7.37519 |

CODE REPORT

*** Stream no. 21 ***

| | | | |
|------------------------------------|---------------------|-------------------------|-------------|
| Temperature deg C. | | All Vapor | 2.01887 |
| Pressure bars. | | | 1.40055 |
| Enthalpy MJ/hr | | | 642.486 |
| Entropy MJ/hr*K | | | .779154 |
| Ave. mol. wt. | | | 28.0407 |
| Total flow kg/hr. | | | 908.518 |
| kgmol/hr | | | 32.4000 |
| Density kg/m3 | | | 1.71828 |
| Viscosity centipoise | | | .167079E-01 |
| Thermal cond. cal/cm*s*K | | | .603186E-04 |
| Specific heat kJ/kg*K | | | 1.04360 |
| Z factor | | | .999007 |
| m3/hr (15.6 deg C & 1 atm) . | | | 767.562 |
| Vol. flowrate m3/hr | | | 528.745 |
| | Vapor mole fraction | Vapor flowrate kgmol/hr | |
| Nitrogen .993061 | | | 32.1752 |
| Oxygen .693858E-02 | | | .224810 |

Appendix D

Computer results of the column-
tray sizing under the nominal
flow rate of air

CODE: Chemical Engineering Simulation System
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TOPOLOGY

| Equipment | Stream Numbers |
|-----------|----------------|
| 1 TOWR | 1 2 -3 -4 |
| 2 HXER | 3 10 -5 -13 |
| 3 HXER | 4 13 -6 -15 |
| 4 HXER | 8 11 -9 -12 |
| 5 VALV | 5 -7 0 0 |
| 6 VALV | 6 -8 0 0 |
| 7 TOWR | 7 9 -10 -11 |
| 8 PUMP | 12 -14 0 0 |
| 9 HXER | 15 -16 0 0 |
| 10 HXER | 14 -17 0 0 |

Stream Connections

| Stream | Equipment | |
|--------|-----------|----|
| | From | To |
| 1 | 0 | 1 |
| 2 | 0 | 1 |
| 3 | 1 | 2 |
| 4 | 1 | 3 |
| 5 | 2 | 5 |
| 6 | 3 | 6 |
| 7 | 5 | 7 |
| 8 | 6 | 4 |
| 9 | 4 | 7 |
| 10 | 7 | 2 |
| 11 | 7 | 4 |
| 12 | 4 | 8 |
| 13 | 2 | 3 |
| 14 | 8 | 10 |
| 15 | 3 | 9 |
| 16 | 9 | 0 |
| 17 | 10 | 0 |

COMPONENTS 2
 ID numbers 46, 47,

THERMODYNAMICS

Kvalue option: Peng-Robinson
 Enthalpy option: Peng-Robinson
 Density option: API method
 CODE REPORT

MISCELLANEOUS

Recycle calculations are converged.

CODE: Chemical Engineering Simulation System
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TOPOLOGY

| Equipment | Stream Numbers |
|-----------|----------------|
| 1 TOWR | 1 2 -3 -4 |
| 2 HXER | 3 10 -5 -13 |
| 3 HXER | 4 13 -6 -15 |
| 4 HXER | 8 11 -9 -12 |
| 5 VALV | 5 -7 0 0 |
| 6 VALV | 6 -8 0 0 |
| 7 TOWR | 7 9 -10 -11 |
| 8 PUMP | 12 -14 0 0 |
| 9 HXER | 15 -16 0 0 |
| 10 HXER | 14 -17 0 0 |

Stream Connections

| Stream | Equipment From | Equipment To |
|--------|----------------|--------------|
| 1 | 0 | 1 |
| 2 | 0 | 1 |
| 3 | 1 | 2 |
| 4 | 1 | 3 |
| 5 | 2 | 5 |
| 6 | 3 | 6 |
| 7 | 5 | 7 |
| 8 | 6 | 4 |
| 9 | 4 | 7 |
| 10 | 7 | 2 |
| 11 | 7 | 4 |
| 12 | 4 | 8 |
| 13 | 2 | 3 |
| 14 | 8 | 10 |
| 15 | 3 | 9 |
| 16 | 9 | 0 |
| 17 | 10 | 0 |

COMPONENTS 2
 ID numbers 46, 47.

THERMODYNAMICS

Kvalue option: Peng-Robinson
 Enthalpy option: Peng-Robinson
 Density option: API method
 CODE REPORT

MISCELLANEOUS

Recycle calculations are converged.

Recycle equipment list (KE2): 2, 3, 5, 6, 4, 7,

Streams used in conv. routine (KE4):(0)
()=Delay factor

Preferred cut stream list (KE3): 10, 11,

| | |
|-------------------------|-----------|
| Convergence tolerances, | Error |
| Flowrates: | .00100000 |
| Vapor fraction: | .00100000 |
| Temperature: | .00100000 |
| Pressure: | .00100000 |
| Enthalpy: | .00100000 |
| Flash calcs: | .00005000 |

| | |
|------------------------------|----|
| Max. loops in recycle calc.: | 30 |
| in flash calcs: | 75 |

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| | | |
|----------------------|--------|--------|
| *** VALVES *** | 5 | 6 |
| Equipment no. | | |
| External name | | |
| Outlet pressure bars | 1.4006 | 1.4572 |

.....

| | | | | |
|----------------------------|---------|---------|--------|---------|
| ***EXCHANGER/CONDENSERS*** | 2 | 3 | 4 | 7 |
| Equipment no. | | | | |
| External name | | | | |
| Heat transfer coeff. | 300.00 | 300.00 | 300.00 | .00000 |
| Area | 5.7562 | 5.8855 | .53238 | .00000 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 3.0 | 3.0 | 3.0 | 5.0 |
| Min. delta T or T-out | 6.00 | 3.00 | 7.00 | -175.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | -10.614 | -7.1327 | 1.3775 | .15194 |
| Water usage, DM3/hr | .00000 | .00000 | .00000 | .00000 |
| Corrected delta T | 6.15 | 4.04 | 8.62 | 8.62 |
| Equipment no. | 10 | | | |
| External name | | | | |
| Heat transfer coeff. | .00000 | | | |
| Area | .00000 | | | |
| Number of shells | .0 | | | |
| Shell passes | .0 | | | |
| Tube passes | .0 | | | |
| Mode | 5.0 | | | |
| Min. delta T or T-out | -180.00 | | | |
| Delta P, stream 1 | .00000 | | | |
| Delta P, stream 2 | .00000 | | | |
| Q, stream 1 MJ/hr | 1.1303 | | | |
| Water usage, DM3/hr | .00000 | | | |
| Corrected delta T | 8.62 | | | |

.....

*** PUMPS/COMPRESSORS ***

186

Equipment no. 8
 External name
 Number of stages .0
 Work capacity MJ/hr .00000
 Outlet pressure bars 190.00
 Power type: .0
 (+) steam
 (0) electricity
 (-) fuel gas
 H. steam out KJ / kg .00000
 Fuel usage, M3 /hr .00000
 Water usage, DM3/hr .00000
 Steam usage Tonnes/hr .00000
 Kilowatt usage 1.1632

.....

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*** RIGOROUS TOWERS ***

Equipment no. 1 7
 External name
 Number of stages 21.0 57.0
 Feed 1, stage # 15.0 1.0
 Feed 2, stage # 21.0 17.0
 Feed 3, stage # .0 .0
 Feed 4, stage # .0 .0
 Feed 5, stage # .0 .0
 Sidestream # 1 stage .0 .0
 Sidestream # 2 stage .0 .0
 Sidestream # 3 stage .0 .0
 Sidestream # 4 stage .0 .0
 Cond. pressure bars 6.7131 1.4006
 Cond. delta P bars .00000 .00000
 Colm. delta P bars .19400E-01 .19850
 Condenser type .0 1.0
 Condenser mode 4.0 .0
 Value of cond. spec. 16.000 .00000
 Cond comp 1 position 1.0 .0
 Cond comp 2 position .0 .0
 Cond. deg. subcooled 1.00 .00
 Reboiler mode .0 4.0
 Val. of reboiler spec .00000 7.6000
 Rebr comp 1 position .0 2.0
 Rebr comp 2 position .0 .0
 Damping ratio .00000 1.0000
 Sidestream 1 mode .0 .0
 Sidestream 2 mode .0 .0
 Sidestream 3 mode .0 .0
 Sidestream 4 mode .0 .0
 Sidestream # 1 spec .00000 .00000
 Sidestream # 2 spec .00000 .00000
 Sidestream # 3 spec .00000 .00000
 Sidestream # 4 spec .00000 .00000
 Sidestrm 1 comp posn .0 .0
 Sidestrm 2 comp posn .0 .0
 Sidestrm 3 comp posn .0 .0

| | | |
|------------------------|---------|---------|
| Sidestrn 4 comp posn | .0 | .0 |
| Cond. duty MJ/hr | -163.53 | .00000 |
| Rebr duty MJ/hr | .00000 | 153.21 |
| Est dist rate Kgmol/hr | 16.000 | .00000 |
| Est. reflux Kgmol/hr | .00000 | .00000 |
| Est. side draw rate 1 | .00000 | .00000 |
| Est. side draw rate 2 | .00000 | .00000 |
| Est. side draw rate 3 | .00000 | .00000 |
| Est. side draw rate 4 | .00000 | .00000 |
| Est. temp stg 1 C | -178.00 | -193.00 |
| Est. temp stg N C | -174.00 | -183.00 |

187

CODE REPORT

*** Stream no. 1 ***

| | Overall | Vapor | Liquid |
|----------------------------|----------|-------------|-------------|
| Temperature deg C. | -172.366 | | |
| Pressure bars. . . | 6.61325 | | |
| Vapor fraction . . . | .817724 | | |
| Enthalpy MJ/hr | 214.671 | 187.651 | 27.0201 |
| Entropy MJ/hr*K | -.474310 | -.269548 | -.204763 |
| Ave. mol. wt. . . . | 28.7704 | 28.6655 | 29.2409 |
| Total flow kg/hr | 460.324 | 375.046 | 85.2782 |
| kgmol/hr | 15.9999 | 13.0835 | 2.91641 |
| Density kg/m3 | | 26.7085 | 1406.48 |
| Viscosity centipoise | | .690154E-02 | .103552 |
| Thermal cond. cal/cm*s*K | | .357676E-04 | .505017E-03 |
| Specific heat kJ/kg*K | | 1.25193 | 2.17510 |
| Z factor | | .847052 | |
| m3/hr (15.6 deg C & 1 atm) | | 309.950 | |
| Vol. flowrate m3/hr | | 14.0424 | |
| Surface tension dyne/cm. | | | 5.67519 |
| B. G. (60/60) | | | .915033 |
| m3/hr (15.6 deg C & 1 atm) | | | .933430E-01 |
| Vol. flowrate m3/hr | | | .606330E-01 |
| | Vapor | Liquid | |
| | mole | mole | |
| | fraction | fraction | |
| | | | Vapor |
| | | | flowrate |
| | | | kgmol/hr |
| Nitrogen | .83630 | .69196 | 10.9418 |
| Oxygen | .16370 | .30804 | 2.14175 |
| | | | .898379 |

*** Stream no. 2 ***

| | Overall | Vapor | Liquid |
|----------------------------|----------|-------------|-------------|
| Temperature deg C. | -172.347 | | |
| Pressure bars. . . | 6.60647 | | |
| Vapor fraction . . . | .832464 | | |
| Enthalpy MJ/hr | 323.802 | 286.566 | 37.2358 |
| Entropy MJ/hr*K | -.693623 | -.411253 | -.282370 |
| Ave. mol. wt. . . . | 28.7702 | 28.6730 | 29.2536 |
| Total flow kg/hr | 690.486 | 572.861 | 117.625 |
| kgmol/hr | 24.0000 | 19.9791 | 4.02087 |
| Density kg/m3 | | 26.6758 | 1407.54 |
| Viscosity centipoise | | .690418E-02 | .103704 |
| Thermal cond. cal/cm*s*K | | .357676E-04 | .504990E-03 |
| Specific heat kJ/kg*K | | 1.25085 | 2.17289 |
| Z factor | | .847282 | |
| m3/hr (15.6 deg C & 1 atm) | | 473.307 | |
| Vol. flowrate m3/hr | | 21.4752 | |
| Surface tension dyne/cm. | | | 5.69055 |

| | | | | |
|----------------------------|-----------|-----------|-----------|-------------|
| S. G. (60/60) | | | | .915375 |
| m3/hr (15.6 deg C & 1 atm) | | | | .128700 |
| Vol. flowrate m3/hr | | | | .835686E-01 |
| | Vapor | Liquid | Vapor | Liquid |
| | mole | mole | flowrate | flowrate |
| | fraction | fraction | kgmol/hr | kgmol/hr |
| Nitrogen | .83443 | .68876 | 16.6712 | 2.76943 |
| Oxygen | .16557 | .31124 | 3.30796 | 1.25144 |

CODE REPORT

*** Stream no. 3 ***

| | | |
|----------------------------|-------------|-------------|
| | | All Liquid |
| Temperature deg C. | | -175.936 |
| Pressure bars. | | 6.71314 |
| Enthalpy MJ/hr | | 152.106 |
| Entropy MJ/hr*K | | -1.12246 |
| Ave. mol. wt. | | 28.0883 |
| Total flow kg/hr. | | 449.415 |
| | kgmol/hr | 16.0001 |
| Density kg/m3 | | 1329.85 |
| Viscosity centipoise | | .947183E-01 |
| Thermal cond. cal/cm*s*K | | .510523E-03 |
| Specific heat kJ/kg*K | | 2.34680 |
| Surface tension dyne/cm. | | 4.74204 |
| S. G. (60/60) | | .893883 |
| m3/hr (15.6 deg C & 1 atm) | | .509252 |
| Vol. flowrate m3/hr | | .337948 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .981119 | 15.6980 |
| Oxygen | .188808E-01 | .302095 |

*** Stream no. 4 ***

| | | |
|----------------------------|-----------|-------------|
| | | All Liquid |
| Temperature deg C. | | -172.151 |
| Pressure bars. | | 6.73254 |
| Enthalpy MJ/hr | | 222.844 |
| Entropy MJ/hr*K | | -1.68106 |
| Ave. mol. wt. | | 29.2250 |
| Total flow kg/hr. | | 701.395 |
| | kgmol/hr | 23.9999 |
| Density kg/m3 | | 1402.47 |
| Viscosity centipoise | | .102867 |
| Thermal cond. cal/cm*s*K | | .504666E-03 |
| Specific heat kJ/kg*K | | 2.18426 |
| Surface tension dyne/cm. | | 5.60303 |
| S. G. (60/60) | | .914606 |
| m3/hr (15.6 deg C & 1 atm) | | .768084 |
| Vol. flowrate m3/hr | | .500121 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .695938 | 16.7024 |
| Oxygen | .304062 | 7.29745 |

CODE REPORT

*** Stream no. 5 ***

| | | |
|--------------------|-----------|------------|
| | | All Liquid |
| Temperature deg C. | | -186.647 |

```

Pressure bars. . . . . 6.71314
Enthalpy MJ/hr . . . . . 141.493
Entropy MJ/hr*K . . . . . -1.23802
Ave. mol. wt. . . . . 28.0883
Total flow kg/hr. . . . . 449.415
      kgmol/hr . . . . . 16.0001
Density kg/m3 . . . . . 1445.97
Viscosity centipoise . . . . . .123407
Thermal cond. cal/cm*s*K . . . . . .527857E-03
Specific heat kJ/kg*K . . . . . 2.09369
Surface tension dyne/cm. . . . . 6.98386
S. G. (60/60) . . . . . .883883
m3/hr (15.6 deg C & 1 atm) . . . . . .509252
Vol. flowrate m3/hr . . . . . .310809
      Liquid      Liquid
      mole      flowrate
      fraction  kgmol/hr
Nitrogen .981119 15.6980
Oxygen .188808E-01 .302095
  
```

*** Stream no. 6 ***

```

All Liquid
Temperature deg C. . . . . -176.935
Pressure bars. . . . . 6.73254
Enthalpy MJ/hr . . . . . 215.711
Entropy MJ/hr*K . . . . . -1.75337
Ave. mol. wt. . . . . 29.2250
Total flow kg/hr. . . . . 701.395
      kgmol/hr . . . . . 23.9999
Density kg/m3 . . . . . 1454.64
Viscosity centipoise . . . . . .113776
Thermal cond. cal/cm*s*K . . . . . .512408E-03
Specific heat kJ/kg*K . . . . . 2.06976
Surface tension dyne/cm. . . . . 6.67650
S. G. (60/60) . . . . . .914606
m3/hr (15.6 deg C & 1 atm) . . . . . .768084
Vol. flowrate m3/hr . . . . . .482182
      Liquid      Liquid
      mole      flowrate
      fraction  kgmol/hr
Nitrogen .695938 16.7024
Oxygen .304062 7.29745
  
```

CODE REPORT

*** Stream no. 7 ***

| | Overall | Vapor | Liquid |
|----------------------------|-------------|--------------|-------------|
| Temperature deg C. | -192.652 | | |
| Pressure bars. | 1.40055 | | |
| Vapor fraction | .668986E-01 | | |
| Enthalpy MJ/hr | 141.493 | 15.1463 | 126.409 |
| Entropy MJ/hr*K | -1.23147 | -.139799E-01 | -1.21749 |
| Ave. mol. wt. | 28.0883 | 28.0396 | 28.0918 |
| Total flow kg/hr | 449.415 | 30.0132 | 419.402 |
| kgmol/hr | 16.0001 | 1.07038 | 14.9297 |
| Density kg/m3 | | 6.12529 | 1503.80 |
| Viscosity centipoise | | .541943E-02 | .147473 |
| Thermal cond. cal/cm*s*K | | .340943E-04 | .537581E-03 |
| Specific heat kJ/kg*K | | 1.13199 | 1.97733 |
| Z factor | | .947868 | |
| m3/hr (15.6 deg C & 1 atm) | | 25.6268 | |

| | | | | |
|----------------------------|------------|------------|-------------|----------|
| Vol. flowrate m3/hr | | | 4.89995 | |
| Surface tension dyne/cm. | | | | 8.31471 |
| S. G. (60/60) | | | | .883978 |
| m3/hr (15.6 deg C & 1 atm) | | | | .475192 |
| Vol. flowrate m3/hr | | | | .278897 |
| | Vapor | Liquid | Vapor | Liquid |
| | mole | mole | flowrate | flowrate |
| | fraction | fraction | kgmol/hr | kgmol/hr |
| Nitrogen | .99332 | .98023 | 1.06323 | 14.6346 |
| Oxygen | .66838E-02 | .19765E-01 | .715428E-02 | .295089 |

*** Stream no. 8 ***

| | Overall | | Vapor | | Liquid |
|----------------------------|----------|----------|--------------|--|-------------|
| Temperature deg C. | -190.027 | | | | |
| Pressure bars. | 1.45725 | | | | |
| Vapor fraction | .138577 | | | | |
| Enthalpy MJ/hr | 215.711 | | 46.6854 | | 168.988 |
| Entropy MJ/hr*K | -1.73072 | | -.409738E-01 | | -1.68975 |
| Ave. mol. wt. | 29.2250 | | 28.5267 | | 29.3371 |
| Total flow kg/hr | 701.395 | | 94.8750 | | 606.515 |
| kgmol/hr | 23.9999 | | 3.32583 | | 20.6740 |
| Density kg/m3 | | | 6.34762 | | 1590.31 |
| Viscosity centipoise | | | .566974E-02 | | .161625 |
| Thermal cond. cal/cm*s*K | | | .339222E-04 | | .533619E-03 |
| Specific heat kJ/kg*K | | | 1.10301 | | 1.84662 |
| Z factor | | | .949507 | | |
| m3/hr (15.6 deg C & 1 atm) | | | 78.6319 | | |
| Vol. flowrate m3/hr | | | 14.9468 | | |
| Surface tension dyne/cm. | | | | | 9.92894 |
| S. G. (60/60) | | | | | .917617 |
| m3/hr (15.6 deg C & 1 atm) | | | | | .662004 |
| Vol. flowrate m3/hr | | | | | .381387 |
| | Vapor | Liquid | Vapor | | Liquid |
| | mole | mole | flowrate | | flowrate |
| | fraction | fraction | kgmol/hr | | kgmol/hr |
| Nitrogen | .87111 | .66782 | 2.89717 | | 13.8066 |
| Oxygen | .12889 | .33218 | .428659 | | 6.86744 |

CODE REPORT

*** Stream no. 9 ***

| | Overall | | Vapor | | Liquid |
|----------------------------|----------|--|--------------|--|-------------|
| Temperature deg C. | -190.008 | | | | |
| Pressure bars. | 1.45725 | | | | |
| Vapor fraction | .148943 | | | | |
| Enthalpy MJ/hr | 217.088 | | 50.2454 | | 166.870 |
| Entropy MJ/hr*K | -1.71318 | | -.440287E-01 | | -1.66915 |
| Ave. mol. wt. | 29.2250 | | 28.5310 | | 29.3463 |
| Total flow kg/hr | 701.395 | | 101.987 | | 599.406 |
| kgmol/hr | 23.9999 | | 3.57461 | | 20.4252 |
| Density kg/m3 | | | 6.33859 | | 1590.93 |
| Viscosity centipoise | | | .567168E-02 | | .161681 |
| Thermal cond. cal/cm*s*K | | | .339417E-04 | | .533592E-03 |
| Specific heat kJ/kg*K | | | 1.10308 | | 1.84427 |
| Z factor | | | .949532 | | |
| m3/hr (15.6 deg C & 1 atm) | | | 84.6253 | | |
| Vol. flowrate m3/hr | | | 16.0901 | | |
| Surface tension dyne/cm. | | | | | 9.94126 |
| S. G. (60/60) | | | | | .917866 |
| m3/hr (15.6 deg C & 1 atm) | | | | | .654067 |
| Vol. flowrate m3/hr | | | | | .376768 |

| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr | Liquid flowrate kgmol/hr |
|----------|---------------------------|----------------------------|-------------------------------|--------------------------------|
| Nitrogen | .87004 | .66549 | 3.11004 | 13.5929 |
| Oxygen | .12996 | .33451 | .464567 | 6.83238 |

*** Stream no. 10 ***

| | All Vapor |
|--------------------------------------|-------------|
| Temperature deg C. | -192.647 |
| Pressure bars. | 1.40055 |
| Enthalpy MJ/hr | 453.660 |
| Entropy MJ/hr*K | -.421952 |
| Ave. mol. wt. | 28.0407 |
| Total flow kg/hr. | 908.515 |
| kgmol/hr | 32.3999 |
| Density kg/m3 | 6.19011 |
| Viscosity centipoise | .541992E-02 |
| Thermal cond. cal/cm*s*K | .339356E-04 |
| Specific heat kJ/kg*K | 1.13097 |
| Z factor | .947875 |
| m3/hr (15.6 deg C & 1 atm) | 767.560 |
| Vol. flowrate m3/hr | 146.771 |

| | Vapor mole fraction | Vapor flowrate kgmol/hr |
|----------|---------------------------|-------------------------------|
| Nitrogen | .993061 | 32.1751 |
| Oxygen | .693924E-02 | .224831 |

CODE REPORT

*** Stream no. 11 ***

| | All Liquid |
|--------------------------------------|-------------|
| Temperature deg C. | -179.524 |
| Pressure bars. | 1.59905 |
| Enthalpy MJ/hr | 58.1288 |
| Entropy MJ/hr*K | -.604787 |
| Ave. mol. wt. | 31.8808 |
| Total flow kg/hr. | 242.295 |
| kgmol/hr | 7.60001 |
| Density kg/m3 | 1708.80 |
| Viscosity centipoise | .175472 |
| Thermal cond. cal/cm*s*K | .517224E-03 |
| Specific heat kJ/kg*K | 1.63202 |
| Surface tension dyne/cm. | 12.0760 |
| S. G. (60/60) | .985091 |
| m3/hr (15.6 deg C & 1 atm) | .246347 |
| Vol. flowrate m3/hr | .141794 |

| | Liquid mole fraction | Liquid flowrate kgmol/hr |
|----------|----------------------------|--------------------------------|
| Nitrogen | .296430E-01 | .225287 |
| Oxygen | .970357 | 7.37472 |

*** Stream no. 12 ***

| | All Liquid |
|----------------------------|------------|
| Temperature deg C. | -183.027 |
| Pressure bars. | 1.59905 |
| Enthalpy MJ/hr | 56.7513 |
| Entropy MJ/hr*K | -.619821 |
| Ave. mol. wt. | 31.8809 |
| Total flow kg/hr. | 242.294 |

kgmol/hr 7.59999
 Density kg/m3 1736.77
 Viscosity centipoise 190473
 Thermal cond. cal/cm*s*K 522893E-03
 Specific heat kJ/kg*K 1.61429
 Surface tension dyne/cm. 12.9410
 S. G. (60/60) 985091
 m3/hr (15.6 deg C & 1 atm) 246347
 Vol. flowrate m3/hr 139510
 Liquid mole fraction
 Nitrogen .296411E-01 .225272
 Oxygen .970359 .7.37472
 CODE REPORT

*** Stream no. 13 ***

All Vapor
 Temperature deg C. -182.231
 Pressure bars. 1.40055
 Enthalpy MJ/hr 464.274
 Entropy MJ/hr*K -.297945
 Ave. mol. wt. 28.0407
 Total flow kg/hr. 908.515
 kgmol/hr 32.3999
 Density kg/m3 5.40047
 Viscosity centipoise612500E-02
 Thermal cond. cal/cm*s*K350415E-04
 Specific heat kJ/kg*K 1.11274
 Z factor961997
 m3/hr (15.6 deg C & 1 atm) 767.562
 Vol. flowrate m3/hr 168.231
 Vapor mole fraction
 Nitrogen .993061 32.1751
 Oxygen .693924E-02 .224831

*** Stream no. 14 ***

All Liquid
 Temperature deg C. -183.027
 Pressure bars. 190.000
 Enthalpy MJ/hr 59.0741
 Entropy MJ/hr*K -.632918
 Ave. mol. wt. 31.8809
 Total flow kg/hr. 242.294
 kgmol/hr 7.59999
 Density kg/m3 1851.29
 Viscosity centipoise 190473
 Thermal cond. cal/cm*s*K 522893E-03
 Specific heat kJ/kg*K 1.53771
 Surface tension dyne/cm. 12.9159
 S. G. (60/60) 985091
 m3/hr (15.6 deg C & 1 atm) 246347
 Vol. flowrate m3/hr 130880
 Liquid mole fraction
 Nitrogen .296411E-01 .225272
 Oxygen .970359 7.37472

*** Stream no. 15 ***

| | | |
|--------------------------------------|-------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -175.151 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 471.407 |
| Entropy MJ/hr*K | | -.222392 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 908.515 |
| kgmol/hr | | 32.3999 |
| Density kg/m3 | | 4.97526 |
| Viscosity centipoise | | .660189E-02 |
| Thermal cond. cal/cm*s*K | | .358105E-04 |
| Specific heat kJ/kg*K | | 1.10448 |
| Z factor | | .968776 |
| m3/hr (15.6 deg C & 1 atm) | | 767.562 |
| Vol. flowrate m3/hr | | 182.609 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .993061 | 32.1751 |
| Oxygen | .693924E-02 | .224831 |

*** Stream no. 16 ***

| | | |
|--------------------------------------|-------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -175.000 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 471.558 |
| Entropy MJ/hr*K | | -.220847 |
| Ave. mol. wt. | | 28.0407 |
| Total flow kg/hr. | | 908.515 |
| kgmol/hr | | 32.3999 |
| Density kg/m3 | | 4.96695 |
| Viscosity centipoise | | .661202E-02 |
| Thermal cond. cal/cm*s*K | | .358270E-04 |
| Specific heat kJ/kg*K | | 1.10414 |
| Z factor | | .968902 |
| m3/hr (15.6 deg C & 1 atm) | | 767.562 |
| Vol. flowrate m3/hr | | 182.915 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .993061 | 32.1751 |
| Oxygen | .693924E-02 | .224831 |

CODE REPORT

*** Stream no. 17 ***

| | | |
|------------------------------------|--|-------------|
| | | All Liquid |
| Temperature deg C. | | -180.000 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 60.2043 |
| Entropy MJ/hr*K | | -.620582 |
| Ave. mol. wt. | | 31.8809 |
| Total flow kg/hr. | | 242.294 |
| kgmol/hr | | 7.59999 |
| Density kg/m3 | | 1832.13 |
| Viscosity centipoise | | .177374 |
| Thermal cond. cal/cm*s*K | | .517974E-03 |
| Specific heat kJ/kg*K | | 1.54416 |

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 | |
|-----|--------------------|---------------|--------------------------------|------------------------------|---------|----------------------------|------|
| 1 | 514.0 | 28.09 | .50 | 107 | 1329.83 | .0947 | 4.74 |
| 2 | 519.4 | 28.17 | .59 | .39 | 1324.15 | .0934 | 4.62 |
| 3 | 517.4 | 28.25 | .58 | .39 | 1330.76 | .0941 | 4.69 |
| 4 | 515.4 | 28.34 | .58 | .39 | 1337.70 | .0949 | 4.78 |
| 5 | 513.3 | 28.44 | .58 | .38 | 1344.85 | .0957 | 4.87 |
| 6 | 511.2 | 28.53 | .57 | .38 | 1352.06 | .0966 | 4.95 |
| 7 | 509.1 | 28.63 | .57 | .37 | 1359.18 | .0974 | 5.04 |
| 8 | 506.7 | 28.72 | .56 | .37 | 1366.03 | .0983 | 5.13 |
| 9 | 505.6 | 28.80 | .56 | .37 | 1372.47 | .0991 | 5.21 |
| 10 | 503.8 | 28.89 | .56 | .37 | 1378.42 | .0998 | 5.29 |
| 11 | 502.3 | 28.96 | .55 | .36 | 1383.77 | .1005 | 5.36 |
| 12 | 501.0 | 29.03 | .55 | .36 | 1388.50 | .1011 | 5.42 |
| 13 | 500.1 | 29.08 | .55 | .36 | 1392.60 | .1016 | 5.47 |
| 14 | 499.1 | 29.13 | .55 | .36 | 1396.11 | .1020 | 5.52 |
| 15 | 584.2 | 29.17 | .64 | .42 | 1399.05 | .1024 | 5.56 |
| 16 | 584.0 | 29.18 | .64 | .42 | 1399.15 | .1024 | 5.56 |
| 17 | 584.1 | 29.18 | .64 | .42 | 1399.33 | .1025 | 5.56 |
| 18 | 584.0 | 29.18 | .64 | .42 | 1399.65 | .1025 | 5.57 |
| 19 | 583.7 | 29.19 | .64 | .42 | 1400.20 | .1026 | 5.57 |
| 20 | 583.5 | 29.20 | .64 | .42 | 1401.05 | .1027 | 5.58 |
| 21 | 701.4 | 29.22 | .77 | .50 | 1402.45 | .1029 | 5.60 |

Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|---|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 1 | *** Total Condenser : No Vapor Outlet *** | | | | | |
| 2 | 963.4 | 28.09 | 812.5 | 34.93 | .8356 | 27.5835 |
| 3 | 968.8 | 28.13 | 815.9 | 35.17 | .8364 | 27.5503 |
| 4 | 966.8 | 28.18 | 812.9 | 35.14 | .8372 | 27.5146 |
| 5 | 964.8 | 28.22 | 809.8 | 35.11 | .8380 | 27.4772 |
| 6 | 962.7 | 28.27 | 806.7 | 35.08 | .8388 | 27.4394 |
| 7 | 960.6 | 28.32 | 803.5 | 35.06 | .8397 | 27.4016 |
| 8 | 958.5 | 28.37 | 800.4 | 35.03 | .8405 | 27.3653 |
| 9 | 956.1 | 28.42 | 797.0 | 34.98 | .8413 | 27.3308 |
| 10 | 955.0 | 28.46 | 794.8 | 34.98 | .8420 | 27.2991 |
| 11 | 953.3 | 28.50 | 792.3 | 34.96 | .8426 | 27.2702 |
| 12 | 951.7 | 28.54 | 790.0 | 34.93 | .8432 | 27.2451 |
| 13 | 950.4 | 28.57 | 788.0 | 34.91 | .8437 | 27.2240 |
| 14 | 949.5 | 28.60 | 786.4 | 34.90 | .8442 | 27.2059 |
| 15 | 948.5 | 28.63 | 784.9 | 34.88 | .8446 | 27.1917 |
| 16 | 573.2 | 28.63 | 474.3 | 21.08 | .8446 | 27.1746 |
| 17 | 573.1 | 28.63 | 474.2 | 21.07 | .8446 | 27.1973 |
| 18 | 573.2 | 28.63 | 474.2 | 21.07 | .8446 | 27.1993 |
| 19 | 573.1 | 28.64 | 474.1 | 21.07 | .8446 | 27.2003 |
| 20 | 572.8 | 28.65 | 473.7 | 21.06 | .8448 | 27.1986 |
| 21 | 572.6 | 28.66 | 473.3 | 21.06 | .8449 | 27.1935 |

CODE: Chemical Engineering Simulation System
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TOWER # 1 Data file: column.TSZ Profile file: link.prf

Smith-Dresser-Ohlswager Shortcut Technique

User Provided Input Data

Tray spacing (in. or cm) 7.0000
 Downcomer area (ft2 or m2) .0151
 Weir length (in. or cm) 24.0000
 Weir height (in. or cm) 3.0000

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|---------------------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 1 | ***Condenser: No tray sizing*** | | | | | | |
| 2 | .3051 | .01 | .01 | 1324.1490 | 27.5839 | .1672 | .0361 |
| 3 | .3053 | .01 | .01 | 1330.7550 | 27.5507 | .1681 | .0361 |
| 4 | .3047 | .01 | .01 | 1337.6980 | 27.5150 | .1689 | .0361 |
| 5 | .3040 | .01 | .01 | 1344.8480 | 27.4776 | .1696 | .0361 |
| 6 | .3034 | .01 | .01 | 1352.0650 | 27.4397 | .1704 | .0362 |
| 7 | .3028 | .01 | .01 | 1359.1760 | 27.4020 | .1711 | .0362 |
| 8 | .3022 | .01 | .01 | 1366.0340 | 27.3657 | .1718 | .0362 |
| 9 | .3016 | .01 | .01 | 1372.4660 | 27.3312 | .1724 | .0362 |
| 10 | .3012 | .01 | .01 | 1378.4210 | 27.2995 | .1731 | .0362 |
| 11 | .3007 | .01 | .01 | 1383.7730 | 27.2706 | .1736 | .0363 |
| 12 | .3003 | .01 | .01 | 1388.5020 | 27.2455 | .1741 | .0363 |
| 13 | .3000 | .01 | .01 | 1392.6050 | 27.2244 | .1745 | .0363 |
| 14 | .2997 | .01 | .01 | 1396.1050 | 27.2063 | .1749 | .0363 |
| 15 | .3029 | .01 | .01 | 1399.0530 | 27.1921 | .1701 | .0359 |
| 16 | .2615 | .01 | .01 | 1399.1530 | 27.1950 | .1517 | .0359 |
| 17 | .2615 | .01 | .01 | 1399.3330 | 27.1977 | .1517 | .0359 |
| 18 | .2615 | .01 | .01 | 1399.6530 | 27.1997 | .1517 | .0359 |
| 19 | .2614 | .01 | .01 | 1400.1980 | 27.2007 | .1517 | .0359 |
| 20 | .2613 | .01 | .01 | 1401.0550 | 27.1990 | .1518 | .0359 |
| 21 | .2661 | .01 | .01 | 1402.4480 | 27.1939 | .1444 | .0354 |

CODE REPORT

TOWER # 2 Data file: column.OUT Profile file: pool.prf

Column Summary

| Stg | Temp C | Pres bars | Net Flow Rates kgmols/hr | | | Duties MJ/hr |
|-----|-----------|--------------|-----------------------------|--------|--------|-----------------|
| | | | Liquid | Vapor | Feed | |
| | | | | | 16.000 | 32.400 |
| 1 | -192.6 | 1.401 | 14.924 | | | |
| 2 | -192.6 | 1.404 | 14.920 | 31.324 | | |
| 3 | -192.6 | 1.408 | 14.915 | 31.320 | | |
| 4 | -192.5 | 1.411 | 14.907 | 31.315 | | |
| 5 | -192.5 | 1.415 | 14.896 | 31.307 | | |
| 6 | -192.5 | 1.418 | 14.881 | 31.296 | | |
| 7 | -192.4 | 1.422 | 14.861 | 31.281 | | |
| 8 | -192.3 | 1.425 | 14.832 | 31.261 | | |
| 9 | -192.2 | 1.429 | 14.794 | 31.232 | | |
| 10 | -192.1 | 1.432 | 14.742 | 31.194 | | |
| 11 | -192.0 | 1.436 | 14.674 | 31.142 | | |
| 12 | -191.8 | 1.440 | 14.587 | 31.074 | | |
| 13 | -191.6 | 1.443 | 14.478 | 30.987 | | |
| 14 | -191.3 | 1.447 | 14.348 | 30.878 | | |
| 15 | -191.0 | 1.450 | 14.199 | 30.748 | | |
| 16 | -190.6 | 1.454 | 14.037 | 30.598 | | |
| 17 | -190.2 | 1.457 | 34.458 | 30.437 | 24.000 | |
| 18 | -190.2 | 1.461 | 34.463 | 26.858 | | |
| 19 | -190.2 | 1.464 | 34.468 | 26.863 | | |

| | | | | | |
|----|--------|-------|--------|--------|--|
| 20 | -190.2 | 1.468 | 34.473 | 26.868 | |
| 21 | -190.2 | 1.471 | 34.478 | 26.873 | |
| 22 | -190.1 | 1.475 | 34.483 | 26.878 | |
| 23 | -190.1 | 1.479 | 34.488 | 26.883 | |
| 24 | -190.1 | 1.482 | 34.493 | 26.888 | |
| 25 | -190.1 | 1.486 | 34.498 | 26.893 | |
| 26 | -190.0 | 1.489 | 34.503 | 26.898 | |
| 27 | -190.0 | 1.493 | 34.508 | 26.903 | |
| 28 | -190.0 | 1.496 | 34.513 | 26.908 | |
| 29 | -190.0 | 1.500 | 34.518 | 26.913 | |
| 30 | -189.9 | 1.503 | 34.523 | 26.918 | |
| 31 | -189.9 | 1.507 | 34.528 | 26.923 | |
| 32 | -189.9 | 1.510 | 34.533 | 26.928 | |
| 33 | -189.9 | 1.514 | 34.538 | 26.933 | |
| 34 | -189.8 | 1.518 | 34.542 | 26.938 | |
| 35 | -189.8 | 1.521 | 34.547 | 26.943 | |
| 36 | -189.8 | 1.525 | 34.552 | 26.947 | |
| 37 | -189.8 | 1.528 | 34.557 | 26.952 | |
| 38 | -189.8 | 1.532 | 34.562 | 26.957 | |
| 39 | -189.7 | 1.535 | 34.567 | 26.962 | |
| 40 | -189.7 | 1.539 | 34.572 | 26.967 | |
| 41 | -189.7 | 1.542 | 34.577 | 26.972 | |
| 42 | -189.7 | 1.546 | 34.582 | 26.977 | |
| 43 | -189.6 | 1.549 | 34.587 | 26.982 | |
| 44 | -189.6 | 1.553 | 34.591 | 26.987 | |
| 45 | -189.6 | 1.557 | 34.595 | 26.991 | |
| 46 | -189.6 | 1.560 | 34.600 | 26.995 | |
| 47 | -189.5 | 1.564 | 34.602 | 27.000 | |

197

| CODE REPORT | Liquid | Vapor | Feed | Product |
|-------------|--------|--------------|--------|---------------|
| 48 | -189.5 | 1.567 34.601 | 27.002 | |
| 49 | -189.5 | 1.571 34.590 | 27.001 | |
| 50 | -189.4 | 1.574 34.554 | 26.990 | |
| 51 | -189.3 | 1.578 34.451 | 26.954 | |
| 52 | -189.0 | 1.581 34.183 | 26.851 | |
| 53 | -188.3 | 1.585 33.566 | 26.583 | |
| 54 | -186.7 | 1.588 32.488 | 25.966 | |
| 55 | -184.1 | 1.592 31.381 | 24.888 | |
| 56 | -181.3 | 1.596 30.829 | 23.781 | |
| 57 | -179.5 | 1.599 | 23.229 | 7.6000 153.21 |

Stream # 7 fed to Stg 1 is 6.690 % Vapor
 Stream # 9 fed to Stg 17 is 14.894 % Vapor

Stream # 10 is Vapor Distillate from Stg 1
 Stream # 11 is Liquid Bottoms from Stg 57

Condenser duty is .000000 MJ/hr
 Reboiler duty is 153.208 MJ/hr
 CODE REPORT

TOWER # 2 Data file: column.OUT Profile file: pool.prf
 Tray Liquid Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise | Surface tension dyne/cm |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|

| | | | | | | | |
|----|--------|-------|------|-----|---------|-------|------|
| 1 | 419.3 | 28.09 | .48 | .28 | 1504.01 | .1477 | 0.32 |
| 2 | 419.2 | 28.10 | .47 | .28 | 1504.12 | .1477 | 0.32 |
| 3 | 419.2 | 28.11 | .47 | .28 | 1504.37 | .1476 | 0.32 |
| 4 | 419.1 | 28.11 | .47 | .28 | 1504.79 | .1476 | 0.33 |
| 5 | 419.0 | 28.12 | .47 | .28 | 1505.45 | .1477 | 0.34 |
| 6 | 418.8 | 28.14 | .47 | .28 | 1506.43 | .1477 | 0.36 |
| 7 | 418.5 | 28.16 | .47 | .28 | 1507.85 | .1479 | 0.38 |
| 8 | 418.1 | 28.19 | .47 | .28 | 1509.87 | .1482 | 0.42 |
| 9 | 417.6 | 28.23 | .47 | .28 | 1512.67 | .1485 | 0.47 |
| 10 | 417.0 | 28.28 | .47 | .27 | 1516.47 | .1491 | 0.53 |
| 11 | 416.1 | 28.35 | .47 | .27 | 1521.52 | .1499 | 0.63 |
| 12 | 414.9 | 28.45 | .47 | .27 | 1528.09 | .1509 | 0.75 |
| 13 | 413.5 | 28.56 | .46 | .27 | 1536.33 | .1522 | 0.90 |
| 14 | 411.8 | 28.70 | .46 | .27 | 1546.30 | .1539 | 0.08 |
| 15 | 409.8 | 28.86 | .45 | .26 | 1557.78 | .1558 | 0.30 |
| 16 | 407.7 | 29.04 | .45 | .26 | 1570.25 | .1580 | 0.54 |
| 17 | 1007.2 | 29.23 | 1.10 | .64 | 1582.90 | .1602 | 0.78 |
| 18 | 1007.3 | 29.23 | 1.10 | .64 | 1582.70 | .1601 | 0.78 |
| 19 | 1007.5 | 29.23 | 1.10 | .64 | 1582.51 | .1600 | 0.77 |
| 20 | 1007.6 | 29.23 | 1.10 | .64 | 1582.31 | .1598 | 0.77 |
| 21 | 1007.8 | 29.23 | 1.10 | .64 | 1582.10 | .1597 | 0.76 |
| 22 | 1007.9 | 29.23 | 1.10 | .64 | 1581.91 | .1596 | 0.76 |
| 23 | 1008.1 | 29.23 | 1.10 | .64 | 1581.71 | .1595 | 0.75 |
| 24 | 1008.2 | 29.23 | 1.10 | .64 | 1581.51 | .1594 | 0.75 |
| 25 | 1008.4 | 29.23 | 1.10 | .64 | 1581.31 | .1593 | 0.74 |
| 26 | 1008.5 | 29.23 | 1.10 | .64 | 1581.12 | .1592 | 0.74 |
| 27 | 1008.6 | 29.23 | 1.10 | .64 | 1580.92 | .1591 | 0.73 |
| 28 | 1008.8 | 29.23 | 1.10 | .64 | 1580.72 | .1590 | 0.72 |
| 29 | 1008.9 | 29.23 | 1.10 | .64 | 1580.53 | .1589 | 0.72 |
| 30 | 1009.1 | 29.23 | 1.10 | .64 | 1580.33 | .1588 | 0.71 |
| 31 | 1009.2 | 29.23 | 1.11 | .64 | 1580.14 | .1587 | 0.71 |
| 32 | 1009.4 | 29.23 | 1.11 | .64 | 1579.94 | .1586 | 0.70 |
| 33 | 1009.5 | 29.23 | 1.11 | .64 | 1579.75 | .1584 | 0.70 |
| 34 | 1009.7 | 29.23 | 1.11 | .64 | 1579.55 | .1583 | 0.69 |
| 35 | 1009.8 | 29.23 | 1.11 | .64 | 1579.36 | .1582 | 0.69 |
| 36 | 1010.0 | 29.23 | 1.11 | .64 | 1579.16 | .1581 | 0.68 |
| 37 | 1010.1 | 29.23 | 1.11 | .64 | 1578.97 | .1580 | 0.68 |
| 38 | 1010.3 | 29.23 | 1.11 | .64 | 1578.78 | .1579 | 0.67 |
| 39 | 1010.4 | 29.23 | 1.11 | .64 | 1578.58 | .1578 | 0.67 |
| 40 | 1010.6 | 29.23 | 1.11 | .64 | 1578.39 | .1577 | 0.66 |
| 41 | 1010.7 | 29.23 | 1.11 | .64 | 1578.19 | .1576 | 0.66 |
| 42 | 1010.9 | 29.23 | 1.11 | .64 | 1578.01 | .1575 | 0.65 |
| 43 | 1011.0 | 29.23 | 1.11 | .64 | 1577.81 | .1574 | 0.65 |
| 44 | 1011.1 | 29.23 | 1.11 | .64 | 1577.62 | .1573 | 0.64 |
| 45 | 1011.3 | 29.23 | 1.11 | .64 | 1577.44 | .1572 | 0.63 |
| 46 | 1011.4 | 29.23 | 1.11 | .64 | 1577.27 | .1571 | 0.63 |
| 47 | 1011.5 | 29.23 | 1.11 | .64 | 1577.14 | .1570 | 0.63 |
| 48 | 1011.6 | 29.24 | 1.11 | .64 | 1577.14 | .1569 | 0.62 |
| 49 | 1011.5 | 29.24 | 1.11 | .64 | 1577.42 | .1569 | 0.63 |

CODE REPORT

TOWER # 2 Data file: column.OUT
Tray Liquid Properties

Profile file: pool.pdf

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise | Surface tension dyne/cm |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|
| 50 | 1011.1 | 29.26 | 1.11 | .64 | 1578.52 | .1571 | 9.65 |

| | | | | | | | |
|----|--------|-------|------|-----|---------|-------|-------|
| 51 | 1007.8 | 29.31 | 1.10 | .64 | 1581.72 | .1576 | 7.71 |
| 52 | 1006.4 | 29.44 | 1.10 | .63 | 1590.22 | .1591 | 9.07 |
| 53 | 998.6 | 29.75 | 1.08 | .62 | 1610.15 | .1627 | 10.26 |
| 54 | 986.0 | 30.35 | 1.05 | .60 | 1646.29 | .1692 | 10.78 |
| 55 | 976.1 | 31.10 | 1.01 | .58 | 1684.65 | .1753 | 11.72 |
| 56 | 975.4 | 31.64 | 1.00 | .57 | 1703.76 | .1764 | 12.04 |
| 57 | 242.3 | 31.88 | .25 | .14 | 1708.77 | .1755 | 12.08 |

CODE REPORT

TOWR # 2 Data file: column.OUT Profile file: pool.pr4
Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|--------------------|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 1 | 908.5 | 28.04 | 767.6 | 146.77 | .9479 | 6.1900 |
| 2 | 878.4 | 28.04 | 742.1 | 141.58 | .9478 | 6.2042 |
| 3 | 878.3 | 28.04 | 742.0 | 141.25 | .9477 | 6.2183 |
| 4 | 878.3 | 28.05 | 741.8 | 140.92 | .9476 | 6.2323 |
| 5 | 878.2 | 28.05 | 741.7 | 140.60 | .9476 | 6.2461 |
| 6 | 878.1 | 28.06 | 741.4 | 140.28 | .9475 | 6.2595 |
| 7 | 877.9 | 28.06 | 741.1 | 139.95 | .9474 | 6.2726 |
| 8 | 877.6 | 28.07 | 740.6 | 139.63 | .9474 | 6.2850 |
| 9 | 877.2 | 28.09 | 739.9 | 139.31 | .9474 | 6.2969 |
| 10 | 876.7 | 28.11 | 739.0 | 139.00 | .9475 | 6.3077 |
| 11 | 876.1 | 28.13 | 737.8 | 138.68 | .9475 | 6.3174 |
| 12 | 875.2 | 28.16 | 736.2 | 138.36 | .9477 | 6.3256 |
| 13 | 874.0 | 28.21 | 734.1 | 138.03 | .9479 | 6.3322 |
| 14 | 872.6 | 28.26 | 731.5 | 137.70 | .9481 | 6.3369 |
| 15 | 870.9 | 28.32 | 728.4 | 137.36 | .9484 | 6.3399 |
| 16 | 868.9 | 28.40 | 724.9 | 137.02 | .9488 | 6.3416 |
| 17 | 866.8 | 28.48 | 721.1 | 136.66 | .9492 | 6.3427 |
| 18 | 764.9 | 28.48 | 636.3 | 120.32 | .9491 | 6.3569 |
| 19 | 765.0 | 28.48 | 636.4 | 120.07 | .9490 | 6.3712 |
| 20 | 765.2 | 28.48 | 636.5 | 119.83 | .9489 | 6.3855 |
| 21 | 765.3 | 28.48 | 636.6 | 119.58 | .9488 | 6.3997 |
| 22 | 765.5 | 28.48 | 636.7 | 119.34 | .9488 | 6.4141 |
| 23 | 765.6 | 28.48 | 636.9 | 119.10 | .9487 | 6.4283 |
| 24 | 765.8 | 28.48 | 637.0 | 118.86 | .9486 | 6.4426 |
| 25 | 765.9 | 28.48 | 637.1 | 118.62 | .9485 | 6.4568 |
| 26 | 766.1 | 28.48 | 637.2 | 118.38 | .9484 | 6.4712 |
| 27 | 766.2 | 28.48 | 637.3 | 118.14 | .9483 | 6.4854 |
| 28 | 766.4 | 28.48 | 637.5 | 117.91 | .9482 | 6.4997 |
| 29 | 766.5 | 28.48 | 637.6 | 117.67 | .9481 | 6.5139 |
| 30 | 766.7 | 28.48 | 637.7 | 117.44 | .9480 | 6.5282 |
| 31 | 766.8 | 28.48 | 637.8 | 117.20 | .9479 | 6.5425 |
| 32 | 766.9 | 28.48 | 637.9 | 116.97 | .9478 | 6.5568 |
| 33 | 767.1 | 28.48 | 638.0 | 116.74 | .9478 | 6.5710 |
| 34 | 767.2 | 28.48 | 638.2 | 116.51 | .9477 | 6.5853 |
| 35 | 767.4 | 28.48 | 638.3 | 116.28 | .9476 | 6.5995 |
| 36 | 767.5 | 28.48 | 638.4 | 116.05 | .9475 | 6.6138 |
| 37 | 767.7 | 28.48 | 638.5 | 115.82 | .9474 | 6.6280 |
| 38 | 767.8 | 28.48 | 638.6 | 115.60 | .9473 | 6.6423 |
| 39 | 768.0 | 28.48 | 638.7 | 115.37 | .9472 | 6.6565 |
| 40 | 768.1 | 28.48 | 638.9 | 115.15 | .9471 | 6.6707 |
| 41 | 768.3 | 28.48 | 639.0 | 114.93 | .9470 | 6.6850 |
| 42 | 768.4 | 28.48 | 639.1 | 114.70 | .9469 | 6.6992 |
| 43 | 768.6 | 28.48 | 639.2 | 114.48 | .9469 | 6.7135 |

| | | | | | | |
|----|-------|-------|-------|--------|-------|--------|
| 44 | 768.7 | 28.49 | 639.3 | 114.26 | .9468 | 6.7277 |
| 45 | 768.9 | 28.49 | 639.4 | 114.04 | .9467 | 6.7419 |
| 46 | 769.0 | 28.49 | 639.5 | 113.82 | .9466 | 6.7561 |
| 47 | 769.1 | 28.49 | 639.6 | 113.60 | .9465 | 6.7702 |
| 48 | 769.2 | 28.49 | 639.7 | 113.38 | .9464 | 6.7843 |
| 49 | 769.3 | 28.49 | 639.7 | 113.16 | .9463 | 6.7980 |

CODE REPORT

TOWER # 2 Data file: column.OUT Profile file: pool.prp
Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|--------------------|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 50 | 769.2 | 28.50 | 639.4 | 112.94 | .9463 | 6.8108 |
| 51 | 768.8 | 28.52 | 638.5 | 112.71 | .9464 | 6.8211 |
| 52 | 767.5 | 28.58 | 636.1 | 112.46 | .9467 | 6.8253 |
| 53 | 764.1 | 28.74 | 629.8 | 112.12 | .9475 | 6.8152 |
| 54 | 756.3 | 29.13 | 615.1 | 111.51 | .9494 | 6.7821 |
| 55 | 743.7 | 29.88 | 589.6 | 110.28 | .9524 | 6.7434 |
| 56 | 733.8 | 30.85 | 563.4 | 108.76 | .9549 | 6.7469 |
| 57 | 733.1 | 31.56 | 550.3 | 108.13 | .9562 | 6.7792 |

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TOWER # 2 Data file: column.TSZ Profile file: pool.prp

Smith-Dresser-Ohlswager Shortcut Technique

User Provided Input Data

| | |
|----------------------------|---------|
| Tray spacing (in. or cm) | 7.0000 |
| Downcomer area (ft2 or m2) | .0236 |
| Weir length (in. or cm) | 30.0000 |
| Weir height (in. or cm) | 3.0000 |

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|-------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 1 | .3980 | .00 | .04 | 1504.0130 | 6.1901 | .4043 | .0373 |
| 2 | .3922 | .00 | .04 | 1504.1240 | 6.2043 | .4046 | .0373 |
| 3 | .3920 | .00 | .04 | 1504.3670 | 6.2184 | .4042 | .0373 |
| 4 | .3918 | .00 | .04 | 1504.7920 | 6.2324 | .4038 | .0373 |
| 5 | .3915 | .00 | .04 | 1505.4480 | 6.2462 | .4035 | .0373 |
| 6 | .3913 | .00 | .04 | 1506.4320 | 6.2596 | .4032 | .0373 |
| 7 | .3910 | .00 | .04 | 1507.8550 | 6.2727 | .4029 | .0373 |
| 8 | .3907 | .00 | .04 | 1509.8700 | 6.2851 | .4028 | .0373 |
| 9 | .3904 | .00 | .04 | 1512.6680 | 6.2970 | .4028 | .0373 |
| 10 | .3899 | .00 | .04 | 1516.4700 | 6.3078 | .4029 | .0373 |
| 11 | .3894 | .00 | .04 | 1521.5240 | 6.3175 | .4033 | .0373 |
| 12 | .3889 | .00 | .04 | 1528.0850 | 6.3257 | .4038 | .0373 |
| 13 | .3882 | .00 | .04 | 1536.3290 | 6.3323 | .4046 | .0374 |
| 14 | .3874 | .00 | .04 | 1546.3010 | 6.3370 | .4057 | .0374 |
| 15 | .3865 | .00 | .04 | 1557.7830 | 6.3400 | .4070 | .0374 |

| | | | | | | |
|----|-------|-----|---------------|--------|-------|-------|
| 16 | .3856 | .00 | .04 1570.2490 | 6.3417 | .4085 | .0374 |
| 17 | .3935 | .01 | .04 1582.9050 | 6.3428 | .3874 | .0353 |
| 18 | .3775 | .01 | .03 1582.7020 | 6.3570 | .3785 | .0353 |
| 19 | .3774 | .01 | .03 1582.5090 | 6.3713 | .3780 | .0353 |
| 20 | .3773 | .01 | .03 1582.3070 | 6.3856 | .3775 | .0353 |
| 21 | .3772 | .01 | .03 1582.1040 | 6.3998 | .3769 | .0353 |
| 22 | .3771 | .01 | .03 1581.9110 | 6.4142 | .3764 | .0353 |
| 23 | .3770 | .01 | .03 1581.7080 | 6.4284 | .3759 | .0353 |
| 24 | .3769 | .01 | .03 1581.5140 | 6.4427 | .3754 | .0353 |
| 25 | .3768 | .01 | .03 1581.3110 | 6.4569 | .3748 | .0353 |
| 26 | .3767 | .01 | .03 1581.1170 | 6.4713 | .3743 | .0353 |
| 27 | .3766 | .01 | .03 1580.9240 | 6.4855 | .3738 | .0353 |
| 28 | .3765 | .01 | .03 1580.7200 | 6.4998 | .3733 | .0353 |

CODE REPORT

Smith-Dresser-Ohlswager Shortcut Technique

| Stg | Diameter meter | Liquid Vol. flow m ³ /min | Vapor Vol. flow m ³ /sec | Liquid density kg/m ³ | Vapor density kg/m ³ | Flooding velocity m/sec | Settling height meter |
|-----|--------------------------------|--|---|--|---------------------------------------|-------------------------------|-----------------------------|
| 29 | .3764 | .01 | .03 1580.5260 | 6.5140 | .3728 | .0353 | |
| 30 | .3763 | .01 | .03 1580.3320 | 6.5283 | .3723 | .0353 | |
| 31 | .3762 | .01 | .03 1580.1380 | 6.5426 | .3718 | .0353 | |
| 32 | .3761 | .01 | .03 1579.9430 | 6.5569 | .3713 | .0353 | |
| 33 | .3760 | .01 | .03 1579.7490 | 6.5711 | .3708 | .0353 | |
| 34 | .3760 | .01 | .03 1579.5550 | 6.5854 | .3703 | .0353 | |
| 35 | .3759 | .01 | .03 1579.3600 | 6.5996 | .3697 | .0353 | |
| 36 | .3758 | .01 | .03 1579.1650 | 6.6139 | .3692 | .0353 | |
| 37 | .3757 | .01 | .03 1578.9700 | 6.6281 | .3687 | .0353 | |
| 38 | .3756 | .01 | .03 1578.7750 | 6.6423 | .3683 | .0353 | |
| 39 | .3755 | .01 | .03 1578.5810 | 6.6566 | .3678 | .0353 | |
| 40 | .3754 | .01 | .03 1578.3860 | 6.6708 | .3673 | .0353 | |
| 41 | .3753 | .01 | .03 1578.1910 | 6.6851 | .3668 | .0353 | |
| 42 | .3752 | .01 | .03 1578.0060 | 6.6993 | .3663 | .0353 | |
| 43 | .3751 | .01 | .03 1577.8130 | 6.7136 | .3658 | .0353 | |
| 44 | .3751 | .01 | .03 1577.6220 | 6.7278 | .3653 | .0353 | |
| 45 | .3750 | .01 | .03 1577.4390 | 6.7420 | .3648 | .0353 | |
| 46 | .3749 | .01 | .03 1577.2740 | 6.7562 | .3643 | .0353 | |
| 47 | .3748 | .01 | .03 1577.1440 | 6.7703 | .3639 | .0353 | |
| 48 | .3747 | .01 | .03 1577.1360 | 6.7844 | .3634 | .0353 | |
| 49 | .3746 | .01 | .03 1577.4200 | 6.7981 | .3630 | .0353 | |
| 50 | .3744 | .01 | .03 1578.5160 | 6.8109 | .3628 | .0353 | |
| 51 | .3740 | .01 | .03 1581.7190 | 6.8212 | .3630 | .0353 | |
| 52 | .3732 | .01 | .03 1590.2160 | 6.8254 | .3642 | .0353 | |
| 53 | .3714 | .01 | .03 1610.1480 | 6.8153 | .3675 | .0354 | |
| 54 | .3682 | .01 | .03 1646.2870 | 6.7822 | .3738 | .0355 | |
| 55 | .3643 | .01 | .03 1684.6500 | 6.7435 | .3798 | .0356 | |
| 56 | .3618 | .01 | .03 1703.7580 | 6.7469 | .3814 | .0356 | |
| 57 | ***Reboiler: No tray sizing*** | | | | | | |

Appendix E

Computer results of the column-
tray sizing under 1.7 times the
nominal flow rate of air

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TOPOLOGY

| Equipment | Stream Numbers |
|-----------|----------------|
| 1 TOWR | 1 2 -3 -4 |
| 2 HXER | 3 10 -5 -13 |
| 3 HXER | 4 13 -6 -15 |
| 4 HXER | 8 11 -9 -12 |
| 5 VALV | 5 -7 0 0 |
| 6 VALV | 6 -8 0 0 |
| 7 TOWR | 7 9 -10 -11 |
| 8 PUMP | 12 -14 0 0 |
| 9 HXER | 15 -16 0 0 |
| 10 HXER | 14 -17 0 0 |

Stream Connections

| Stream | Equipment | |
|--------|-----------|----|
| | From | To |
| 1 | 0 | 1 |
| 2 | 0 | 1 |
| 3 | 1 | 2 |
| 4 | 1 | 3 |
| 5 | 2 | 5 |
| 6 | 3 | 6 |
| 7 | 5 | 7 |
| 8 | 6 | 4 |
| 9 | 4 | 7 |
| 10 | 7 | 2 |
| 11 | 7 | 4 |
| 12 | 4 | 8 |
| 13 | 2 | 3 |
| 14 | 8 | 10 |
| 15 | 3 | 9 |
| 16 | 9 | 0 |
| 17 | 10 | 0 |

COMPONENTS 2
 IN numbers 46, 47,

THERMODYNAMICS

Kvalue option: Peng-Robinson
 Enthalpy option: Peng-Robinson
 Density option: API method
 CODE REPORT

MISCELLANEOUS

Recycle calculations are converged.

Recycle equipment list (KE2): 2, 3, 5, 6, 4, 7,

Streams used in conv. routine (KE4):(0)
()=Delay factor

Preferred cut stream list (KE3): 10, 11,

| Convergence tolerances, | Error |
|-------------------------|-----------|
| Flowrates: | .00100000 |
| Vapor fraction: | .00100000 |
| Temperature: | .00100000 |
| Pressure: | .00100000 |
| Enthalpy: | .00100000 |
| Flash calcs: | .00005000 |

| | |
|------------------------------|----|
| Max. loops in recycle calc.: | 30 |
| in flash calcs: | 75 |

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| *** VALVES *** | 5 | 6 |
|----------------------|--------|--------|
| Equipment no. | | |
| External name | | |
| Outlet pressure bars | 1.4006 | 1.4572 |

| ***EXCHANGER/CONDENSERS*** | 2 | 3 | 4 | 9 |
|----------------------------|---------|---------|--------|---------|
| Equipment no. | | | | |
| External name | | | | |
| Heat transfer coeff. | 300.00 | 300.00 | 300.00 | .00000 |
| Area | 9.7848 | 10.011 | .91125 | .00000 |
| Number of shells | .0 | .0 | .0 | .0 |
| Shell passes | .0 | .0 | .0 | .0 |
| Tube passes | .0 | .0 | .0 | .0 |
| Mode | 3.0 | 3.0 | 3.0 | 5.0 |
| Min. delta T or T-out | 6.00 | 3.00 | 7.00 | -175.00 |
| Delta P, stream 1 | .00000 | .00000 | .00000 | .00000 |
| Delta P, stream 2 | .00000 | .00000 | .00000 | .00000 |
| Q, stream 1 MJ/hr | -18.045 | -12.132 | 2.3613 | .25606 |
| Water usage, DM3/hr | .00000 | .00000 | .00000 | .00000 |
| Corrected delta T | 6.15 | 4.04 | 8.64 | 8.64 |
| Equipment no. | 10 | | | |
| External name | | | | |
| Heat transfer coeff. | .00000 | | | |
| Area | .00000 | | | |
| Number of shells | .0 | | | |
| Shell passes | .0 | | | |
| Tube passes | .0 | | | |
| Mode | 5.0 | | | |
| Min. delta T or T-out | -180.00 | | | |
| Delta P, stream 1 | .00000 | | | |
| Delta P, stream 2 | .00000 | | | |
| Q, stream 1 MJ/hr | 1.9207 | | | |
| Water usage, DM3/hr | .00000 | | | |
| Corrected delta T | 8.64 | | | |

```

*** PUMPS/COMPRESSORS ***
Equipment no.          8
External name
Number of stages      .0
Work capacity MJ/hr   .00000
Outlet pressure bars  190.00
Power type:          .0
  (+) steam
  (0) electricity
  (-) fuel gas
H, steam out KJ / kg  .00000
Fuel usage, M3 /hr   .00000
Water usage, DM3/hr  .00000
Steam usage Tonnes/hr .00000
Kilowatt usage       1.9769

```

205

.....

```

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```

```

*** RIGOROUS TOWERS ***
Equipment no.          1          7
External name
Number of stages      21.0       57.0
Feed 1, stage #      15.0         1.0
Feed 2, stage #      21.0       17.0
Feed 3, stage #       .0         .0
Feed 4, stage #       .0         .0
Feed 5, stage #       .0         .0
Sidestream # 1 stage  .0         .0
Sidestream # 2 stage  .0         .0
Sidestream # 3 stage  .0         .0
Sidestream # 4 stage  .0         .0
Cond. pressure bars   6.7131      1.4006
Cond. delta P bars   .00000      .00000
Colm. delta P bars   .19400E-01  .19850
Condenser type        .0         1.0
Condenser mode        4.0         .0
Value of cond. spec. 27.200      .00000
Cond comp 1 position  1.0         .0
Cond comp 2 position  .0         .0
Cond. deg. subcooled  1.00        .00
Reboiler mode         .0         4.0
Val. of reboiler spec .00000      12.920
Rebr comp 1 position  .0         2.0
Rebr comp 2 position  .0         .0
Damping ratio         .00000      1.0000
Sidestream 1 mode     .0         .0
Sidestream 2 mode     .0         .0
Sidestream 3 mode     .0         .0
Sidestream 4 mode     .0         .0
Sidestream # 1 spec   .00000      .00000
Sidestream # 2 spec   .00000      .00000
Sidestream # 3 spec   .00000      .00000
Sidestream # 4 spec   .00000      .00000
Sidestrm 1 comp posn  .0         .0
Sidestrm 2 comp posn  .0         .0
Sidestrm 3 comp posn  .0         .0

```

| | | |
|------------------------|---------|---------|
| Sidestrm 4 comp posn | .0 | .0 |
| Cond. duty MJ/hr | -277.55 | .00000 |
| Rebr duty MJ/hr | .00000 | 260.55 |
| Est dist rate Kgmol/hr | 16.000 | .00000 |
| Est. reflux Kgmol/hr | .00000 | .00000 |
| Est. side draw rate 1 | .00000 | .00000 |
| Est. side draw rate 2 | .00000 | .00000 |
| Est. side draw rate 3 | .00000 | .00000 |
| Est. side draw rate 4 | .00000 | .00000 |
| Est. temp stg 1 C | -178.00 | -193.00 |
| Est. temp stg N C | -174.00 | -183.00 |

CODE REPORT

*** Stream no. 1 ***

| | Overall | Vapor | Liquid |
|--------------------------------------|----------|-------------|-------------|
| Temperature deg C. | -172.366 | | |
| Pressure bars. . . | 6.61325 | | |
| Vapor fraction . . | .814077 | | |
| Enthalpy MJ/hr . . | 364.679 | 317.794 | 46.8845 |
| Entropy MJ/hr*K . . | -.811794 | -.456491 | -.355303 |
| Ave. mol. wt. . . | 28.7725 | 28.6655 | 29.2409 |
| Total flow kg/hr . . | 783.129 | 635.157 | 147.972 |
| Kgmol/hr . . | 27.2180 | 22.1575 | 5.06045 |
| Density kg/m3 | | 26.7085 | 1406.48 |
| Viscosity centipoise | | .690154E-02 | .103556 |
| Thermal cond. cal/cm*s*K | | .357696E-04 | .505017E-03 |
| Specific heat kJ/kg*K | | 1.25117 | 2.17498 |
| Z factor | | .847052 | |
| m3/hr (15.6 deg C & 1 atm) | | 524.913 | |
| Vol. flowrate m3/hr | | 23.7814 | |
| Surface tension dyne/cm. | | | 5.67517 |
| S. G. (60/60) | | | .915033 |
| m3/hr (15.6 deg C & 1 atm) | | | .161966 |
| Vol. flowrate m3/hr | | | .105208 |
| | Vapor | Liquid | Vapor |
| | mole | mole | flowrate |
| | fraction | fraction | kgmol/hr |
| Nitrogen | .83630 | .69196 | 18.5304 |
| Oxygen | .16370 | .30804 | 3.62715 |
| | | | Liquid |
| | | | flowrate |
| | | | kgmol/hr |
| | | | 3.50163 |
| | | | 1.55883 |

*** Stream no. 2 ***

| | Overall | Vapor | Liquid |
|--------------------------------------|----------|-------------|-------------|
| Temperature deg C. | -172.347 | | |
| Pressure bars. . . | 6.60647 | | |
| Vapor fraction . . | .832295 | | |
| Enthalpy MJ/hr . . | 550.428 | 487.063 | 63.3645 |
| Entropy MJ/hr*K . . | -1.17950 | -.698987 | -.480512 |
| Ave. mol. wt. . . | 28.7703 | 28.6730 | 29.2536 |
| Total flow kg/hr . . | 1173.83 | 973.666 | 200.164 |
| Kgmol/hr . . | 40.8000 | 33.9576 | 6.84237 |
| Density kg/m3 | | 26.6758 | 1407.54 |
| Viscosity centipoise | | .690418E-02 | .103704 |
| Thermal cond. cal/cm*s*K | | .357676E-04 | .504990E-03 |
| Specific heat kJ/kg*K | | 1.25043 | 2.17322 |
| Z factor | | .847282 | |
| m3/hr (15.6 deg C & 1 atm) | | 804.459 | |
| Vol. flowrate m3/hr | | 36.5005 | |
| Surface tension dyne/cm. | | | 5.69054 |

| | | | | | |
|----------------------------|-----------|-----------|-----------|-----------|---------|
| S. G. (60/60) | | | | | .915375 |
| m3/hr (15.6 deg C & 1 atm) | | | | | .219011 |
| Vol. flowrate m3/hr | | | | | .142210 |
| | Vapor | Liquid | Vapor | Liquid | |
| | mole | mole | flowrate | flowrate | |
| | fraction | fraction | kgmol/hr | kgmol/hr | |
| Nitrogen | .83443 | .68876 | 28.3352 | 4.71278 | |
| Oxygen | .16557 | .31124 | 5.62239 | 2.12959 | |

CODE REPORT

*** Stream no. 3 ***

| | | |
|----------------------------|-------------|-------------|
| | | All Liquid |
| Temperature deg C. | | -175.934 |
| Pressure bars. | | 6.71314 |
| Enthalpy MJ/hr | | 258.574 |
| Entropy MJ/hr*K | | -1.90819 |
| Ave. mol. wt. | | 28.0894 |
| Total flow kg/hr. | | 764.031 |
| | kgmol/hr | 27.1999 |
| Density kg/m3 | | 1329.95 |
| Viscosity centipoise | | .947303E-01 |
| Thermal cond. cal/cm*s*K | | .510520E-03 |
| Specific heat kJ/kg*K | | 2.34611 |
| Surface tension dyne/cm. | | 4.74328 |
| S. G. (60/60) | | .883915 |
| m3/hr (15.6 deg C & 1 atm) | | .865727 |
| Vol. flowrate m3/hr | | .574488 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .980825 | 26.6784 |
| Oxygen | .191745E-01 | .521546 |

*** Stream no. 4 ***

| | | |
|----------------------------|-----------|-------------|
| | | All Liquid |
| Temperature deg C. | | -172.150 |
| Pressure bars. | | 6.73254 |
| Enthalpy MJ/hr | | 378.995 |
| Entropy MJ/hr*K | | -2.85909 |
| Ave. mol. wt. | | 29.2255 |
| Total flow kg/hr. | | 1192.93 |
| | kgmol/hr | 40.8180 |
| Density kg/m3 | | 1402.51 |
| Viscosity centipoise | | .102874 |
| Thermal cond. cal/cm*s*K | | .504664E-03 |
| Specific heat kJ/kg*K | | 2.18318 |
| Surface tension dyne/cm. | | 5.60360 |
| S. G. (60/60) | | .914620 |
| m3/hr (15.6 deg C & 1 atm) | | 1.30633 |
| Vol. flowrate m3/hr | | .850576 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .695808 | 28.4015 |
| Oxygen | .304192 | 12.4165 |

CODE REPORT

*** Stream no. 5 ***

| | | |
|--------------------|-----------|------------|
| | | All Liquid |
| Temperature deg C. | | -186.645 |

| | | |
|--------------------------------------|-------------|--|
| Pressure bars. | 6.71314 | |
| Enthalpy MJ/hr | 240.529 | |
| Entropy MJ/hr*K | -2.10464 | |
| Ave. mol. wt. | 28.0894 | |
| Total flow kg/hr. | 764.031 | |
| kgmol/hr | 27.1999 | |
| Density kg/m3 | 1446.06 | |
| Viscosity centipoise | .123420 | |
| Thermal cond. cal/cm*s*K | .527854E-03 | |
| Specific heat kJ/kg*K | 2.09313 | |
| Surface tension dyne/cm. | 6.98535 | |
| S. G. (60/60) | .883915 | |
| m3/hr (15.6 deg C & 1 atm) | .865727 | |
| Vol. flowrate m3/hr | .528360 | |
| Liquid | Liquid | |
| mole | flowrate | |
| fraction | kgmol/hr | |
| Nitrogen .980825 | 26.6784 | |
| Oxygen .191745E-01 | .521546 | |

*** Stream no. 6 ***

| | All Liquid | |
|--------------------------------------|-------------|--|
| Temperature deg C. | -176.936 | |
| Pressure bars. | 6.73254 | |
| Enthalpy MJ/hr | 366.863 | |
| Entropy MJ/hr*K | -2.98213 | |
| Ave. mol. wt. | 29.2255 | |
| Total flow kg/hr. | 1192.93 | |
| kgmol/hr | 40.8180 | |
| Density kg/m3 | 1454.70 | |
| Viscosity centipoise | .113786 | |
| Thermal cond. cal/cm*s*K | .512410E-03 | |
| Specific heat kJ/kg*K | 2.06949 | |
| Surface tension dyne/cm. | 6.67757 | |
| S. G. (60/60) | .914620 | |
| m3/hr (15.6 deg C & 1 atm) | 1.30633 | |
| Vol. flowrate m3/hr | .820056 | |
| Liquid | Liquid | |
| mole | flowrate | |
| fraction | kgmol/hr | |
| Nitrogen .695808 | 28.4015 | |
| Oxygen .304192 | 12.4165 | |

CODE REPORT

*** Stream no. 7 ***

| | Overall | Vapor | Liquid |
|--------------------------------------|-------------|--------------|-------------|
| Temperature deg C. | -192.650 | | |
| Pressure bars. | 1.40055 | | |
| Vapor fraction | .668756E-01 | | |
| Enthalpy MJ/hr | 240.529 | 25.7341 | 214.895 |
| Entropy MJ/hr*K | -2.09356 | -.237600E-01 | -2.06980 |
| Ave. mol. wt. | 28.0894 | 28.0401 | 28.0930 |
| Total flow kg/hr | 764.031 | 51.0205 | 713.011 |
| kgmol/hr | 27.1999 | 1.81956 | 25.3804 |
| Density kg/m3 | | 6.12840 | 1503.90 |
| Viscosity centipoise | | .541963E-02 | .147499 |
| Thermal cond. cal/cm*s*K | | .340865E-04 | .537577E-03 |
| Specific heat kJ/kg*K | | 1.13159 | 1.97731 |
| Z factor | | .947871 | |
| m3/hr (15.6 deg C & 1 atm) | | 43.5406 | |

| | | | | |
|--------------------------------------|------------|------------|-------------|----------|
| Vol. flowrate m3/hr | | | 8.32537 | |
| Surface tension dyne/cm. | | | | 8.31641 |
| S. G. (60/60) | | | | .881012 |
| m3/hr (15.6 deg C & 1 atm) | | | | .807828 |
| Vol. flowrate m3/hr | | | | .474114 |
| | Vapor | Liquid | Vapor | Liquid |
| | mole | mole | flowrate | flowrate |
| | fraction | fraction | kgmol/hr | kgmol/hr |
| Nitrogen | .99321 | .97993 | 1.80720 | 24.8710 |
| Oxygen | .67883E-02 | .20072E-01 | .123517E-01 | .509438 |

*** Stream no. 8 ***

| | Overall | | Vapor | | Liquid |
|--------------------------------------|----------|----------|--------------|---|-------------|
| Temperature deg C. | -190.026 | | | | |
| Pressure bars. | 1.45725 | | | | |
| Vapor fraction | .138561 | | | | |
| Enthalpy MJ/hr | 366.863 | : | 79.3547 | : | 287.431 |
| Entropy MJ/hr*K | -2.94376 | : | -.696667E-01 | : | -2.87410 |
| Ave. mol. wt. | 29.2255 | : | 28.5270 | : | 29.3375 |
| Total flow kg/hr | 1192.93 | : | 161.342 | : | 1031.57 |
| kgmol/hr | 40.8180 | : | 5.65578 | : | 35.1622 |
| Density kg/m3 | | | 6.35054 | | 1590.34 |
| Viscosity centipoise | | | .566984E-02 | | .161652 |
| Thermal cond. cal/cm*s*K | | | .339152E-04 | | .533617E-03 |
| Specific heat kJ/kg*K | | | 1.10402 | | 1.84609 |
| Z factor | | | .949508 | | |
| m3/hr (15.6 deg C & 1 atm) | | | 133.656 | | |
| Vol. flowrate m3/hr | | | 25.4064 | | |
| Surface tension dyne/cm. | | | | | 9.92959 |
| S. G. (60/60) | | | | | .917630 |
| m3/hr (15.6 deg C & 1 atm) | | | | | 1.12593 |
| Vol. flowrate m3/hr | | | | | .648657 |
| | Vapor | Liquid | Vapor | | Liquid |
| | mole | mole | flowrate | | flowrate |
| | fraction | fraction | kgmol/hr | | kgmol/hr |
| Nitrogen | .87106 | .66770 | 4.92650 | | 23.4778 |
| Oxygen | .12894 | .33230 | .729281 | | 11.6844 |

CODE REPORT

*** Stream no. 9 ***

| | Overall | | Vapor | | Liquid |
|--------------------------------------|----------|---|--------------|---|-------------|
| Temperature deg C. | -190.007 | | | | |
| Pressure bars. | 1.45725 | | | | |
| Vapor fraction | .149001 | | | | |
| Enthalpy MJ/hr | 369.224 | : | 85.4078 | : | 283.830 |
| Entropy MJ/hr*K | -2.91394 | : | -.748865E-01 | : | -2.83905 |
| Ave. mol. wt. | 29.2255 | : | 28.5313 | : | 29.3468 |
| Total flow kg/hr | 1192.93 | : | 173.525 | : | 1019.39 |
| kgmol/hr | 40.8180 | : | 6.08192 | : | 34.7361 |
| Density kg/m3 | | | 6.34457 | | 1590.97 |
| Viscosity centipoise | | | .567178E-02 | | .161735 |
| Thermal cond. cal/cm*s*K | | | .339275E-04 | | .533589E-03 |
| Specific heat kJ/kg*K | | | 1.10395 | | 1.84485 |
| Z factor | | | .949533 | | |
| m3/hr (15.6 deg C & 1 atm) | | | 143.847 | | |
| Vol. flowrate m3/hr | | | 27.3505 | | |
| Surface tension dyne/cm. | | | | | 9.94191 |
| S. G. (60/60) | | | | | .917879 |
| m3/hr (15.6 deg C & 1 atm) | | | | | 1.11234 |
| Vol. flowrate m3/hr | | | | | .640746 |

| | Vapor mole fraction | Liquid mole fraction | Vapor flowrate kgmol/hr | Liquid flowrate kgmol/hr |
|----------|---------------------------|----------------------------|-------------------------------|--------------------------------|
| Nitrogen | .86998 | .66537 | 5.29115 | 23.1124 |
| Oxygen | .13002 | .33463 | .790769 | 11.6237 |

*** Stream no. 10 ***

| | | All Vapor |
|----------------------------|-------------|-------------|
| Temperature deg C. | | -192.645 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 771.479 |
| Entropy MJ/hr*K | | -.717509 |
| Ave. mol. wt. | | 28.0411 |
| Total flow kg/hr. | | 1545.01 |
| | kgmol/hr | 55.0980 |
| Density kg/m3 | | 6.19003 |
| Viscosity centipoise | | .542011E-02 |
| Thermal cond. cal/cm*s*K | | .339356E-04 |
| Specific heat kJ/kg*K | | 1.13147 |
| Z factor | | .947878 |
| m3/hr (15.6 deg C & 1 atm) | | 1305.28 |
| Vol. flowrate m3/hr | | 249.600 |
| | | Vapor |
| | | mole |
| | | fraction |
| | | flowrate |
| | | kgmol/hr |
| Nitrogen | .992954 | 54.7098 |
| Oxygen | .704628E-02 | .388236 |

CODE REPORT

*** Stream no. 11 ***

| | | All Liquid |
|----------------------------|-------------|-------------|
| Temperature deg C. | | -179.494 |
| Pressure bars. | | 1.59905 |
| Enthalpy MJ/hr | | 98.8147 |
| Entropy MJ/hr*K | | -1.02800 |
| Ave. mol. wt. | | 31.8848 |
| Total flow kg/hr. | | 411.950 |
| | kgmol/hr | 12.9199 |
| Density kg/m3 | | 1708.86 |
| Viscosity centipoise | | .175450 |
| Thermal cond. cal/cm*s*K | | .517176E-03 |
| Specific heat kJ/kg*K | | 1.63153 |
| Surface tension dyne/cm. | | 12.0763 |
| S. G. (60/60) | | .985195 |
| m3/hr (15.6 deg C & 1 atm) | | .418796 |
| Vol. flowrate m3/hr | | .241069 |
| | | Liquid |
| | | mole |
| | | fraction |
| | | flowrate |
| | | kgmol/hr |
| Nitrogen | .286495E-01 | .370150 |
| Oxygen | .971351 | 12.5498 |

*** Stream no. 12 ***

| | | All Liquid |
|--------------------|--|------------|
| Temperature deg C. | | -183.026 |
| Pressure bars. | | 1.59905 |
| Enthalpy MJ/hr | | 96.4537 |
| Entropy MJ/hr*K | | -1.05378 |
| Ave. mol. wt. | | 31.8848 |
| Total flow kg/hr. | | 411.951 |

| | | |
|----------------------------|----------------------|-------------|
| | kgmol/hr | 12.9200 |
| Density | kg/m3 | 1737.06 |
| Viscosity | centipoise | .190574 |
| Thermal cond. | cal/cm*s*K | .522892E-03 |
| Specific heat | kJ/kg*K | 1.61370 |
| Surface tension | dyne/cm. | 12.9483 |
| S. G. (60/60) | | .985194 |
| m3/hr (15.6 deg C & 1 atm) | | .418798 |
| Vol. flowrate | m3/hr | .237156 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .286528E-01 | .370194 |
| Oxygen | .971347 | 12.5498 |

CODE REPORT

*** Stream no. 13 ***

| | | |
|----------------------------|----------------------|-------------|
| | | All Vapor |
| Temperature | deg C. | -182.231 |
| Pressure | bars. | 1.40055 |
| Enthalpy | MJ/hr | 789.524 |
| Entropy | MJ/hr*K | -.506673 |
| Ave. mol. wt. | | 28.0411 |
| Total flow | kg/hr. | 1545.01 |
| | kgmol/hr | 55.0980 |
| Density | kg/m3 | 5.40057 |
| Viscosity | centipoise | .612507E-02 |
| Thermal cond. | cal/cm*s*K | .350412E-04 |
| Specific heat | kJ/kg*K | 1.11367 |
| Z factor | | .961977 |
| m3/hr (15.6 deg C & 1 atm) | | 1305.28 |
| Vol. flowrate | m3/hr | 286.086 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .992954 | 54.7098 |
| Oxygen | .704622E-02 | .388233 |

*** Stream no. 14 ***

| | | |
|----------------------------|----------------------|-------------|
| | | All Liquid |
| Temperature | deg C. | -183.026 |
| Pressure | bars. | 190.000 |
| Enthalpy | MJ/hr | 100.402 |
| Entropy | MJ/hr*K | -1.07603 |
| Ave. mol. wt. | | 31.8848 |
| Total flow | kg/hr. | 411.951 |
| | kgmol/hr | 12.9200 |
| Density | kg/m3 | 1851.52 |
| Viscosity | centipoise | .190574 |
| Thermal cond. | cal/cm*s*K | .522892E-03 |
| Specific heat | kJ/kg*K | 1.53708 |
| Surface tension | dyne/cm. | 12.9240 |
| S. G. (60/60) | | .985194 |
| m3/hr (15.6 deg C & 1 atm) | | .418798 |
| Vol. flowrate | m3/hr | .222496 |
| | Liquid | Liquid |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .286528E-01 | .370194 |
| Oxygen | .971347 | 12.5498 |

*** Stream no. 15 ***

| | | |
|--------------------------------------|-------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -175.150 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 801.656 |
| Entropy MJ/hr*K | | -.378173 |
| Ave. mol. wt. | | 28.0411 |
| Total flow kg/hr. | | 1545.01 |
| kgmol/hr | | 55.0980 |
| Density kg/m3 | | 4.97529 |
| Viscosity centipoise | | .660203E-02 |
| Thermal cond. cal/cm*s*K | | .358103E-04 |
| Specific heat kJ/kg*K | | 1.10436 |
| Z factor | | .968776 |
| m3/hr (15.6 deg C & 1 atm) | | 1305.28 |
| Vol. flowrate m3/hr | | 310.541 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .992954 | 54.7098 |
| Oxygen | .704622E-02 | .388233 |

*** Stream no. 16 ***

| | | |
|--------------------------------------|-------------|-------------|
| | | All Vapor |
| Temperature deg C. | | -175.000 |
| Pressure bars. | | 1.40055 |
| Enthalpy MJ/hr | | 801.912 |
| Entropy MJ/hr*K | | -.375563 |
| Ave. mol. wt. | | 28.0411 |
| Total flow kg/hr. | | 1545.01 |
| kgmol/hr | | 55.0980 |
| Density kg/m3 | | 4.96705 |
| Viscosity centipoise | | .661210E-02 |
| Thermal cond. cal/cm*s*K | | .358268E-04 |
| Specific heat kJ/kg*K | | 1.10436 |
| Z factor | | .968902 |
| m3/hr (15.6 deg C & 1 atm) | | 1305.28 |
| Vol. flowrate m3/hr | | 311.056 |
| | Vapor | Vapor |
| | mole | flowrate |
| | fraction | kgmol/hr |
| Nitrogen | .992954 | 54.7098 |
| Oxygen | .704622E-02 | .388233 |

CODE REPORT

*** Stream no. 17 ***

| | | |
|------------------------------------|--|-------------|
| | | All Liquid |
| Temperature deg C. | | -180.000 |
| Pressure bars. | | 190.000 |
| Enthalpy MJ/hr | | 102.323 |
| Entropy MJ/hr*K | | -1.05506 |
| Ave. mol. wt. | | 31.8848 |
| Total flow kg/hr. | | 411.951 |
| kgmol/hr | | 12.9200 |
| Density kg/m3 | | 1832.37 |
| Viscosity centipoise | | .177473 |
| Thermal cond. cal/cm*s*K | | .517995E-03 |
| Specific heat kJ/kg*K | | 1.54391 |

| | | | | | | | |
|----|-------|-------|-----|-----|---------|-------|------|
| 1 | 514.0 | 28.09 | .58 | .39 | 1329.83 | .0947 | 4.74 |
| 2 | 519.4 | 28.17 | .59 | .39 | 1324.15 | .0934 | 4.62 |
| 3 | 517.4 | 28.25 | .58 | .39 | 1330.76 | .0941 | 4.69 |
| 4 | 515.4 | 28.34 | .58 | .39 | 1337.70 | .0949 | 4.78 |
| 5 | 513.3 | 28.44 | .58 | .38 | 1344.85 | .0957 | 4.87 |
| 6 | 511.2 | 28.53 | .57 | .38 | 1352.06 | .0966 | 4.95 |
| 7 | 509.1 | 28.63 | .57 | .37 | 1359.18 | .0974 | 5.04 |
| 8 | 506.7 | 28.72 | .56 | .37 | 1366.03 | .0983 | 5.13 |
| 9 | 505.6 | 28.80 | .56 | .37 | 1372.47 | .0991 | 5.21 |
| 10 | 503.8 | 28.89 | .56 | .37 | 1378.42 | .0998 | 5.29 |
| 11 | 502.3 | 28.96 | .55 | .36 | 1383.77 | .1005 | 5.36 |
| 12 | 501.0 | 29.03 | .55 | .36 | 1388.50 | .1011 | 5.42 |
| 13 | 500.1 | 29.08 | .55 | .36 | 1392.60 | .1016 | 5.47 |
| 14 | 499.1 | 29.13 | .55 | .36 | 1396.11 | .1020 | 5.52 |
| 15 | 584.2 | 29.17 | .64 | .42 | 1399.05 | .1024 | 5.56 |
| 16 | 584.0 | 29.18 | .64 | .42 | 1399.15 | .1024 | 5.56 |
| 17 | 584.1 | 29.18 | .64 | .42 | 1399.33 | .1025 | 5.56 |
| 18 | 584.0 | 29.18 | .64 | .42 | 1399.65 | .1025 | 5.57 |
| 19 | 583.7 | 29.19 | .64 | .42 | 1400.20 | .1026 | 5.57 |
| 20 | 583.5 | 29.20 | .64 | .42 | 1401.05 | .1027 | 5.58 |
| 21 | 701.4 | 29.22 | .77 | .50 | 1402.45 | .1029 | 5.60 |

Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|---|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 1 | *** Total Condenser : No Vapor Outlet *** | | | | | |
| 2 | 963.4 | 28.09 | 812.5 | 34.93 | .8356 | 27.5835 |
| 3 | 968.8 | 28.13 | 815.9 | 35.17 | .8364 | 27.5503 |
| 4 | 966.8 | 28.18 | 812.9 | 35.14 | .8372 | 27.5146 |
| 5 | 964.8 | 28.22 | 809.8 | 35.11 | .8380 | 27.4772 |
| 6 | 962.7 | 28.27 | 806.7 | 35.08 | .8388 | 27.4394 |
| 7 | 960.6 | 28.32 | 803.5 | 35.06 | .8397 | 27.4016 |
| 8 | 958.5 | 28.37 | 800.4 | 35.03 | .8405 | 27.3653 |
| 9 | 956.1 | 28.42 | 797.0 | 34.98 | .8413 | 27.3308 |
| 10 | 955.0 | 28.46 | 794.8 | 34.98 | .8420 | 27.2991 |
| 11 | 953.3 | 28.50 | 792.3 | 34.96 | .8426 | 27.2702 |
| 12 | 951.7 | 28.54 | 790.0 | 34.93 | .8432 | 27.2451 |
| 13 | 950.4 | 28.57 | 788.0 | 34.91 | .8437 | 27.2240 |
| 14 | 949.5 | 28.60 | 786.4 | 34.90 | .8442 | 27.2059 |
| 15 | 948.5 | 28.63 | 784.9 | 34.88 | .8446 | 27.1917 |
| 16 | 573.2 | 28.63 | 474.3 | 21.08 | .8446 | 27.1946 |
| 17 | 573.1 | 28.63 | 474.2 | 21.07 | .8446 | 27.1973 |
| 18 | 573.2 | 28.63 | 474.2 | 21.07 | .8446 | 27.1993 |
| 19 | 573.1 | 28.64 | 474.1 | 21.07 | .8446 | 27.2003 |
| 20 | 572.8 | 28.65 | 473.7 | 21.06 | .8448 | 27.1986 |
| 21 | 572.6 | 28.66 | 473.3 | 21.06 | .8449 | 27.1935 |

CODE: Chemical Engineering Simulation System
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TOWER # 1 Data file: col17.TSZ Profile file: link.prp

Smith-Dresser-Ohlswager Shortcut Technique

User Provided Input Data

Tray spacing (in. or cm) 7.0000
 Downcomer area (ft2 or m2) .0151
 Weir length (in. or cm) 24.0000
 Weir height (in. or cm) 3.0000

215

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|---------------------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 1 | ***Condenser: No tray sizing*** | | | | | | |
| 2 | .3051 | .01 | .01 | 1324.1490 | 27.5839 | .1672 | .0361 |
| 3 | .3053 | .01 | .01 | 1330.7550 | 27.5507 | .1681 | .0361 |
| 4 | .3047 | .01 | .01 | 1337.6980 | 27.5150 | .1687 | .0361 |
| 5 | .3040 | .01 | .01 | 1344.8480 | 27.4776 | .1696 | .0361 |
| 6 | .3034 | .01 | .01 | 1352.0650 | 27.4397 | .1704 | .0362 |
| 7 | .3028 | .01 | .01 | 1359.1760 | 27.4020 | .1711 | .0362 |
| 8 | .3022 | .01 | .01 | 1366.0340 | 27.3657 | .1718 | .0362 |
| 9 | .3016 | .01 | .01 | 1372.4660 | 27.3312 | .1724 | .0362 |
| 10 | .3012 | .01 | .01 | 1378.4210 | 27.2995 | .1731 | .0362 |
| 11 | .3007 | .01 | .01 | 1383.7730 | 27.2706 | .1736 | .0363 |
| 12 | .3003 | .01 | .01 | 1388.5020 | 27.2455 | .1741 | .0363 |
| 13 | .3000 | .01 | .01 | 1392.6050 | 27.2244 | .1745 | .0363 |
| 14 | .2997 | .01 | .01 | 1396.1050 | 27.2063 | .1749 | .0363 |
| 15 | .3029 | .01 | .01 | 1399.0530 | 27.1921 | .1701 | .0359 |
| 16 | .2615 | .01 | .01 | 1399.1530 | 27.1950 | .1517 | .0359 |
| 17 | .2615 | .01 | .01 | 1399.3330 | 27.1977 | .1517 | .0359 |
| 18 | .2615 | .01 | .01 | 1399.6530 | 27.1997 | .1517 | .0359 |
| 19 | .2614 | .01 | .01 | 1400.1980 | 27.2007 | .1517 | .0359 |
| 20 | .2613 | .01 | .01 | 1401.0550 | 27.1990 | .1518 | .0359 |
| 21 | .2661 | .01 | .01 | 1402.4480 | 27.1939 | .1444 | .0354 |

CODE REPORT

TOWER # 2

Data file: col17.OUT

Profile file: pool.prf

Column Summary

| Stg | Temp C | Pres bars | Net Flow Rates kgmols/hr | | | Duties MJ/hr |
|-----|-----------|--------------|-----------------------------|--------|-----------------|-----------------|
| | | | Liquid | Vapor | Feed Product | |
| 1 | -192.6 | 1.401 | 14.924 | | 27.200 55.098 | |
| 2 | -192.6 | 1.404 | 14.920 | 31.324 | | |
| 3 | -192.6 | 1.408 | 14.915 | 31.320 | | |
| 4 | -192.5 | 1.411 | 14.907 | 31.315 | | |
| 5 | -192.5 | 1.415 | 14.896 | 31.307 | | |
| 6 | -192.5 | 1.418 | 14.881 | 31.296 | | |
| 7 | -192.4 | 1.422 | 14.861 | 31.281 | | |
| 8 | -192.3 | 1.425 | 14.832 | 31.261 | | |
| 9 | -192.2 | 1.429 | 14.794 | 31.232 | | |
| 10 | -192.1 | 1.432 | 14.742 | 31.194 | | |
| 11 | -192.0 | 1.436 | 14.674 | 31.142 | | |
| 12 | -191.8 | 1.440 | 14.587 | 31.074 | | |
| 13 | -191.6 | 1.443 | 14.478 | 30.987 | | |
| 14 | -191.3 | 1.447 | 14.348 | 30.878 | | |
| 15 | -191.0 | 1.450 | 14.199 | 30.748 | | |
| 16 | -190.6 | 1.454 | 14.037 | 30.598 | | |
| 17 | -190.2 | 1.457 | 34.458 | 30.437 | 40.818 | |
| 18 | -190.2 | 1.461 | 34.463 | 26.858 | | |
| 19 | -190.2 | 1.464 | 34.468 | 26.863 | | |

| | | | | |
|----|--------|-------|--------|--------|
| 20 | -190.2 | 1.468 | 34.473 | 26.868 |
| 21 | -190.2 | 1.471 | 34.478 | 26.873 |
| 22 | -190.1 | 1.475 | 34.483 | 26.878 |
| 23 | -190.1 | 1.479 | 34.488 | 26.883 |
| 24 | -190.1 | 1.482 | 34.493 | 26.888 |
| 25 | -190.1 | 1.486 | 34.498 | 26.893 |
| 26 | -190.0 | 1.489 | 34.503 | 26.898 |
| 27 | -190.0 | 1.493 | 34.508 | 26.903 |
| 28 | -190.0 | 1.496 | 34.513 | 26.908 |
| 29 | -190.0 | 1.500 | 34.518 | 26.913 |
| 30 | -189.9 | 1.503 | 34.523 | 26.918 |
| 31 | -189.9 | 1.507 | 34.528 | 26.923 |
| 32 | -189.9 | 1.510 | 34.533 | 26.928 |
| 33 | -189.9 | 1.514 | 34.538 | 26.933 |
| 34 | -189.8 | 1.518 | 34.542 | 26.938 |
| 35 | -189.8 | 1.521 | 34.547 | 26.943 |
| 36 | -189.8 | 1.525 | 34.552 | 26.947 |
| 37 | -189.8 | 1.528 | 34.557 | 26.952 |
| 38 | -189.8 | 1.532 | 34.562 | 26.957 |
| 39 | -189.7 | 1.535 | 34.567 | 26.962 |
| 40 | -189.7 | 1.539 | 34.572 | 26.967 |
| 41 | -189.7 | 1.542 | 34.577 | 26.972 |
| 42 | -189.7 | 1.546 | 34.582 | 26.977 |
| 43 | -189.6 | 1.549 | 34.587 | 26.982 |
| 44 | -189.6 | 1.553 | 34.591 | 26.987 |
| 45 | -189.6 | 1.557 | 34.595 | 26.991 |
| 46 | -189.6 | 1.560 | 34.600 | 26.995 |
| 47 | -189.5 | 1.564 | 34.602 | 27.000 |

CODE REPORT

| | | Liquid | Vapor | Feed | Product |
|----|--------|--------|--------|--------|---------------|
| 48 | -189.5 | 1.567 | 34.601 | 27.002 | |
| 49 | -189.5 | 1.571 | 34.590 | 27.001 | |
| 50 | -189.4 | 1.574 | 34.554 | 26.990 | |
| 51 | -189.3 | 1.578 | 34.451 | 26.954 | |
| 52 | -189.0 | 1.581 | 34.183 | 26.851 | |
| 53 | -188.3 | 1.585 | 33.566 | 26.583 | |
| 54 | -186.7 | 1.588 | 32.488 | 25.966 | |
| 55 | -184.1 | 1.592 | 31.381 | 24.888 | |
| 56 | -181.3 | 1.596 | 30.829 | 23.781 | |
| 57 | -179.5 | 1.599 | 23.229 | | 7.6000 260.55 |

Stream # 7 fed to Stg 1 is 6.690 % Vapor
 Stream # 9 fed to Stg 17 is 14.900 % Vapor

Stream # 10 is Vapor Distillate from Stg 1
 Stream # 11 is Liquid Bottoms from Stg 57

Condenser duty is .000000 MJ/hr
 Reboiler duty is 260.549 MJ/hr
 CODE REPORT

TOWER # 2 Data file: coll7.OUT Profile file: pool.prf
 Tray Liquid Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise | Surface tension dyne/cm |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|

| | | | | | | | |
|----|--------|-------|------|-----|---------|-------|------|
| 1 | 419.3 | 28.09 | .48 | .28 | 1504.01 | .1477 | 8.32 |
| 2 | 419.2 | 28.10 | .47 | .28 | 1504.12 | .1477 | 8.32 |
| 3 | 419.2 | 28.11 | .47 | .28 | 1504.37 | .1476 | 8.32 |
| 4 | 419.1 | 28.11 | .47 | .28 | 1504.79 | .1476 | 8.33 |
| 5 | 419.0 | 28.12 | .47 | .28 | 1505.45 | .1477 | 8.34 |
| 6 | 418.8 | 28.14 | .47 | .28 | 1506.43 | .1477 | 8.36 |
| 7 | 418.5 | 28.16 | .47 | .28 | 1507.85 | .1479 | 8.38 |
| 8 | 418.1 | 28.19 | .47 | .28 | 1509.87 | .1482 | 8.42 |
| 9 | 417.6 | 28.23 | .47 | .28 | 1512.67 | .1485 | 8.47 |
| 10 | 417.0 | 28.28 | .47 | .27 | 1516.47 | .1491 | 8.53 |
| 11 | 416.1 | 28.35 | .47 | .27 | 1521.52 | .1499 | 8.63 |
| 12 | 414.9 | 28.45 | .47 | .27 | 1528.09 | .1509 | 8.75 |
| 13 | 413.5 | 28.56 | .46 | .27 | 1536.33 | .1522 | 8.90 |
| 14 | 411.8 | 28.70 | .46 | .27 | 1546.30 | .1539 | 9.08 |
| 15 | 409.8 | 28.86 | .45 | .26 | 1557.78 | .1558 | 9.30 |
| 16 | 407.7 | 29.04 | .45 | .26 | 1570.25 | .1580 | 9.54 |
| 17 | 1007.2 | 29.23 | 1.10 | .64 | 1582.90 | .1602 | 9.78 |
| 18 | 1007.3 | 29.23 | 1.10 | .64 | 1582.70 | .1601 | 9.78 |
| 19 | 1007.5 | 29.23 | 1.10 | .64 | 1582.51 | .1600 | 9.77 |
| 20 | 1007.6 | 29.23 | 1.10 | .64 | 1582.31 | .1598 | 9.77 |
| 21 | 1007.8 | 29.23 | 1.10 | .64 | 1582.10 | .1597 | 9.76 |
| 22 | 1007.9 | 29.23 | 1.10 | .64 | 1581.91 | .1596 | 9.76 |
| 23 | 1008.1 | 29.23 | 1.10 | .64 | 1581.71 | .1595 | 9.75 |
| 24 | 1008.2 | 29.23 | 1.10 | .64 | 1581.51 | .1594 | 9.75 |
| 25 | 1008.4 | 29.23 | 1.10 | .64 | 1581.31 | .1593 | 9.74 |
| 26 | 1008.5 | 29.23 | 1.10 | .64 | 1581.12 | .1592 | 9.74 |
| 27 | 1008.6 | 29.23 | 1.10 | .64 | 1580.92 | .1591 | 9.73 |
| 28 | 1008.8 | 29.23 | 1.10 | .64 | 1580.72 | .1590 | 9.72 |
| 29 | 1008.9 | 29.23 | 1.10 | .64 | 1580.53 | .1589 | 9.72 |
| 30 | 1009.1 | 29.23 | 1.10 | .64 | 1580.33 | .1588 | 9.71 |
| 31 | 1009.2 | 29.23 | 1.11 | .64 | 1580.14 | .1587 | 9.71 |
| 32 | 1009.4 | 29.23 | 1.11 | .64 | 1579.94 | .1586 | 9.70 |
| 33 | 1009.5 | 29.23 | 1.11 | .64 | 1579.75 | .1584 | 9.70 |
| 34 | 1009.7 | 29.23 | 1.11 | .64 | 1579.55 | .1583 | 9.69 |
| 35 | 1009.8 | 29.23 | 1.11 | .64 | 1579.36 | .1582 | 9.69 |
| 36 | 1010.0 | 29.23 | 1.11 | .64 | 1579.16 | .1581 | 9.68 |
| 37 | 1010.1 | 29.23 | 1.11 | .64 | 1578.97 | .1580 | 9.68 |
| 38 | 1010.3 | 29.23 | 1.11 | .64 | 1578.78 | .1579 | 9.67 |
| 39 | 1010.4 | 29.23 | 1.11 | .64 | 1578.58 | .1578 | 9.67 |
| 40 | 1010.6 | 29.23 | 1.11 | .64 | 1578.39 | .1577 | 9.66 |
| 41 | 1010.7 | 29.23 | 1.11 | .64 | 1578.19 | .1576 | 9.66 |
| 42 | 1010.9 | 29.23 | 1.11 | .64 | 1578.01 | .1575 | 9.65 |
| 43 | 1011.0 | 29.23 | 1.11 | .64 | 1577.81 | .1574 | 9.65 |
| 44 | 1011.1 | 29.23 | 1.11 | .64 | 1577.62 | .1573 | 9.64 |
| 45 | 1011.3 | 29.23 | 1.11 | .64 | 1577.44 | .1572 | 9.63 |
| 46 | 1011.4 | 29.23 | 1.11 | .64 | 1577.27 | .1571 | 9.63 |
| 47 | 1011.5 | 29.23 | 1.11 | .64 | 1577.14 | .1570 | 9.63 |
| 48 | 1011.6 | 29.24 | 1.11 | .64 | 1577.14 | .1569 | 9.62 |
| 49 | 1011.5 | 29.24 | 1.11 | .64 | 1577.42 | .1569 | 9.63 |

CODE REPORT

TOWER # 2 Data file: col17.OUT
Tray Liquid Properties

Profile file: pool.prf

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Actual Density kg/m3 | Viscosity centipoise | Surface tension dyne/cm |
|-----|--------------------|---------------|--------------------------------|------------------------------|----------------------------|-------------------------|-------------------------------|
| 50 | 1011.1 | 29.26 | 1.11 | .64 | 1578.52 | .1571 | 9.65 |

| | | | | | | | |
|----|--------|-------|------|-----|---------|-------|-------|
| 51 | 1009.8 | 29.31 | 1.10 | .64 | 1581.72 | .1576 | 9.71 |
| 52 | 1006.4 | 29.44 | 1.10 | .63 | 1590.22 | .1591 | 9.87 |
| 53 | 998.6 | 29.75 | 1.08 | .62 | 1610.15 | .1627 | 10.26 |
| 54 | 986.0 | 30.35 | 1.05 | .60 | 1646.29 | .1692 | 10.98 |
| 55 | 976.1 | 31.10 | 1.01 | .58 | 1684.65 | .1753 | 11.72 |
| 56 | 975.4 | 31.64 | 1.00 | .57 | 1703.76 | .1764 | 12.04 |
| 57 | 242.3 | 31.88 | .25 | .14 | 1708.77 | .1755 | 12.08 |

CODE REPORT

TOWER # 2 Data file: col17.DUT Profile file: pool.prf
 Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|--------------------|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 1 | 908.5 | 28.04 | 767.6 | 146.77 | .9479 | 6.1900 |
| 2 | 878.4 | 28.04 | 742.1 | 141.58 | .9478 | 6.2042 |
| 3 | 878.3 | 28.04 | 742.0 | 141.25 | .9477 | 6.2183 |
| 4 | 878.3 | 28.05 | 741.8 | 140.92 | .9476 | 6.2323 |
| 5 | 878.2 | 28.05 | 741.7 | 140.60 | .9476 | 6.2461 |
| 6 | 878.1 | 28.06 | 741.4 | 140.28 | .9475 | 6.2595 |
| 7 | 877.9 | 28.06 | 741.1 | 139.95 | .9474 | 6.2726 |
| 8 | 877.6 | 28.07 | 740.6 | 139.63 | .9474 | 6.2850 |
| 9 | 877.2 | 28.09 | 739.9 | 139.31 | .9474 | 6.2969 |
| 10 | 876.7 | 28.11 | 739.0 | 139.00 | .9475 | 6.3077 |
| 11 | 876.1 | 28.13 | 737.8 | 138.68 | .9475 | 6.3174 |
| 12 | 875.2 | 28.16 | 736.2 | 138.36 | .9477 | 6.3256 |
| 13 | 874.0 | 28.21 | 734.1 | 138.03 | .9479 | 6.3322 |
| 14 | 872.6 | 28.26 | 731.5 | 137.70 | .9481 | 6.3369 |
| 15 | 870.9 | 28.32 | 728.4 | 137.36 | .9484 | 6.3399 |
| 16 | 868.9 | 28.40 | 724.9 | 137.02 | .9488 | 6.3416 |
| 17 | 866.8 | 28.48 | 721.1 | 136.66 | .9492 | 6.3427 |
| 18 | 764.9 | 28.48 | 636.3 | 120.32 | .9491 | 6.3569 |
| 19 | 765.0 | 28.48 | 636.4 | 120.07 | .9490 | 6.3712 |
| 20 | 765.2 | 28.48 | 636.5 | 119.83 | .9489 | 6.3855 |
| 21 | 765.3 | 28.48 | 636.6 | 119.58 | .9488 | 6.3997 |
| 22 | 765.5 | 28.48 | 636.7 | 119.34 | .9488 | 6.4141 |
| 23 | 765.6 | 28.48 | 636.9 | 119.10 | .9487 | 6.4283 |
| 24 | 765.8 | 28.48 | 637.0 | 118.86 | .9486 | 6.4426 |
| 25 | 765.9 | 28.48 | 637.1 | 118.62 | .9485 | 6.4568 |
| 26 | 766.1 | 28.48 | 637.2 | 118.38 | .9484 | 6.4712 |
| 27 | 766.2 | 28.48 | 637.3 | 118.14 | .9483 | 6.4854 |
| 28 | 766.4 | 28.48 | 637.5 | 117.91 | .9482 | 6.4997 |
| 29 | 766.5 | 28.48 | 637.6 | 117.67 | .9481 | 6.5139 |
| 30 | 766.7 | 28.48 | 637.7 | 117.44 | .9480 | 6.5282 |
| 31 | 766.8 | 28.48 | 637.8 | 117.20 | .9479 | 6.5425 |
| 32 | 766.9 | 28.48 | 637.9 | 116.97 | .9478 | 6.5568 |
| 33 | 767.1 | 28.48 | 638.0 | 116.74 | .9478 | 6.5710 |
| 34 | 767.2 | 28.48 | 638.2 | 116.51 | .9477 | 6.5853 |
| 35 | 767.4 | 28.48 | 638.3 | 116.28 | .9476 | 6.5995 |
| 36 | 767.5 | 28.48 | 638.4 | 116.05 | .9475 | 6.6138 |
| 37 | 767.7 | 28.48 | 638.5 | 115.82 | .9474 | 6.6280 |
| 38 | 767.8 | 28.48 | 638.6 | 115.60 | .9473 | 6.6423 |
| 39 | 768.0 | 28.48 | 638.7 | 115.37 | .9472 | 6.6565 |
| 40 | 768.1 | 28.48 | 638.9 | 115.15 | .9471 | 6.6707 |
| 41 | 768.3 | 28.48 | 639.0 | 114.93 | .9470 | 6.6850 |
| 42 | 768.4 | 28.48 | 639.1 | 114.70 | .9469 | 6.6992 |
| 43 | 768.6 | 28.48 | 639.2 | 114.48 | .9469 | 6.7135 |

| | | | | | | | |
|----|-------|-------|-------|--------|-------|--------|-----|
| 44 | 768.7 | 28.49 | 639.3 | 114.26 | .9468 | 6.7277 | 219 |
| 45 | 768.9 | 28.49 | 639.4 | 114.04 | .9467 | 6.7419 | |
| 46 | 769.0 | 28.49 | 639.5 | 113.82 | .9466 | 6.7561 | |
| 47 | 769.1 | 28.49 | 639.6 | 113.60 | .9465 | 6.7702 | |
| 48 | 769.2 | 28.49 | 639.7 | 113.38 | .9464 | 6.7843 | |
| 49 | 769.3 | 28.49 | 639.7 | 113.16 | .9463 | 6.7980 | |

CODE REPORT

TOWER # 2 Data file: col17.OUT Profile file: pool.prf
 Tray Vapor Properties

| Stg | Mass flow kg/hr | Avg mol wt | Standard Vol. flow m3/hr | Actual Vol. flow m3/hr | Z | Actual density kg/m3 |
|-----|--------------------|---------------|--------------------------------|------------------------------|-------|----------------------------|
| 50 | 769.2 | 28.50 | 639.4 | 112.94 | .9463 | 6.8108 |
| 51 | 768.8 | 28.52 | 638.5 | 112.71 | .9464 | 6.8211 |
| 52 | 767.5 | 28.58 | 636.1 | 112.46 | .9467 | 6.8253 |
| 53 | 764.1 | 28.74 | 629.8 | 112.12 | .9475 | 6.8152 |
| 54 | 756.3 | 29.13 | 615.1 | 111.51 | .9494 | 6.7821 |
| 55 | 743.7 | 29.88 | 589.6 | 110.28 | .9524 | 6.7434 |
| 56 | 733.8 | 30.85 | 563.4 | 108.76 | .9549 | 6.7469 |
| 57 | 733.1 | 31.56 | 550.3 | 108.13 | .9562 | 6.7792 |

CODE: Chemical Engineering Simulation System
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TOWER # 2 Data file: col17.TSZ Profile file: pool.prf

Smith-Dresser-Ohlswager Shortcut Technique

User Provided Input Data

Tray spacing (in. or cm) 7.0000
 Downcomer area (ft2 or m2) .0236
 Weir length (in. or cm) 30.0000
 Weir height (in. or cm) 3.0000

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|-------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 1 | .3980 | .00 | .04 | 1504.0130 | 6.1901 | .4043 | .0373 |
| 2 | .3922 | .00 | .04 | 1504.1240 | 6.2043 | .4046 | .0373 |
| 3 | .3920 | .00 | .04 | 1504.3670 | 6.2184 | .4042 | .0373 |
| 4 | .3918 | .00 | .04 | 1504.7920 | 6.2324 | .4038 | .0373 |
| 5 | .3915 | .00 | .04 | 1505.4480 | 6.2462 | .4035 | .0373 |
| 6 | .3913 | .00 | .04 | 1506.4320 | 6.2596 | .4032 | .0373 |
| 7 | .3910 | .00 | .04 | 1507.8550 | 6.2727 | .4029 | .0373 |
| 8 | .3907 | .00 | .04 | 1509.8700 | 6.2851 | .4028 | .0373 |
| 9 | .3904 | .00 | .04 | 1512.6680 | 6.2970 | .4028 | .0373 |
| 10 | .3899 | .00 | .04 | 1516.4700 | 6.3078 | .4029 | .0373 |
| 11 | .3894 | .00 | .04 | 1521.5240 | 6.3175 | .4033 | .0373 |
| 12 | .3889 | .00 | .04 | 1528.0850 | 6.3257 | .4038 | .0373 |
| 13 | .3882 | .00 | .04 | 1536.3290 | 6.3323 | .4046 | .0374 |
| 14 | .3874 | .00 | .04 | 1546.3010 | 6.3370 | .4057 | .0374 |
| 15 | .3865 | .00 | .04 | 1557.7830 | 6.3400 | .4070 | .0374 |

392091

| | | | | | | | |
|----|-------|-----|-----|-----------|--------|-------|-------|
| 16 | .3856 | .00 | .04 | 1570.2490 | 6.3417 | .4085 | .0374 |
| 17 | .3935 | .01 | .04 | 1582.9050 | 6.3428 | .3874 | .0353 |
| 18 | .3775 | .01 | .03 | 1582.7020 | 6.3570 | .3785 | .0353 |
| 19 | .3774 | .01 | .03 | 1582.5090 | 6.3713 | .3780 | .0353 |
| 20 | .3773 | .01 | .03 | 1582.3070 | 6.3856 | .3775 | .0353 |
| 21 | .3772 | .01 | .03 | 1582.1040 | 6.3998 | .3769 | .0353 |
| 22 | .3771 | .01 | .03 | 1581.9110 | 6.4142 | .3764 | .0353 |
| 23 | .3770 | .01 | .03 | 1581.7080 | 6.4284 | .3759 | .0353 |
| 24 | .3769 | .01 | .03 | 1581.5140 | 6.4427 | .3754 | .0353 |
| 25 | .3768 | .01 | .03 | 1581.3110 | 6.4569 | .3748 | .0353 |
| 26 | .3767 | .01 | .03 | 1581.1170 | 6.4713 | .3743 | .0353 |
| 27 | .3766 | .01 | .03 | 1580.9240 | 6.4855 | .3738 | .0353 |
| 28 | .3765 | .01 | .03 | 1580.7200 | 6.4998 | .3733 | .0353 |

CODE REPORT

Smith-Dresser-Ohlswager Shortcut Technique

| Stg | Diameter meter | Liquid Vol. flow m3/min | Vapor Vol. flow m3/sec | Liquid density kg/m3 | Vapor density kg/m3 | Flooding velocity m/sec | Settling height meter |
|-----|--------------------------------|-------------------------------|------------------------------|----------------------------|---------------------------|-------------------------------|-----------------------------|
| 29 | .3764 | .01 | .03 | 1580.5260 | 6.5140 | .3728 | .0353 |
| 30 | .3763 | .01 | .03 | 1580.3320 | 6.5283 | .3723 | .0353 |
| 31 | .3762 | .01 | .03 | 1580.1380 | 6.5426 | .3718 | .0353 |
| 32 | .3761 | .01 | .03 | 1579.9430 | 6.5569 | .3713 | .0353 |
| 33 | .3760 | .01 | .03 | 1579.7490 | 6.5711 | .3708 | .0353 |
| 34 | .3760 | .01 | .03 | 1579.5550 | 6.5854 | .3703 | .0353 |
| 35 | .3759 | .01 | .03 | 1579.3600 | 6.5996 | .3697 | .0353 |
| 36 | .3758 | .01 | .03 | 1579.1650 | 6.6139 | .3692 | .0353 |
| 37 | .3757 | .01 | .03 | 1578.9700 | 6.6281 | .3687 | .0353 |
| 38 | .3756 | .01 | .03 | 1578.7750 | 6.6423 | .3683 | .0353 |
| 39 | .3755 | .01 | .03 | 1578.5810 | 6.6566 | .3678 | .0353 |
| 40 | .3754 | .01 | .03 | 1578.3860 | 6.6708 | .3673 | .0353 |
| 41 | .3753 | .01 | .03 | 1578.1910 | 6.6851 | .3668 | .0353 |
| 42 | .3752 | .01 | .03 | 1578.0060 | 6.6993 | .3663 | .0353 |
| 43 | .3751 | .01 | .03 | 1577.8130 | 6.7136 | .3658 | .0353 |
| 44 | .3751 | .01 | .03 | 1577.6220 | 6.7278 | .3653 | .0353 |
| 45 | .3750 | .01 | .03 | 1577.4390 | 6.7420 | .3648 | .0353 |
| 46 | .3749 | .01 | .03 | 1577.2740 | 6.7562 | .3643 | .0353 |
| 47 | .3748 | .01 | .03 | 1577.1440 | 6.7703 | .3639 | .0353 |
| 48 | .3747 | .01 | .03 | 1577.1360 | 6.7844 | .3634 | .0353 |
| 49 | .3746 | .01 | .03 | 1577.4200 | 6.7981 | .3630 | .0353 |
| 50 | .3744 | .01 | .03 | 1578.5160 | 6.8109 | .3628 | .0353 |
| 51 | .3740 | .01 | .03 | 1581.7190 | 6.8212 | .3630 | .0353 |
| 52 | .3732 | .01 | .03 | 1590.2160 | 6.8254 | .3642 | .0353 |
| 53 | .3714 | .01 | .03 | 1610.1480 | 6.8153 | .3675 | .0354 |
| 54 | .3682 | .01 | .03 | 1646.2870 | 6.7822 | .3738 | .0355 |
| 55 | .3643 | .01 | .03 | 1684.6500 | 6.7435 | .3798 | .0356 |
| 56 | .3618 | .01 | .03 | 1703.7580 | 6.7469 | .3814 | .0356 |
| 57 | ***Reboiler: No tray sizing*** | | | | | | |